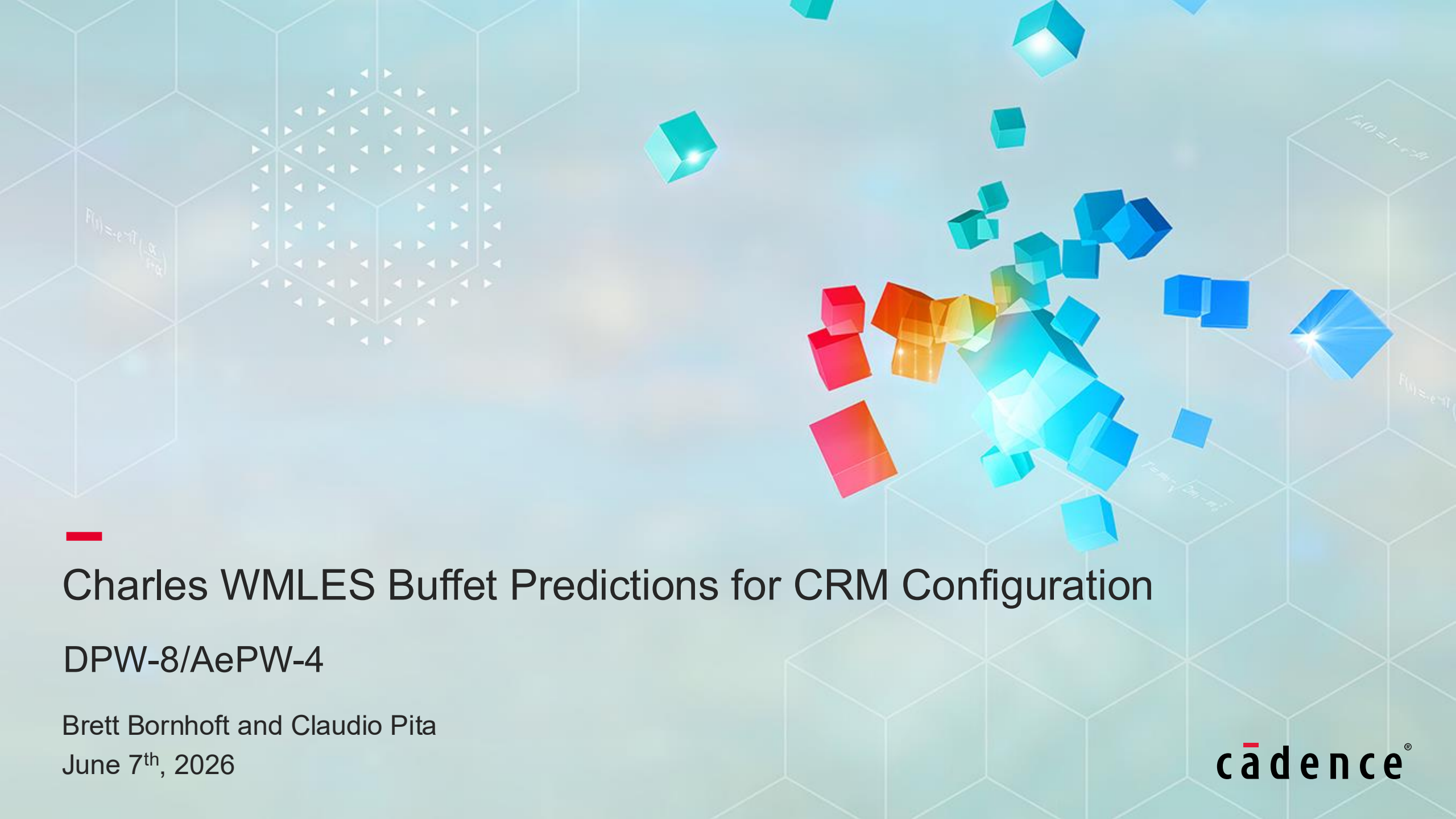




Charles WMLES Buffet Predictions for CRM Configuration

DPW-8/AePW-4

Brett Bornhoft and Claudio Pita

June 7th, 2026

Prediction of Buffet on the 2.16% scale NASA CRM

Notes on the experimental setup

- Focus on DPW-8 Test Case 2
- Operation Conditions:
 - $Re=1.5M$, $M=0.85$
 - AoAs : 1.22, 2.29, 4.84, 5.89
 - Geometry is different for each AoA given the scanned model's deformation
- Uncertainty of setup from provided CAD:
 - Simulating as far-field (w/o 2 x 2m tunnel)
 - No sting

Methodology

- Compressible Flow Solver: **Fidelity Charles**

- Low-dissipation numerics
- 2nd order finite-volume method
- Kinetic Energy and Entropy Preserving (KEEP)
- Explicit RK time integration
- GPU Accelerated

- Wall Modeled:

- Algebraic equilibrium wall model (EQWM)

- 2nd Point matching EQWM (N2WM)

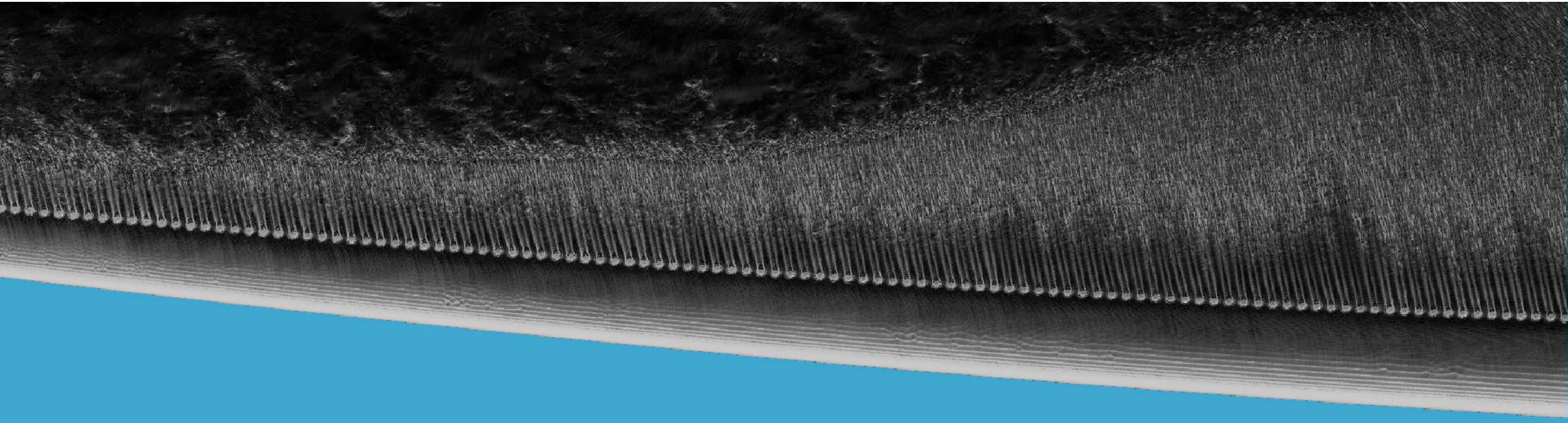
- Sensor-based WM for transition (SBWM)

- Subgrid-Scale Model:

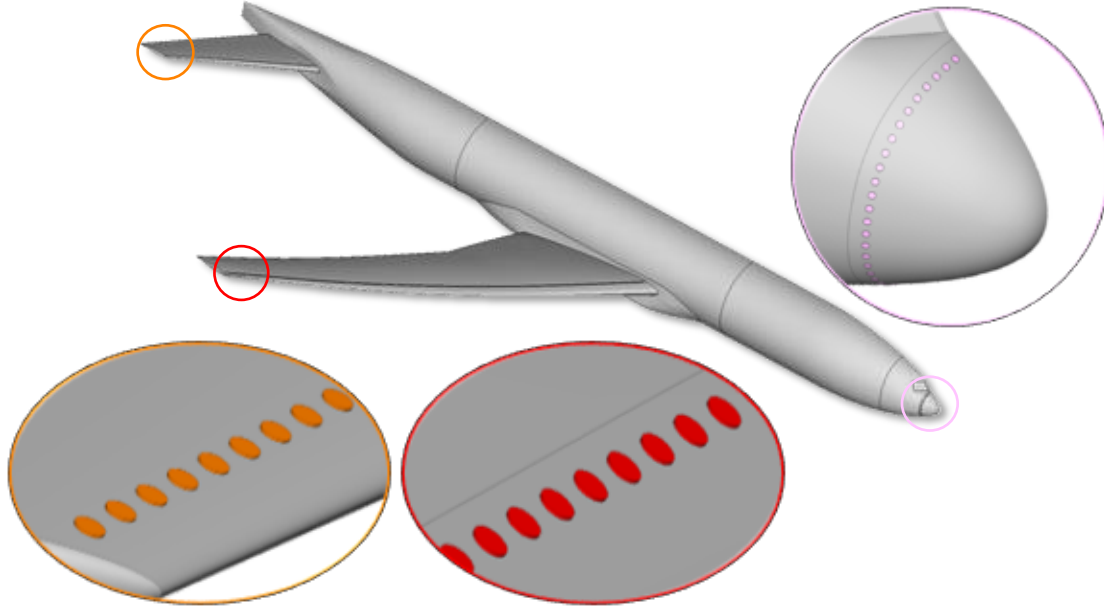
- Dynamic Smagorinsky model

- Grid Generation: StitchTM

- Custom grid generator for Fidelity Charles
- Voronoi grids of hexagonal close-packed topology with near wall stranded meshes



Gridding Approach



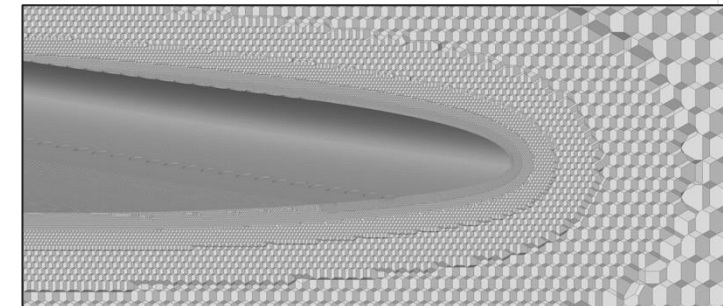
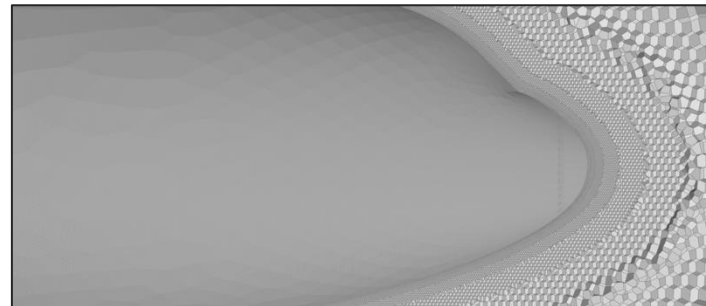
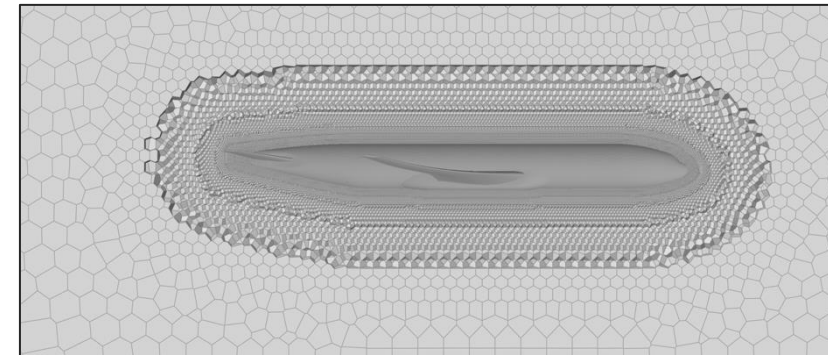
Trip	Aeronautical trip dot (CAD Cut)
Diameter [mm]	1.27
Distance (between dot centers) [mm]	2.54
Height (main wing) [mm]	0.11430 (inner-wing) 0.09906 (mid-wing) 0.08890 (outer-wing)
Location (main wing)	10% chord (upper and lower sides)
Height (horizontal stabilizers) [mm]	0.09906
Location (horizontal stabilizers)	10% chord (upper and lower sides)
Height (body) [mm]	0.08890
Location (body)	1.5% body length (azimuthally around the nose)

Surface Tessellation (Fidelity Pointwise)

- Trip dots created and added to the original CAD data via a Glyph script (~5 minutes).
- Surface tessellation generated via the Automatic Surface Mesh tool (~5 minutes)
- Surface tessellation exported in *.sbin format to be used with Stitch (~1 minute)

Voronoi Volume Meshes (Stich)

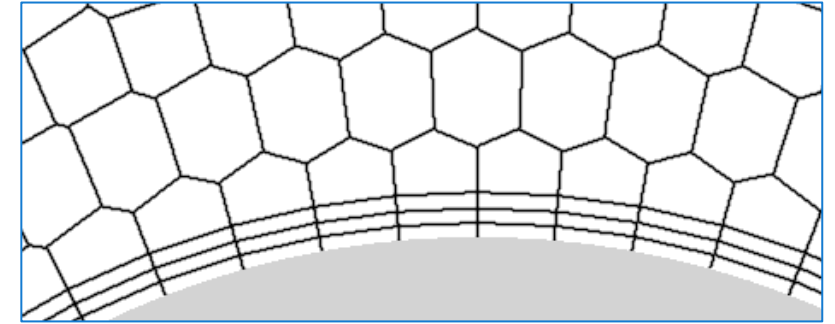
- Stich is the native mesh generator for Fidelity Charles.
- Generation of Voronoi volume meshes as detailed in previous slide.



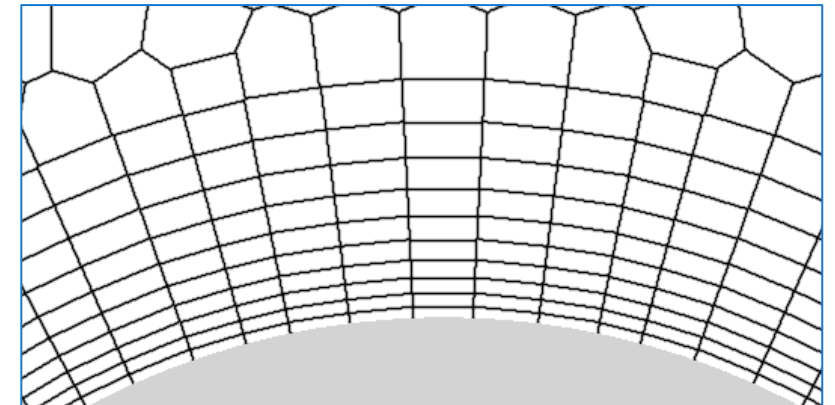
Gridding Approach

- We employ three different gridding approaches:
 - Adding higher-aspect ratio cells to the first wall cell (AR)
 - Boundary layer stranded mesh (SVP)
 - AR cells with physical trip dots (TR)
- Mesh level is a scaling based on :
 - $\Delta_L = \Delta_0 \left(\frac{1}{2}\right)^L$, where $\Delta_0 = MAC = 0.1513\ m$
- Resolutions include (LVL <streamwise>/<wall normal>)
 - LVL9/11 → 141 Mcvs, $y_{LE}^+ \sim 24$, $y_{\eta=0.5}^+ \sim 8$
 - LVL10/12 → 399 Mcvs, $y_{LE}^+ \sim 12$, $y_{\eta=0.5}^+ \sim 4$
 - LVL 11/13 → 609 Mcvs, $y_{LE}^+ \sim 6$, $y_{\eta=0.5}^+ \sim 2$
 - Local increase to wing LE, TE, upper surface, and wing tip
 - Up to LVL 13/15 → 884 Mcvs, $y_{LE}^+ \sim 3$, $y_{\eta=0.5}^+ \sim 2$
 - Uses a solution-based refinement technique (Agrawal et al.*) from Xfine mesh and excludes horizontal stabilizer and lower wing surface..
- **Note:** Trip dots set to LVL 13 w/isotropic cells ensuring enough resolution to be geometrically resolved

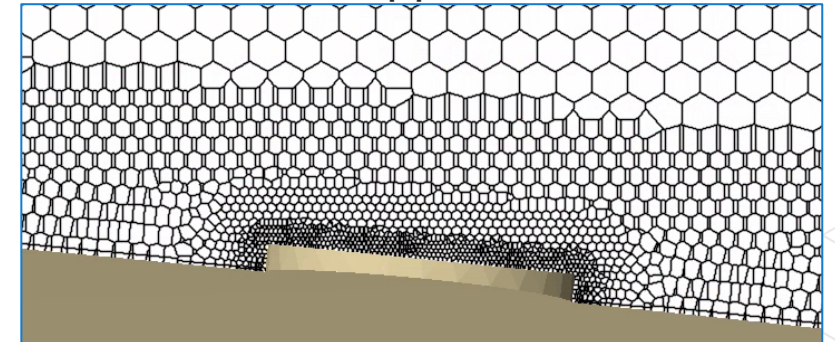
AR approach (4:1)



SVP approach (5:1)



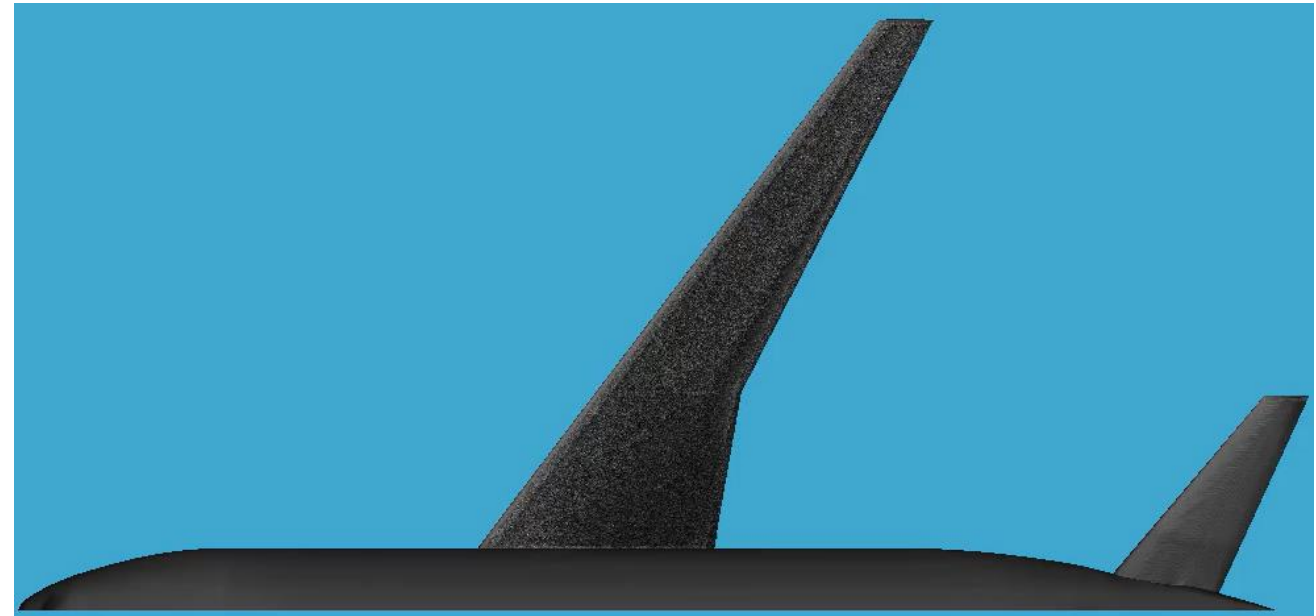
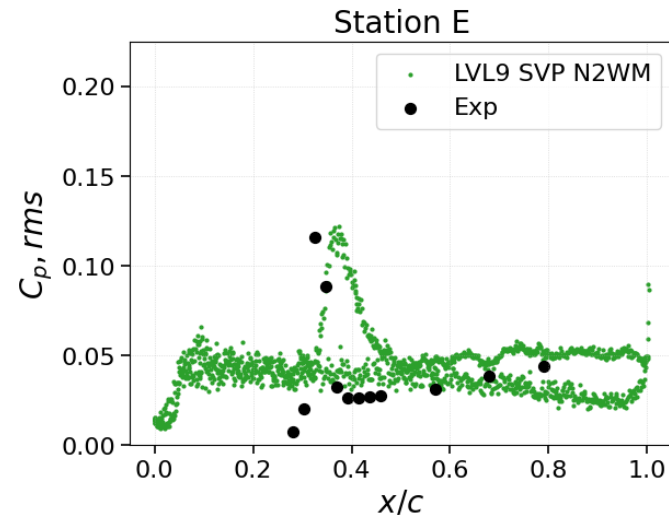
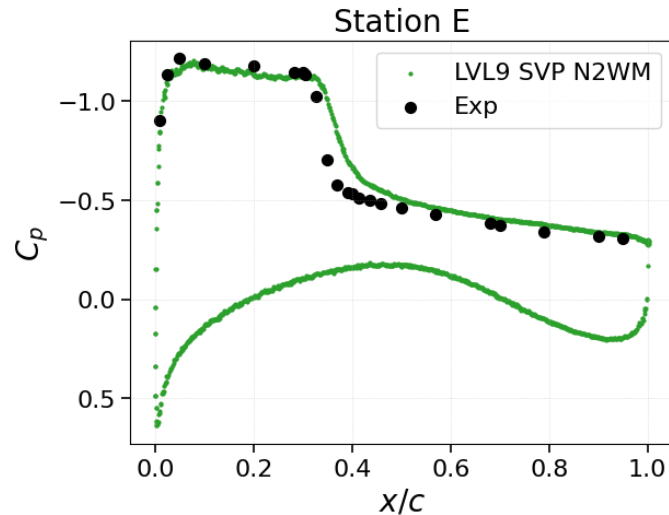
TR approach



Near Wall Modeling Sensitivities

Grid Resolution and Wall Model Treatment, AoA=4.84 degrees

2nd Point Matching WM

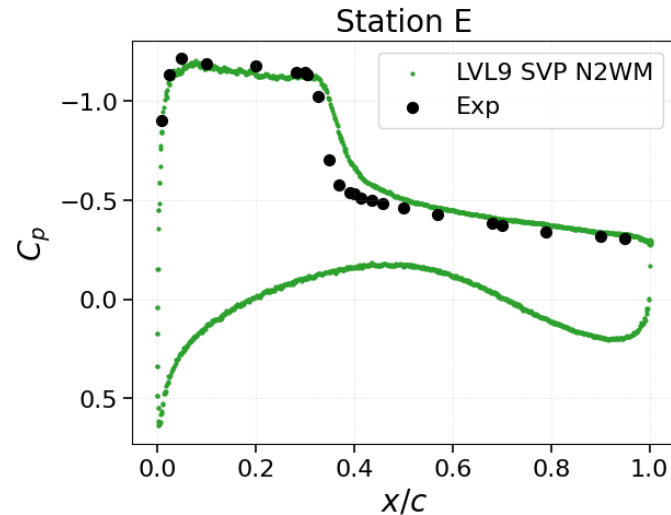


- Coarse grid + stranded mesh + 2nd point matching WM yields reasonable shock location and ok $C_{p,rms}$ peak
- Upstream C_p value wildly over predicted
- Transition occurs instantly, but $C_{p,rms}$ curve suggests delayed transition

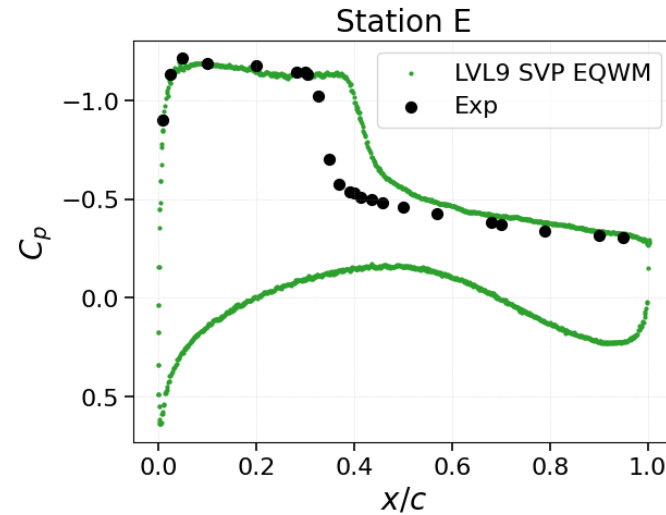
Near Wall Modeling Sensitivities

Grid Resolution and Wall Model Treatment, AoA=4.84 degrees

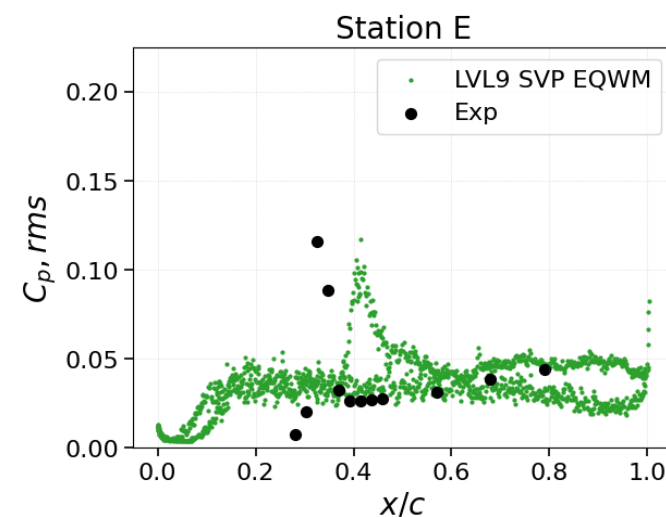
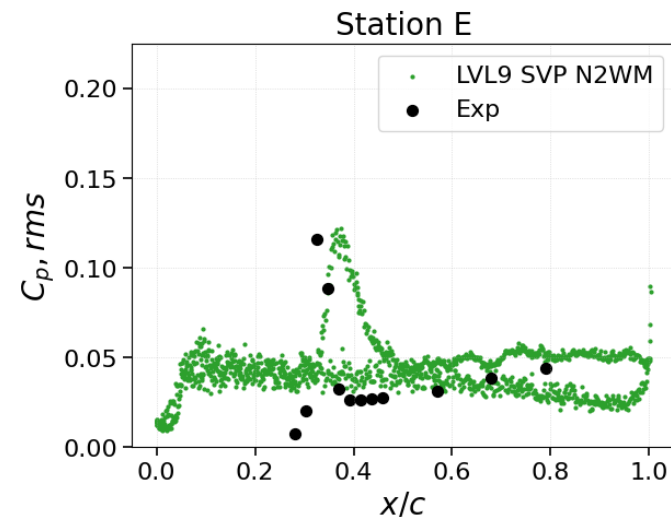
2nd Point Matching WM



EQWM



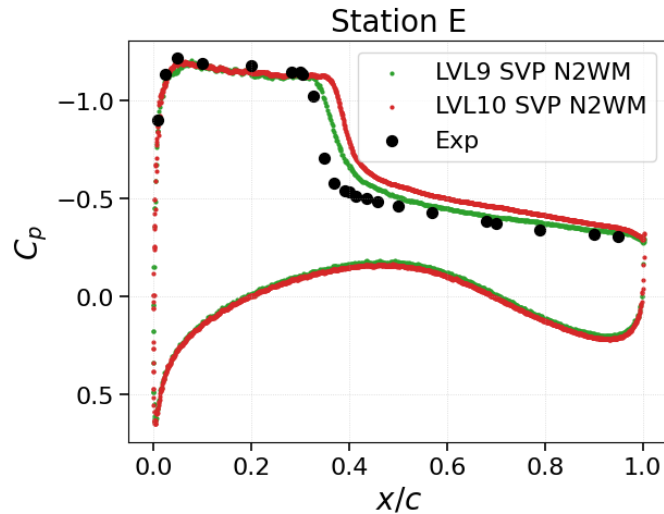
- EQWM had a further downstream shock position location compared to experiment
- Upstream boundary layer remains laminar further downstream



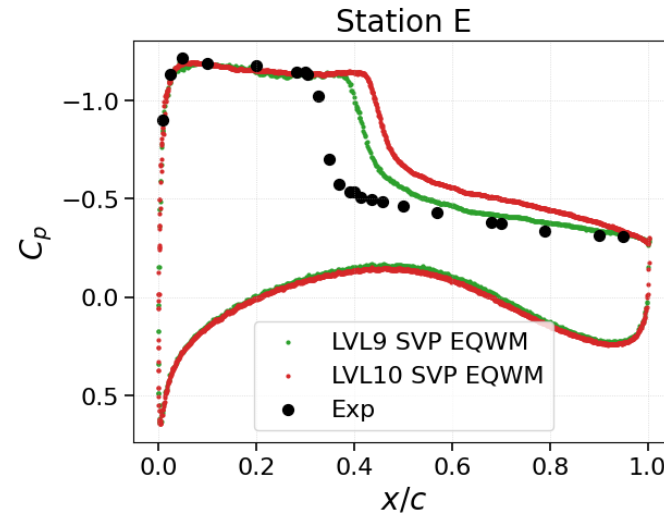
Near Wall Modeling Sensitivities

Grid Resolution and Wall Model Treatment, AoA=4.84 degrees

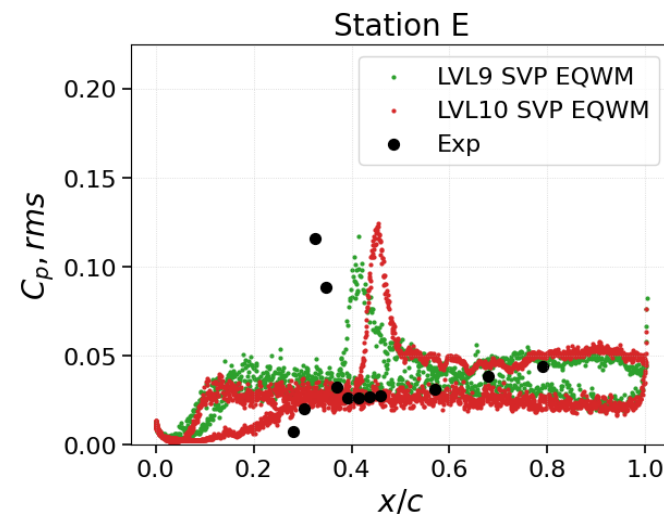
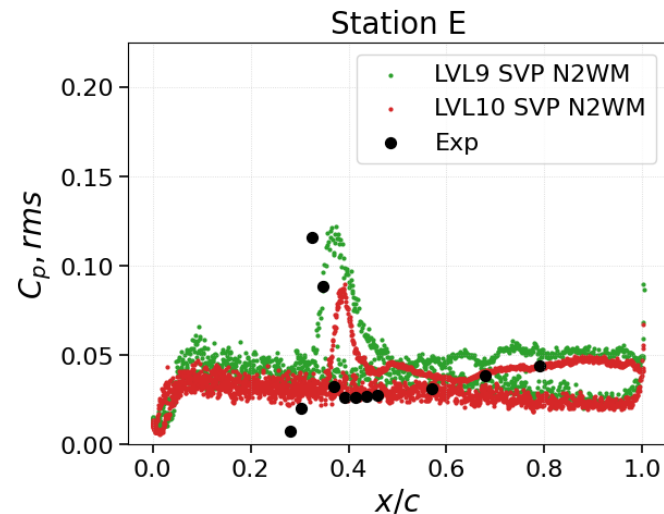
2nd Point Matching WM



EQWM



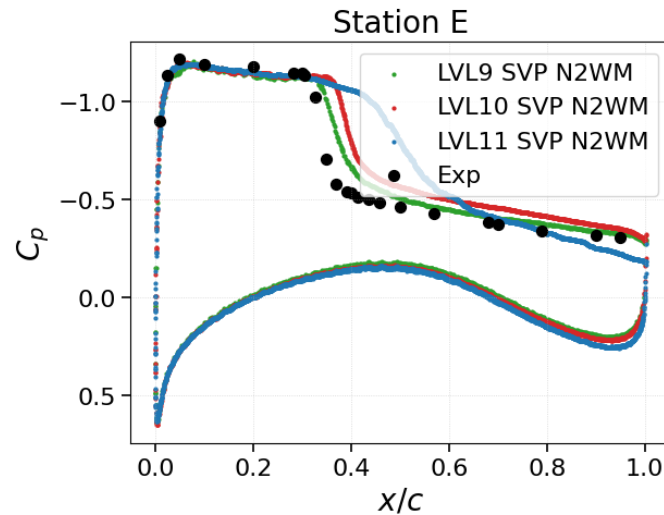
- 2nd point matching is more robust to shock location from grid
- EQWM improves upstream RMS value prior to the shock.



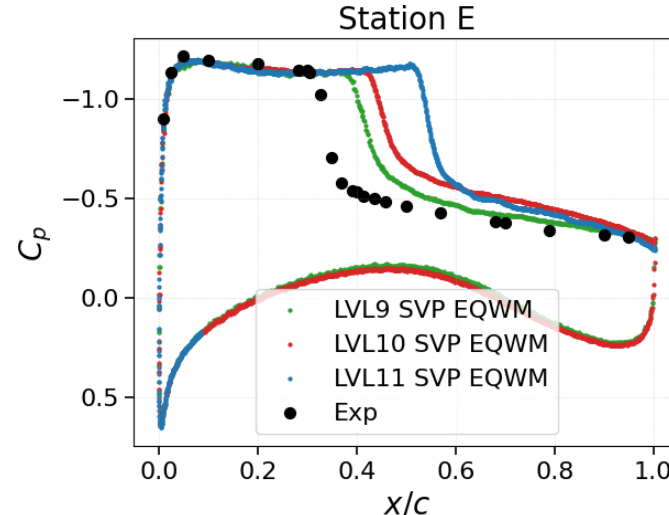
Near Wall Modeling Sensitivities

Grid Resolution and Wall Model Treatment, AoA=4.84 degrees

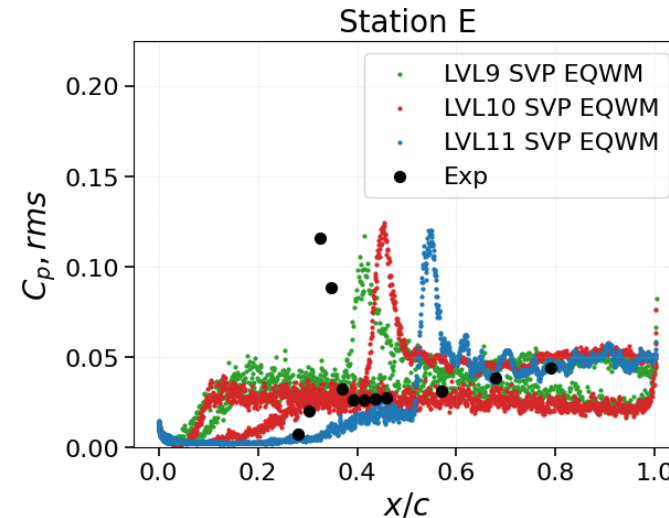
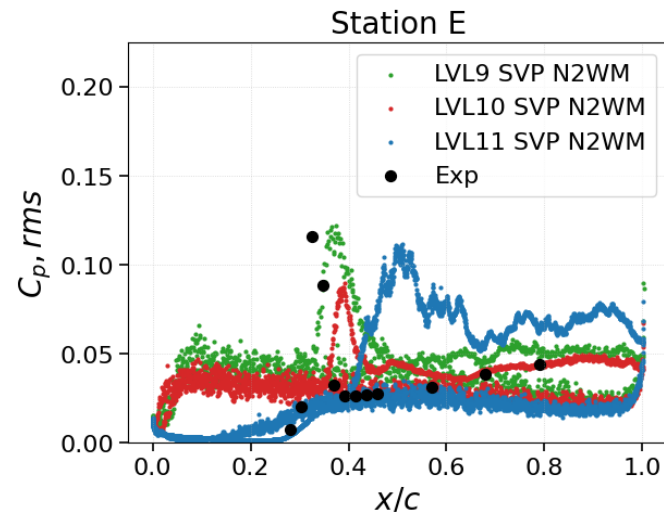
2nd Point Matching WM



EQWM



- At LVL11, both shock positions shift to the right.
- The region of laminar flow appears to have grown significantly



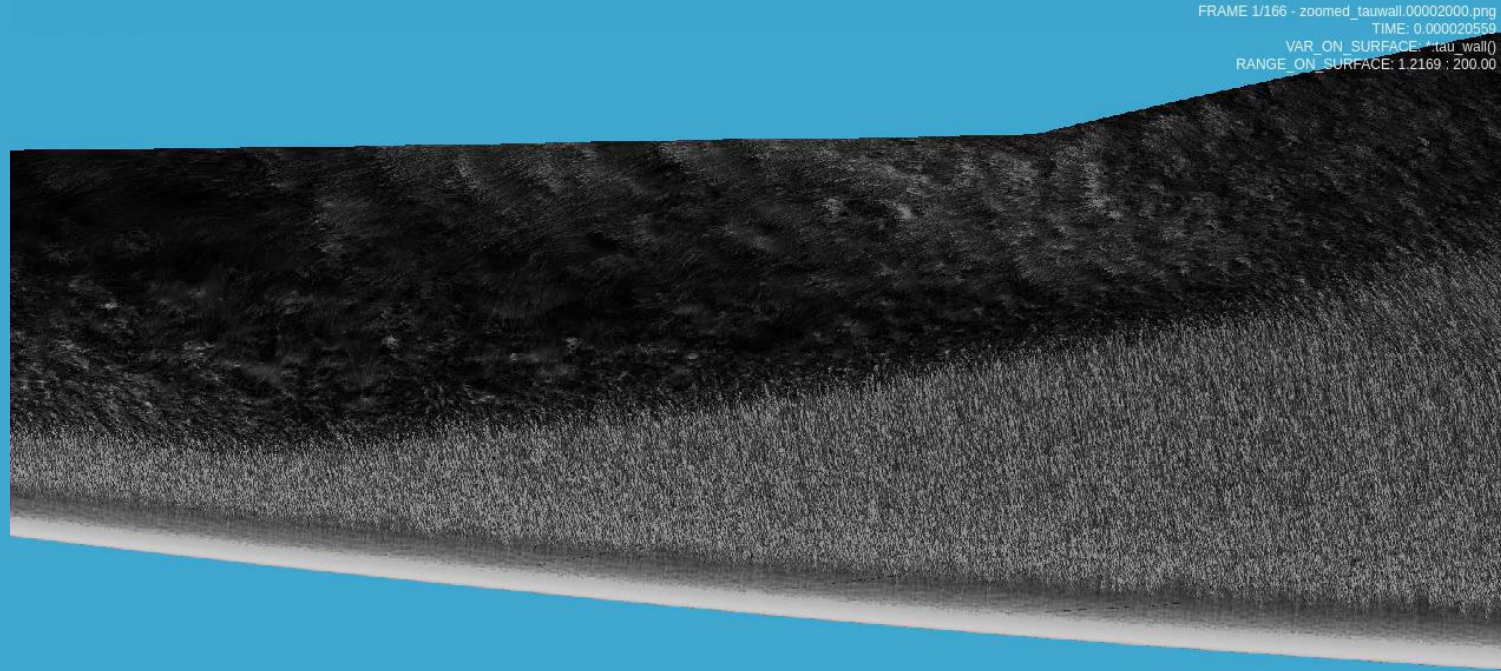
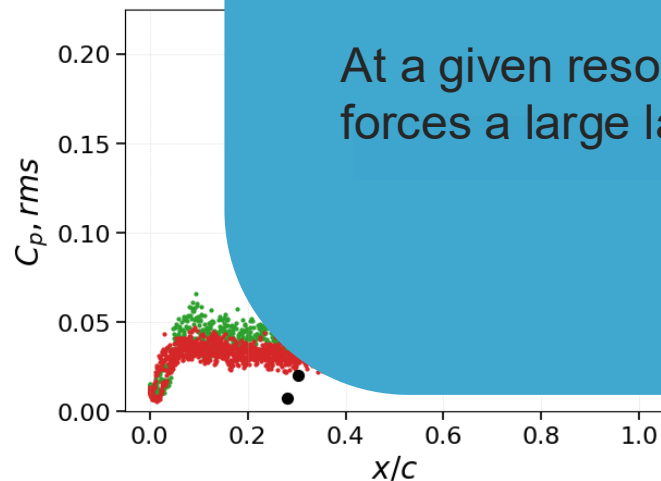
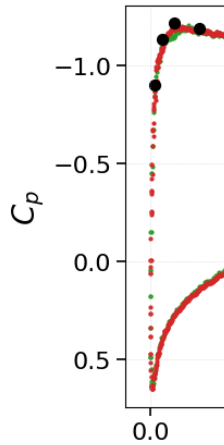
Note: 2nd point has fewer statistics at LVL11

Near Wall Modeling Sensitivities

Grid Resolution and Wall Model Treatment AoA=4.84 degrees

Increased resolution from LVL10->11 w/2nd point matching

2nd P



FRAME 1/166 - zoomed_tauwall.00002000.png
TIME: 0.000020559
VAR_ON_SURFACE: tau_wall()
RANGE_ON_SURFACE: 1.2169 ; 200.00

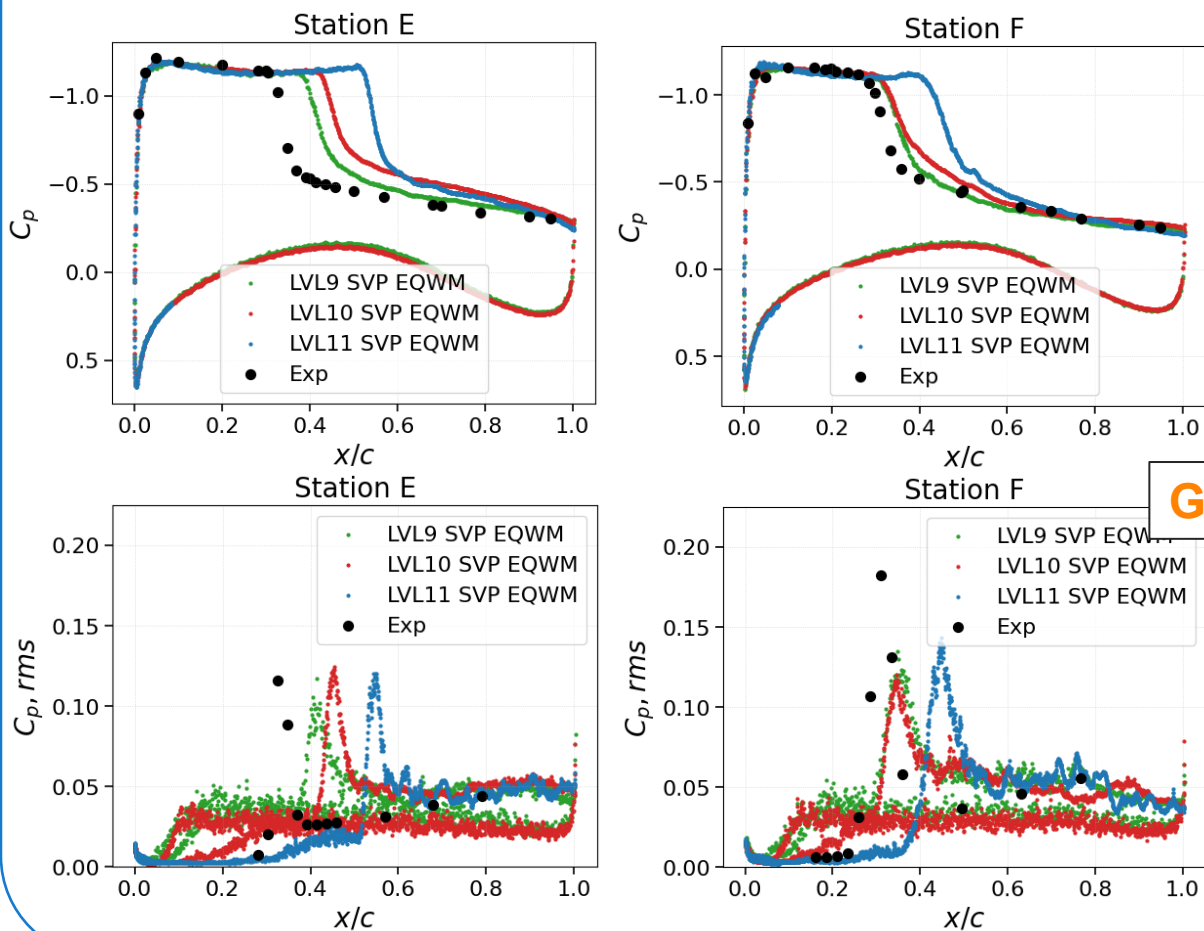
At a given resolution, the boundary layer begins to be better resolved and forces a large laminar region. This motivates the use of two things:

1. Geometrically resolved trip dots
2. A transition-sensor wall model

Near Wall Modeling Sensitivities

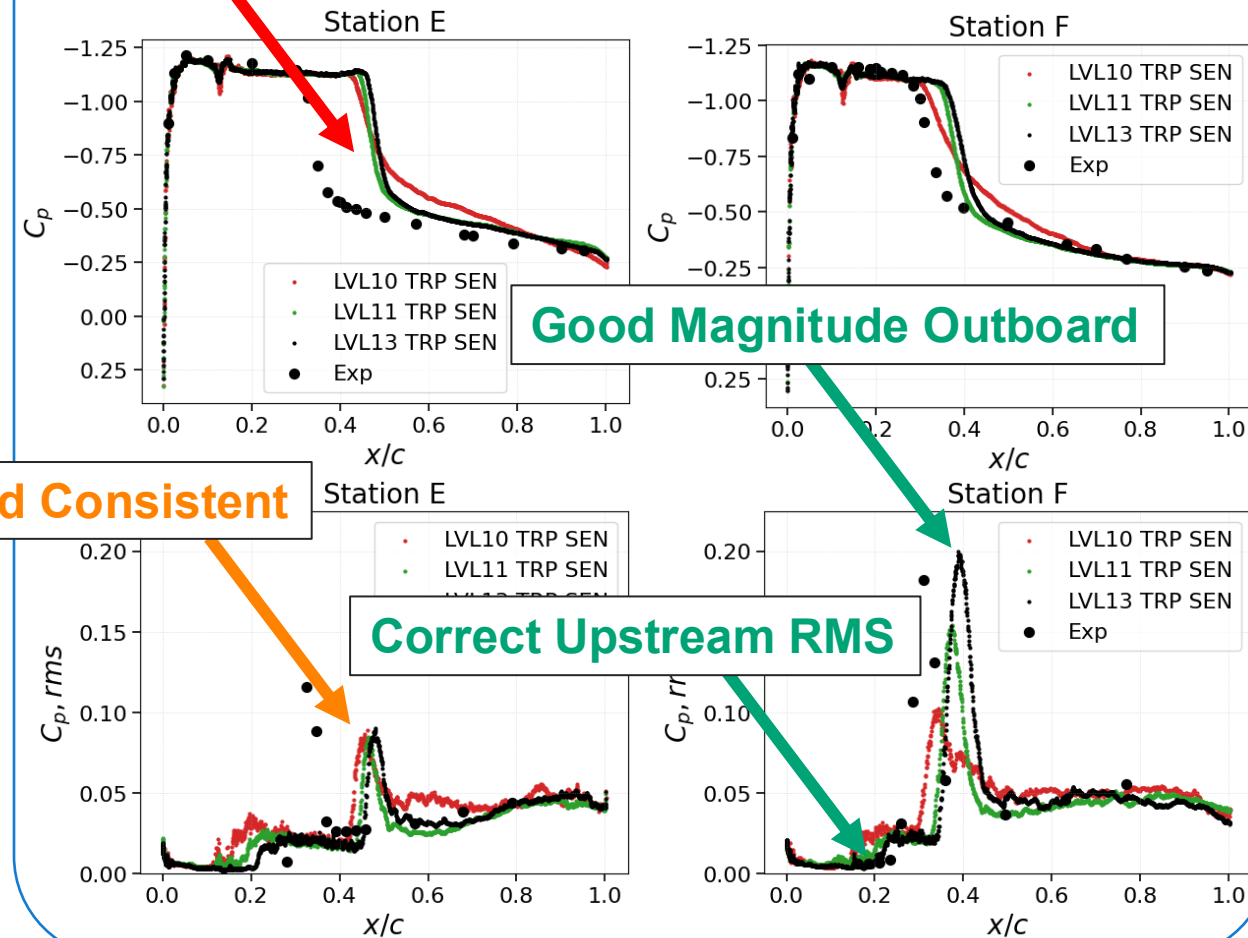
Effect of Trip Dots + Sensor WM

Nat Trans. + EQWM



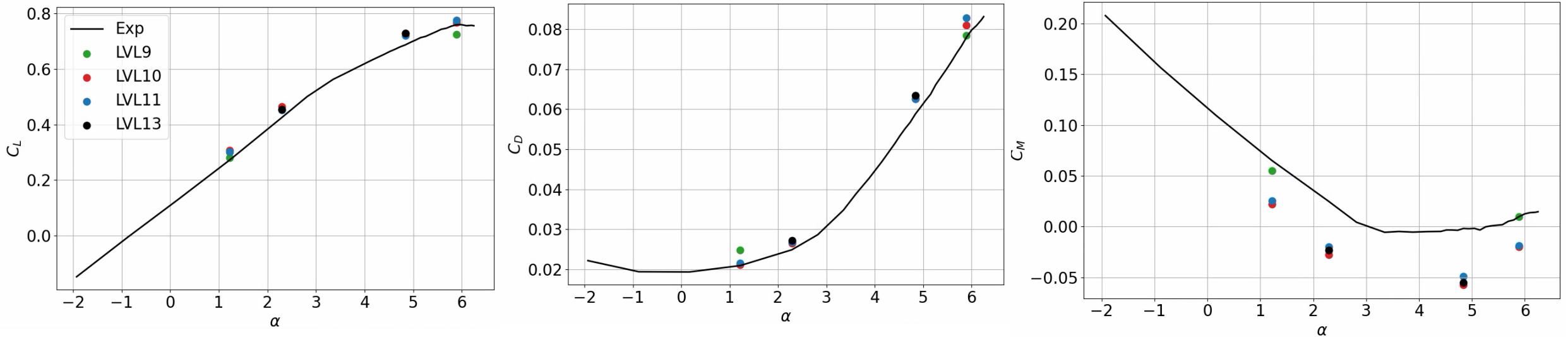
Delayed Shock

Trip Dots + Sensor WM



Forces and Moments

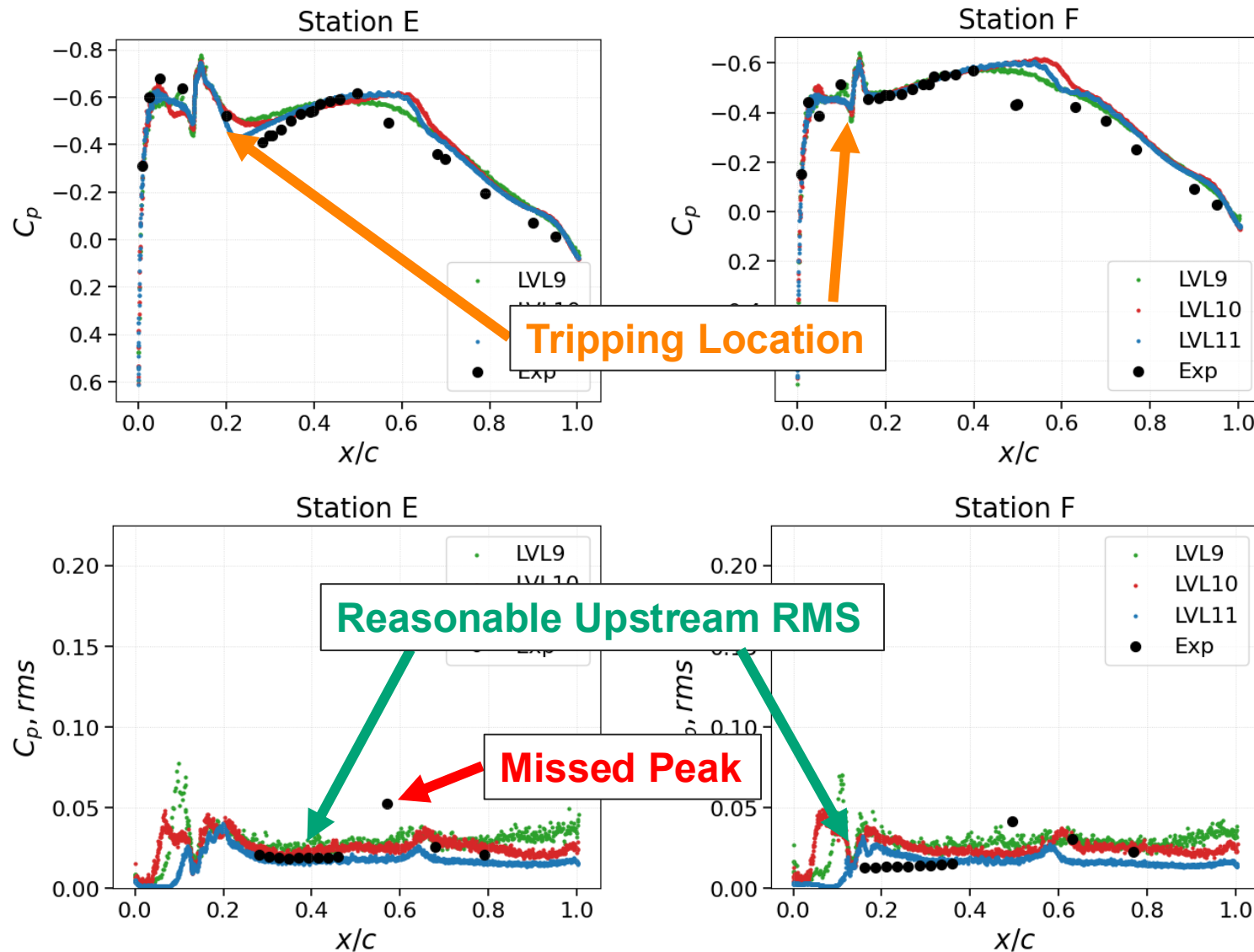
Angle of Attack Sweep with Trip Dots and Sensor-Based Wall Model



- Forces and moments do not differ much from grid to grid for the trip dots with sensor-based wall model approach.
- Lift/Drag yield reasonable results while moment is largely underpredicted
 - Note : Moment issues are consistent with transonic cases found in the literature*

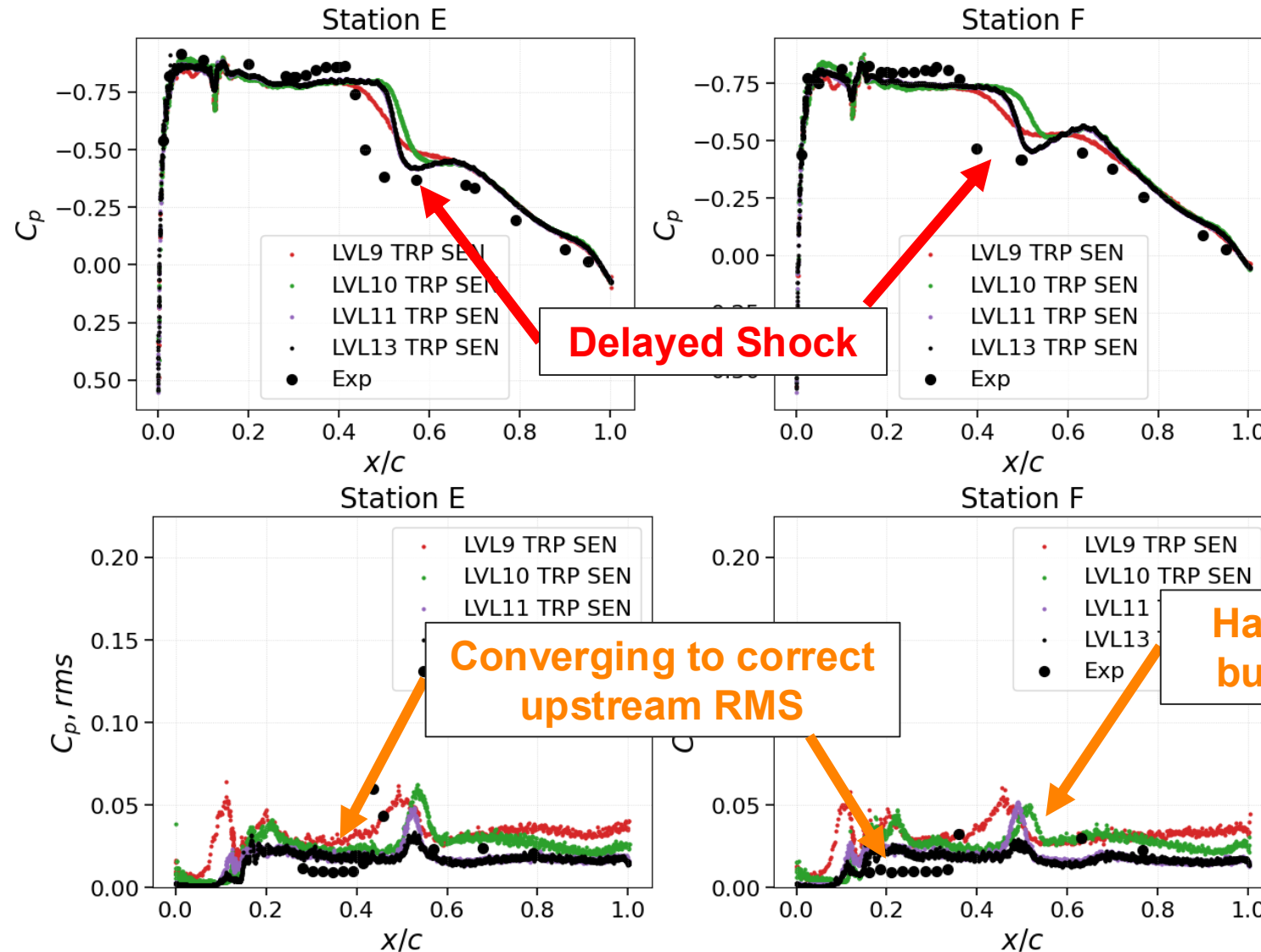
Mean and RMS Pressures

AoA = 1.22



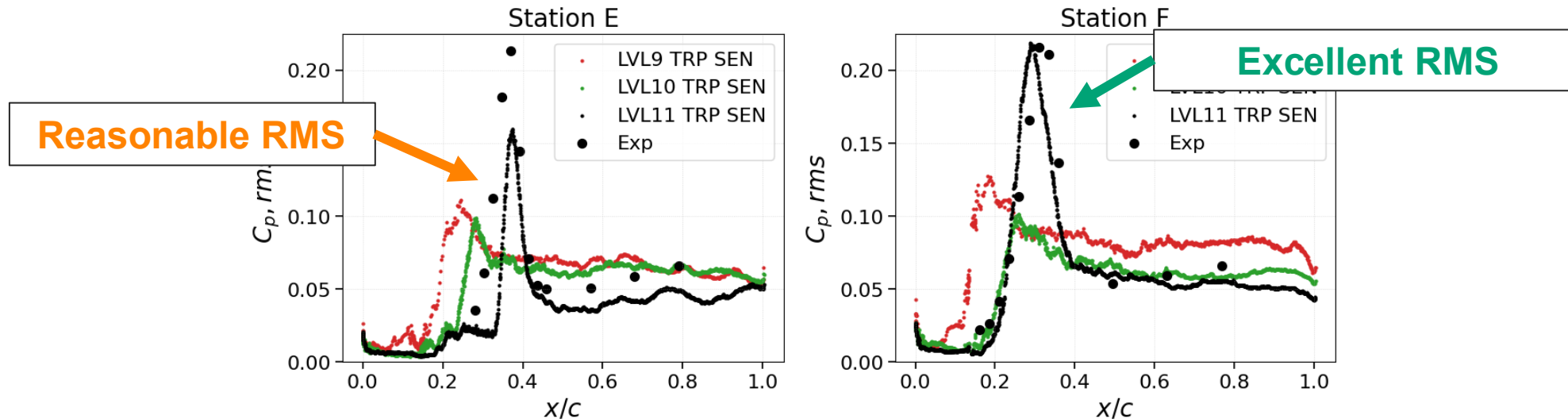
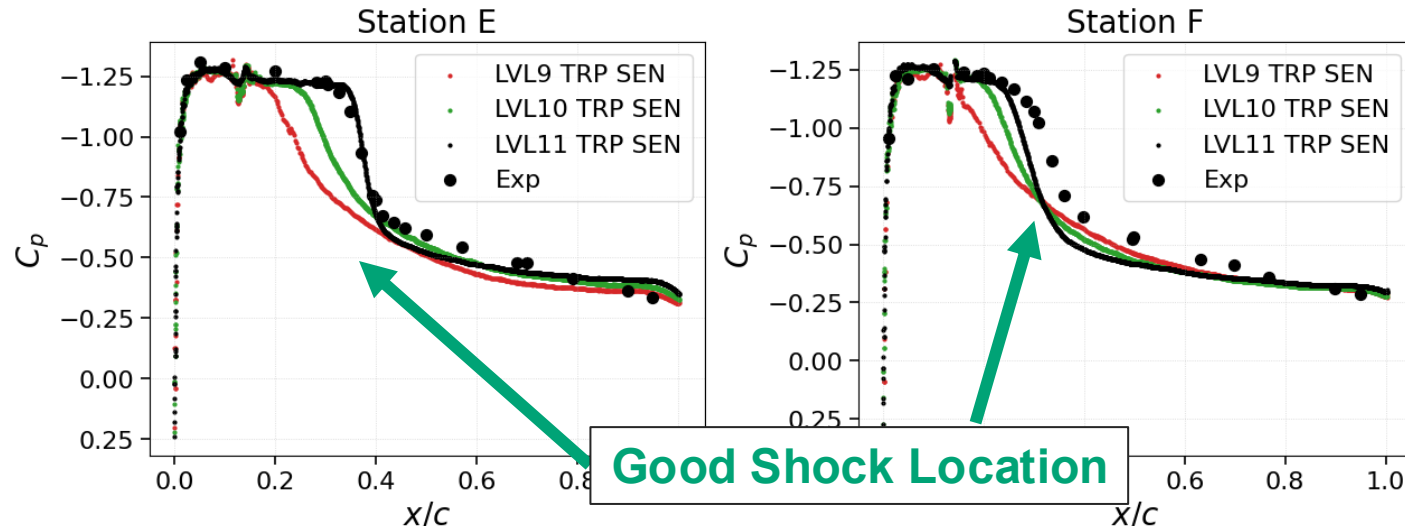
Mean and RMS Pressures

AoA = 2.29

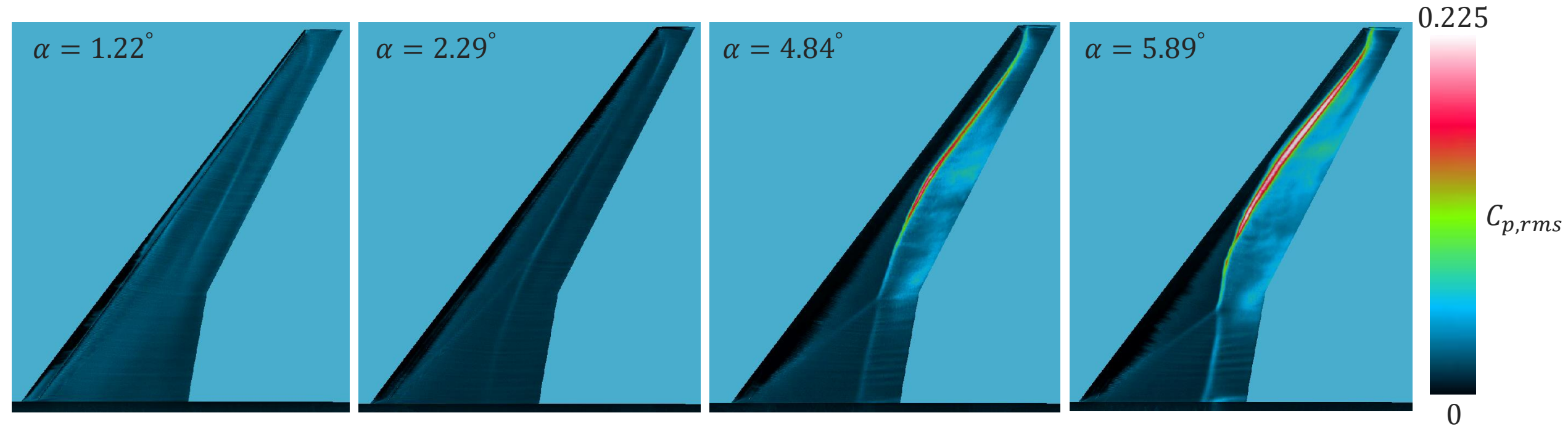


Mean and RMS Pressures

AoA = 5.89



Comparison of RMS Values



Increasing angle of attack shows increased peak *RMS* values as expected

Key Conclusions and Open Questions

- **Key Conclusions:**

- Stranded mesh with a coarse grid and 2nd-point matching predicts reasonable shock location; however, **shock shifts downstream with refinement**, indicating sensitivity to near-wall treatment
- 2nd-point matching induces **early boundary-layer tripping near the leading edge** until the laminar region is sufficiently resolved
- **Trip dots with sensor-based wall modeling** show consistent behavior across grid levels
- Accurate RMS prediction at the leading edge requires **resolving the upstream boundary layer**

- **Open Questions:**

- What is the impact of **wind tunnel effects** (sting, confinement, turbulence intensity) on shock position?
- Do sensor-based wall model settings influence shock location?

- **Requests from Workshop:**

- Provide trip dot CAD geometry or, at minimum, precise (x,y,z) coordinates for each trip dot
- Provide additional CAD geometry for case with sting and additional details for the wind tunnel setup



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