

Kestrel Dual-Mesh Simulations for DPW-VII: Expanding the Envelope

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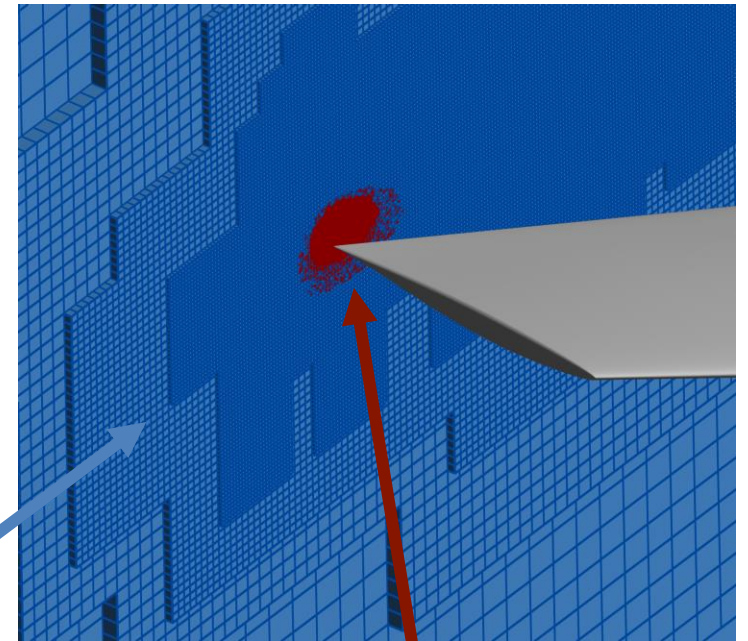
Outline

- **Kestrel Overview and Compute Environment**
- **Grids and Computational Methodology**
- **Selected Cases**
 - Case 1a: Grid Convergence Study
 - Case 2a: Alpha Sweep
 - Case 3: Reynolds Number Sweep
 - Case 4: RANS Grid Adaptation
 - Case 5: Beyond RANS (DDES with Grid Adaptation)
 - Extra credit interspersed throughout various Cases
- **Conclusions**

Kestrel CFD Solver



- **High-fidelity code from Department of Defense CREATE-AV**
 - Multidisciplinary tool that couples aerodynamics, S&C, thermochemistry, and propulsion
 - Cell centered
 - Includes RANS, URANS, and DDES schemes
 - Alpha-seeking for local time stepping
 - Alpha and C_L seeking for global time stepping
- **Inner/outer dual-mesh approach**
 - Static inner unstructured grid
 - Static or adaptive offbody Cartesian grid
 - Unstructured grid trimmed at constant distance
- **Executed with Kestrel 12.1 SDK**



Outer Cartesian Grid

Inner Unstructured Grid

Supercomputing Environment

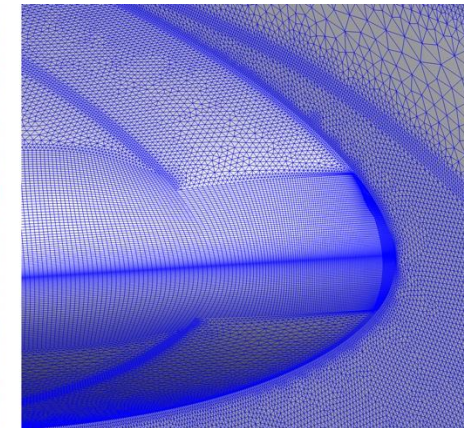
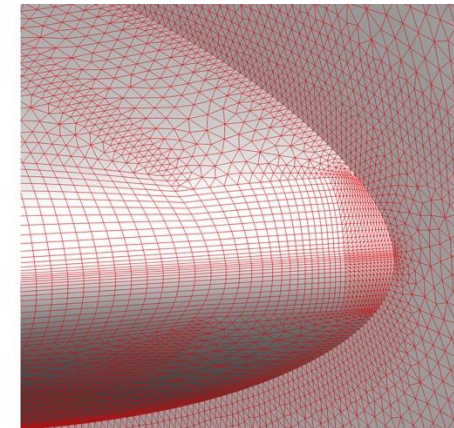
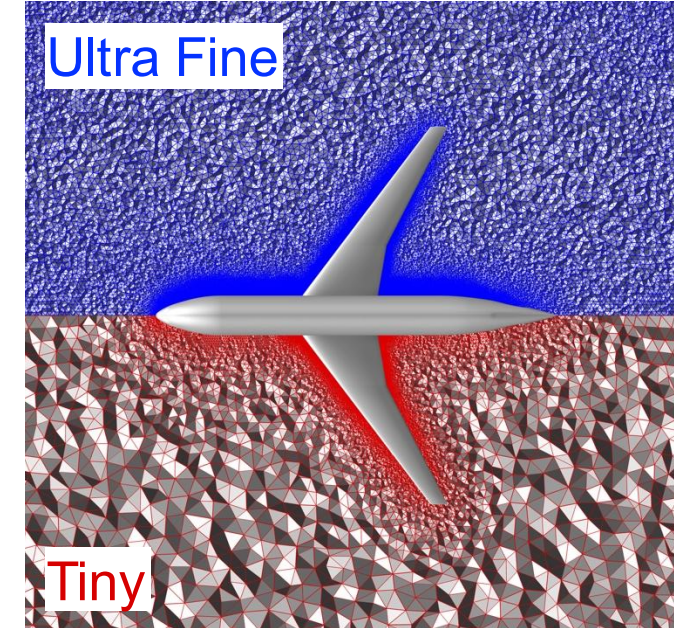
- **Executed on NASA Advanced Supercomputing (NAS) facility**
 - Comprised of four different supercomputers (Pleiades, Electra, Aitken, and Endeavour)
 - More than 11,000 nodes and 241,000 compute cores
 - Contains both Intel and AMD chips; TOSS3 (Linux 3) operating system
- **Resource usage for DPW-VII**
 - Intel Skylake nodes on Electra (a few select jobs on Haswell)
 - Between 1,600 and 3,200 processors
 - Walltime from a few hours to days
- **Total of 216 simulations**
 - Well in excess of 30 requested jobs for Cases 1a, 2a, 3, 4, and 5
 - Large number of runs due to significant additional investigation and alpha-searching



Grid Overview (1/2)

- Committee-supplied JAXA unstructured grids
- Variety of aeroelastic deformations
- Six different grid densities

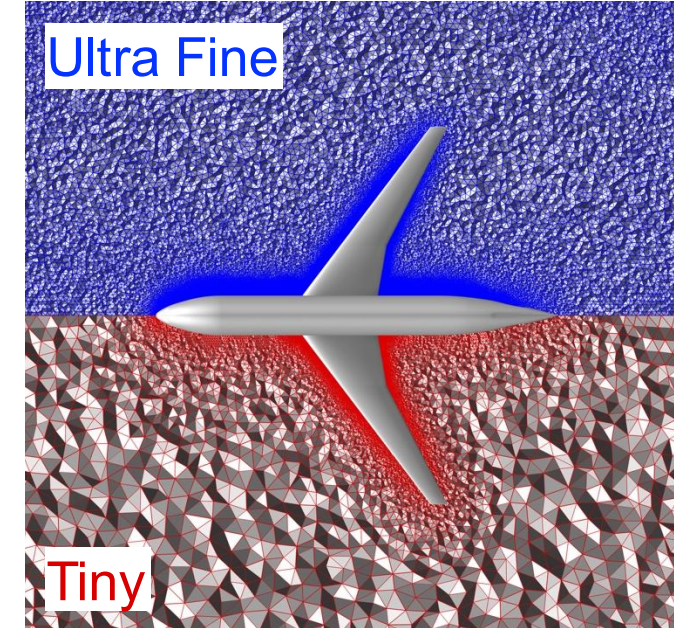
	Tiny	Coarse	Medium	Fine	Extra Fine	Ultra Fine
Level	L1	L2	L3	L4	L5	L6
Approximate Cell Count	8.7×10^6	26.9×10^6	60.2×10^6	111.8×10^6	184.1×10^6	291.2×10^6



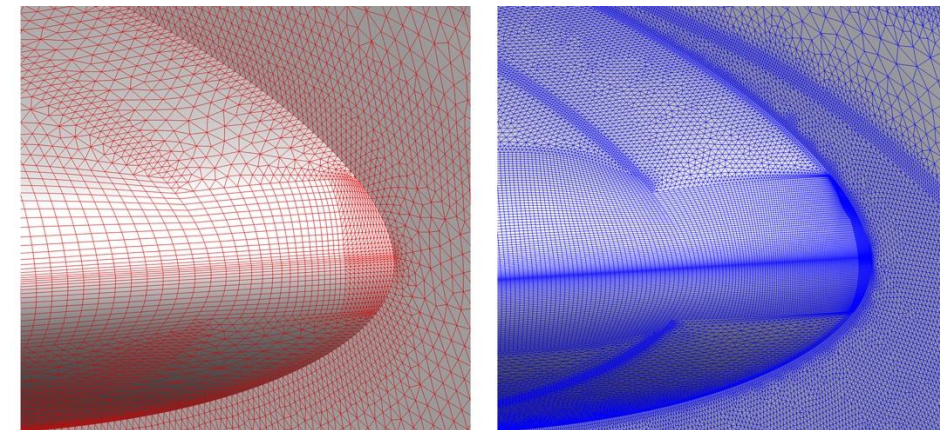
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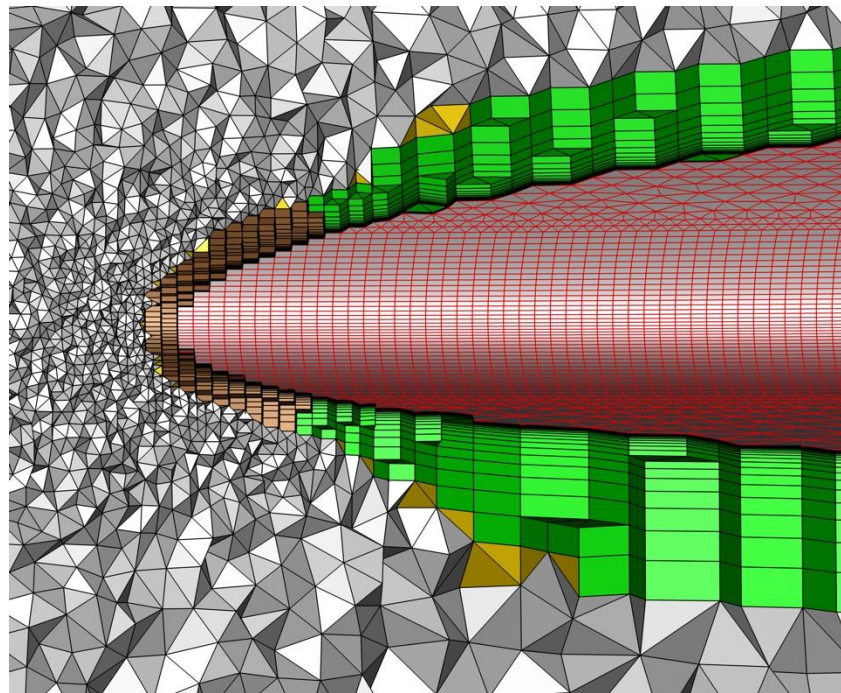


	Fully Unstructured	Adaptive Unstructured	Fixed Cartesian	Adaptive Cartesian
Case 1a	✓		✓	
Case 2a			✓	
Case 3			✓	
Case 4				✓
Case 5				✓



Grid Overview (2/2)

- Mixed element surface and volume grid
- Surface grid made of quadrilaterals and triangles
- Volume grid included tetrahedron, pyramids, prisms, and hexahedron



Surface

Red: quadrilaterals and triangles

Volume

Gray: tetrahedron

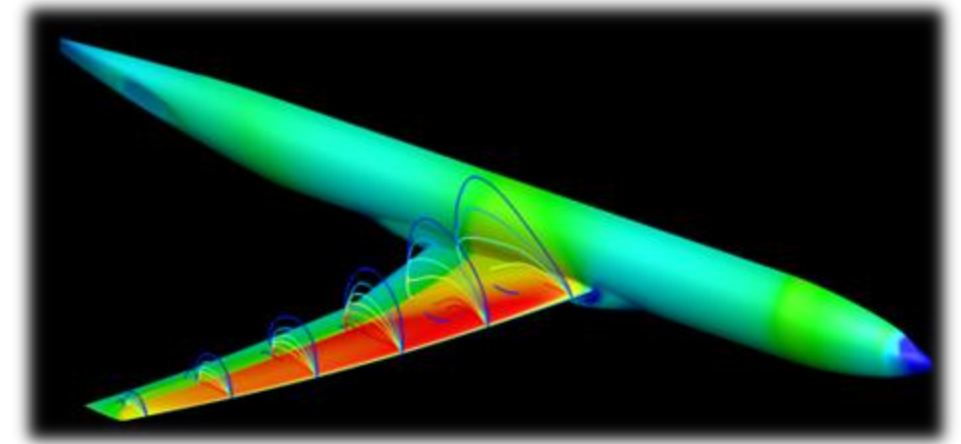
Gold: pyramids

Green: prisms

Brown: hexahedron

Solution Setup

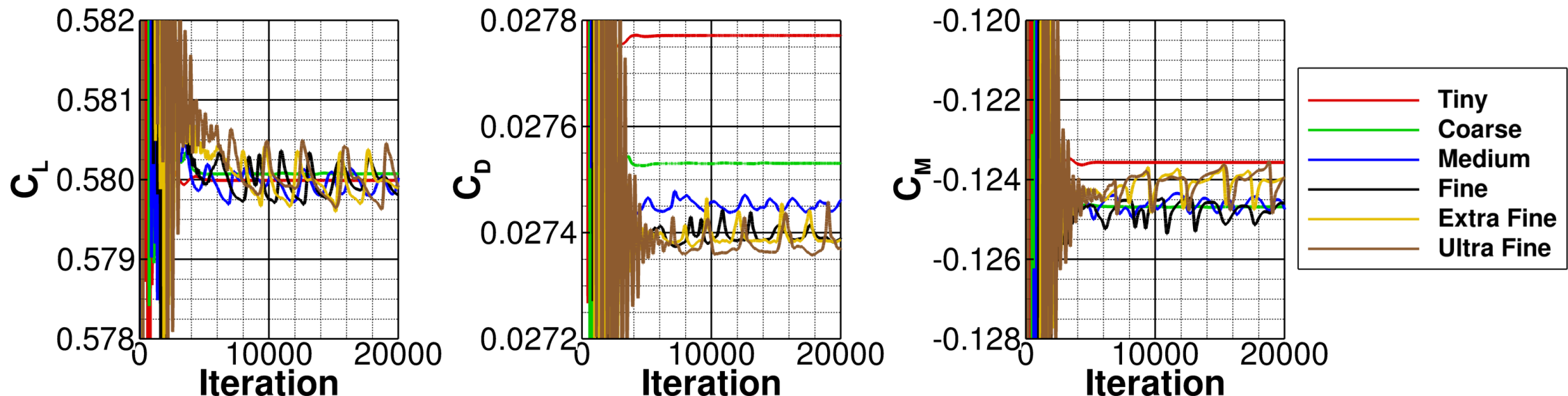
- **Computational approach**
 - HLLC++ inviscid flux and LDD+ viscous flux
 - Second-order spatial and temporal accuracy
 - Temporal damping applied to inner and outer grid
 - Fully-turbulent SARC-QCR (QCR2000)
- **KCFD (inner solver) and SAMAir (outer solver)**
- **Executed all RANS cases to 20,000 iterations, regardless of convergence behavior**
- **Appreciation extended to the Committee for accelerating development of the reduction scripts and data file format**



Case 1a: Unstructured Grid Convergence

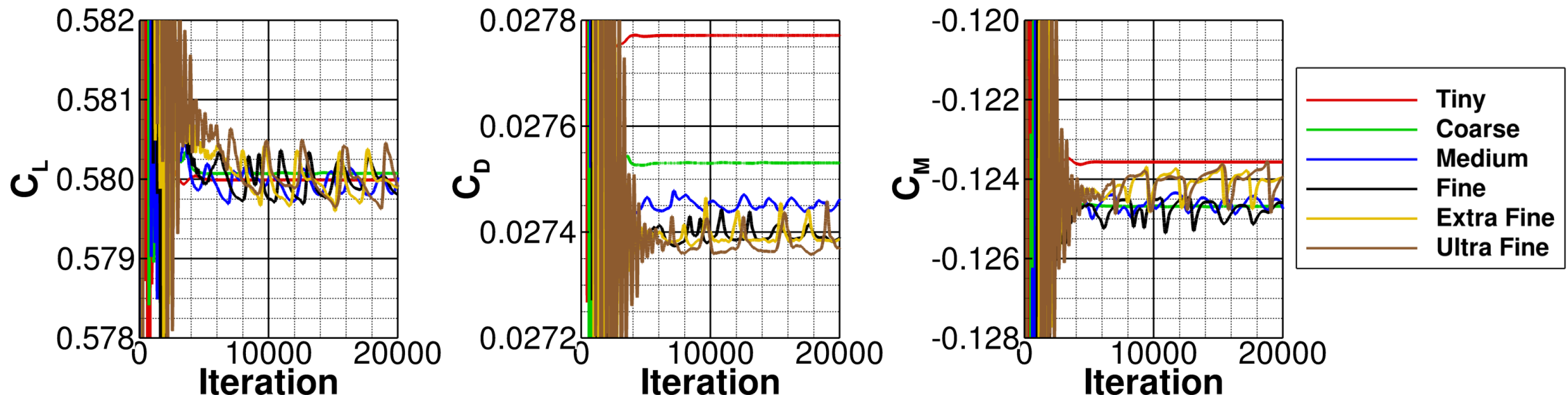
Mach 0.85
Re = 20 million
 $C_L = 0.58$

- Simulations executed on all six densities
- Data averaged over last 2,000 iterations
 - From user's best practices; may need more analysis
 - More stable grid convergence for coarser grids
 - Variations in C_L consistent with typical Kestrel results



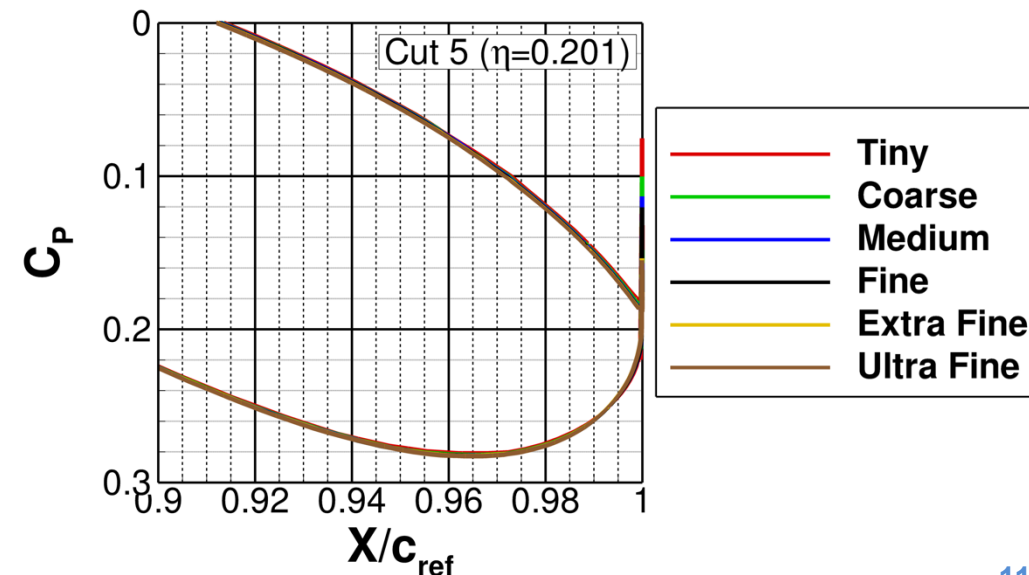
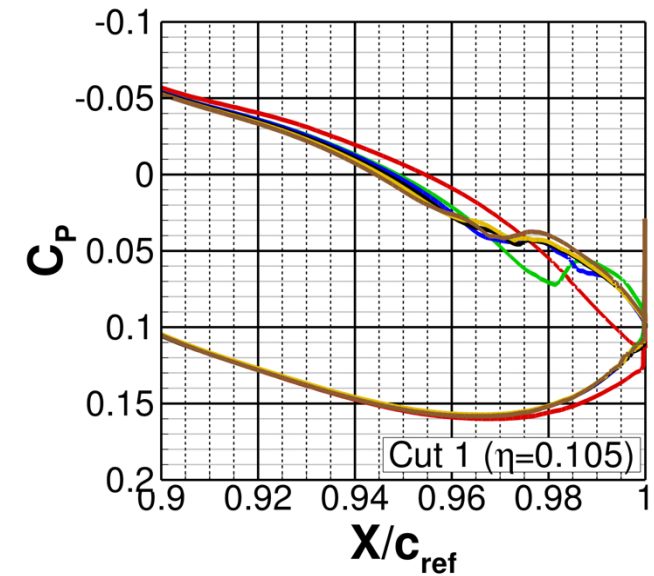
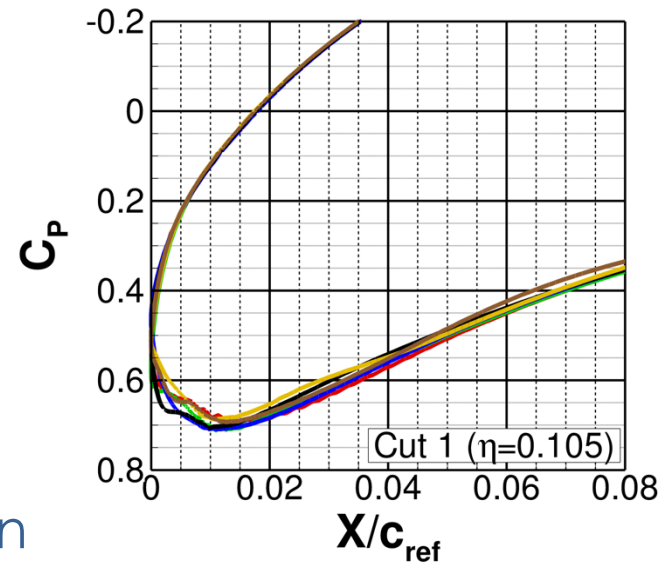
Case 1a: Unstructured Grid Convergence

- Simulations executed on all six densities
- Data averaged over last 2,000 iterations
 - From user's best practices; may need more analysis
 - More stable grid convergence for coarser grids
 - Variations in C_L consistent with typical Kestrel results
- Excellent grid convergence with increasing density



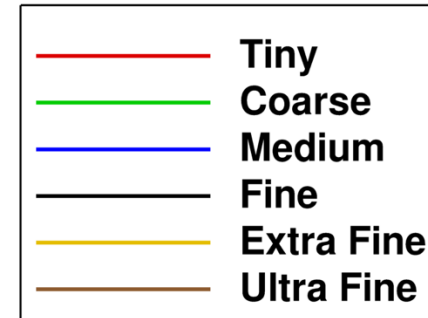
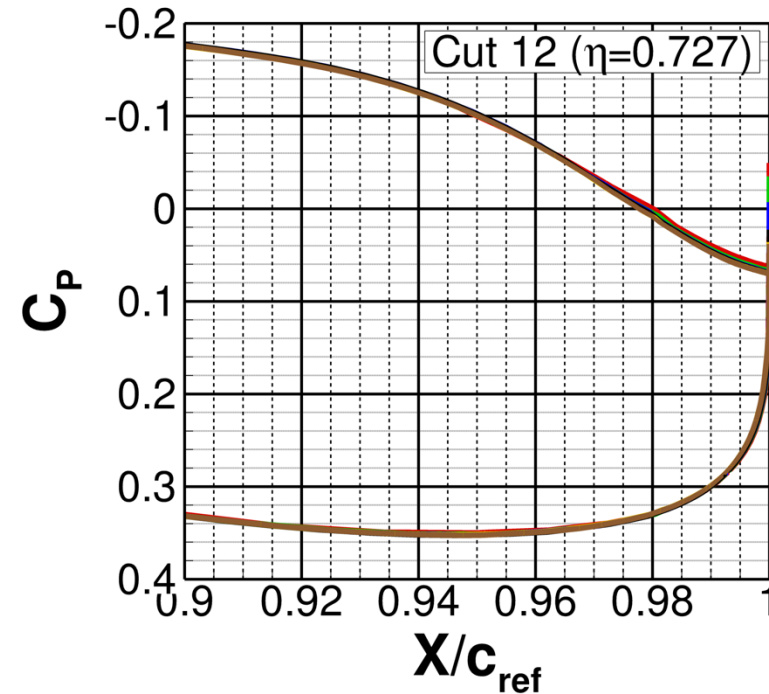
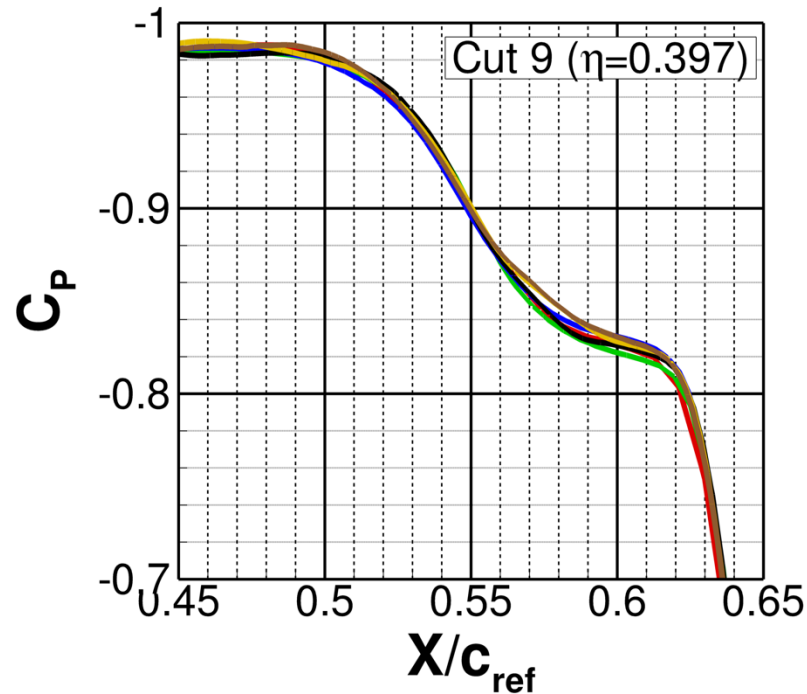
Case 1a: Inboard Pressure Cuts

- Only minimal differences seen in inboard-most C_p cuts
- Largest differences seen at inboard cut trailing edge
 - Region of interest for SOB separation region
 - Grid density has a large effect on the junction flow
- Moderate deviations near the leading edge lower surface
- Decreased differences outside of junction flow region (Cut 5 plotted)



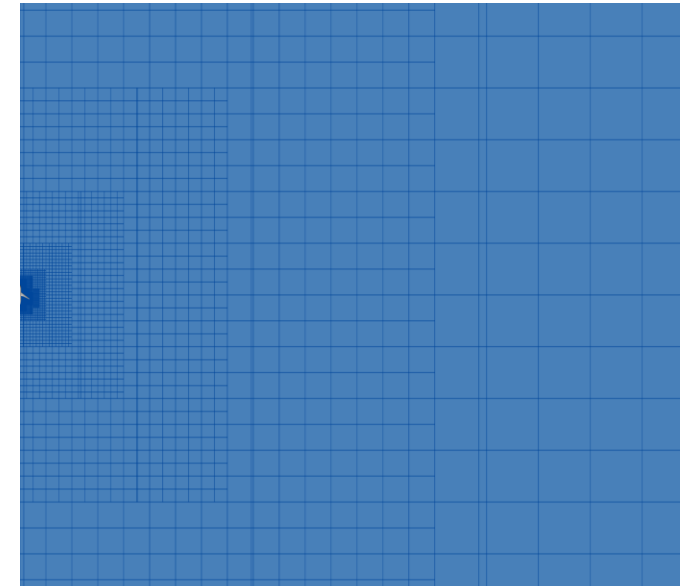
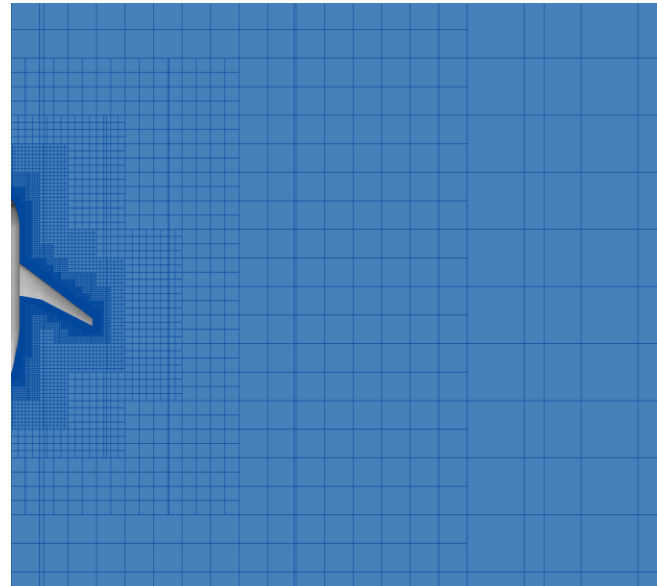
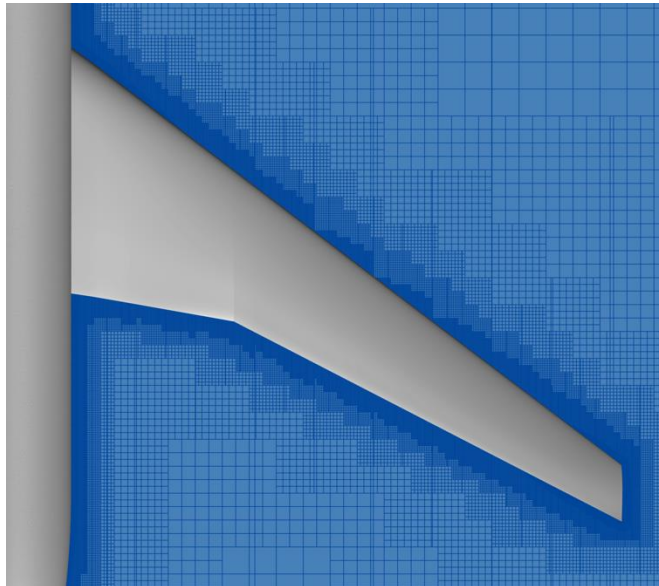
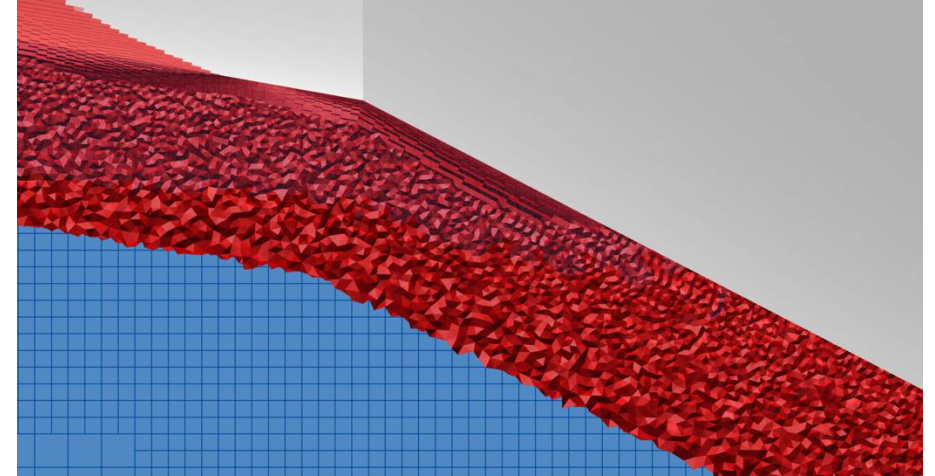
Case 1a: Midspan and Outboard Pressure Cuts

- Few differences seen in shock strength or location for the midspan and outboard locations (Cuts 9 and 12 representative of all results)
- Minimal variations seen in trailing edge behavior (Cut 12 is representative)



Case 1a: Overset Computational Domain

- Inner-most Cartesian cell size of outer unstructured cell (best practice)
- Outer box extends $\sim 110 c_{\text{ref}}$ in all directions
- Cartesian growth rate automatically determined

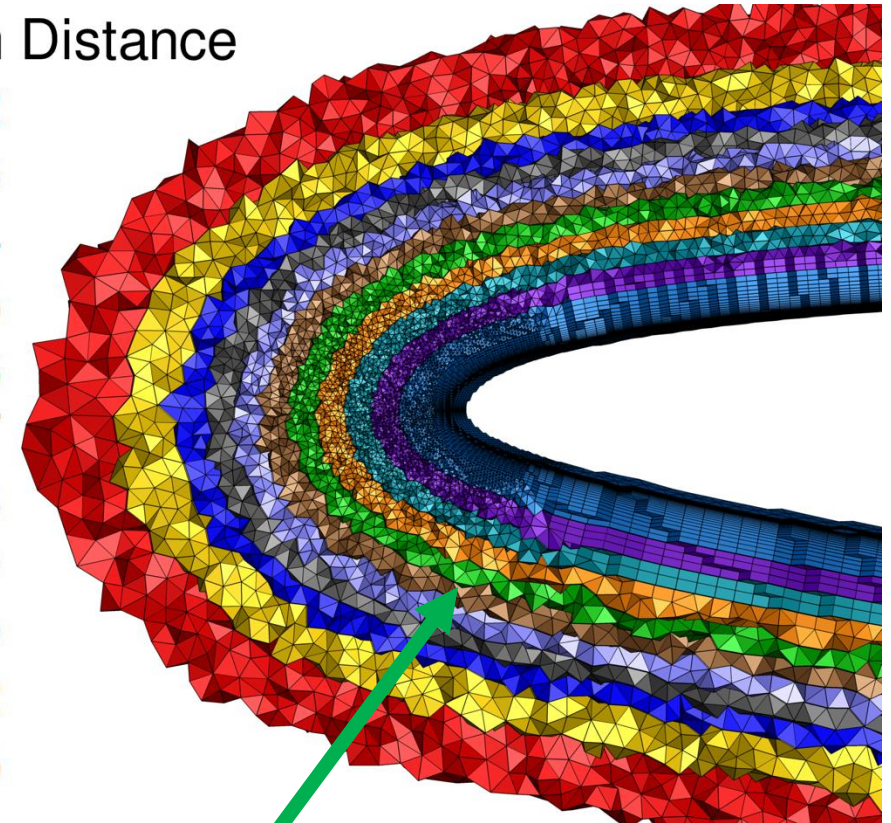


Case 1a: Trim Distance Study

- **Nearbody grids trimmed using carp**
 - Kestrel's grid manipulation package
 - Supports numerous grid formats (including ugrid)
 - Inner grid trimmed at a range of distances
- **Simulations were executed at constant α (2.758 deg.) with minimal difference in drag or convergence**

Trim Distance

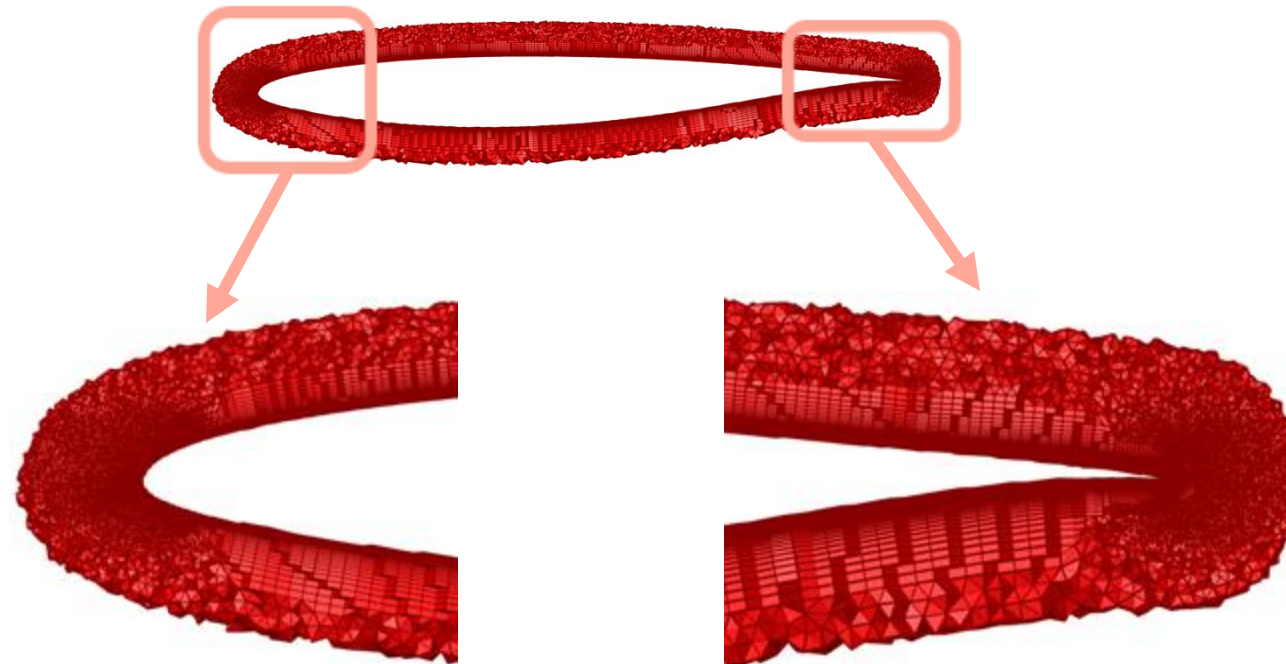
0.02
0.03
0.04
0.05
0.06
0.07
0.08
0.09
0.10
0.12
0.15



Selected trim
distance (0.06)

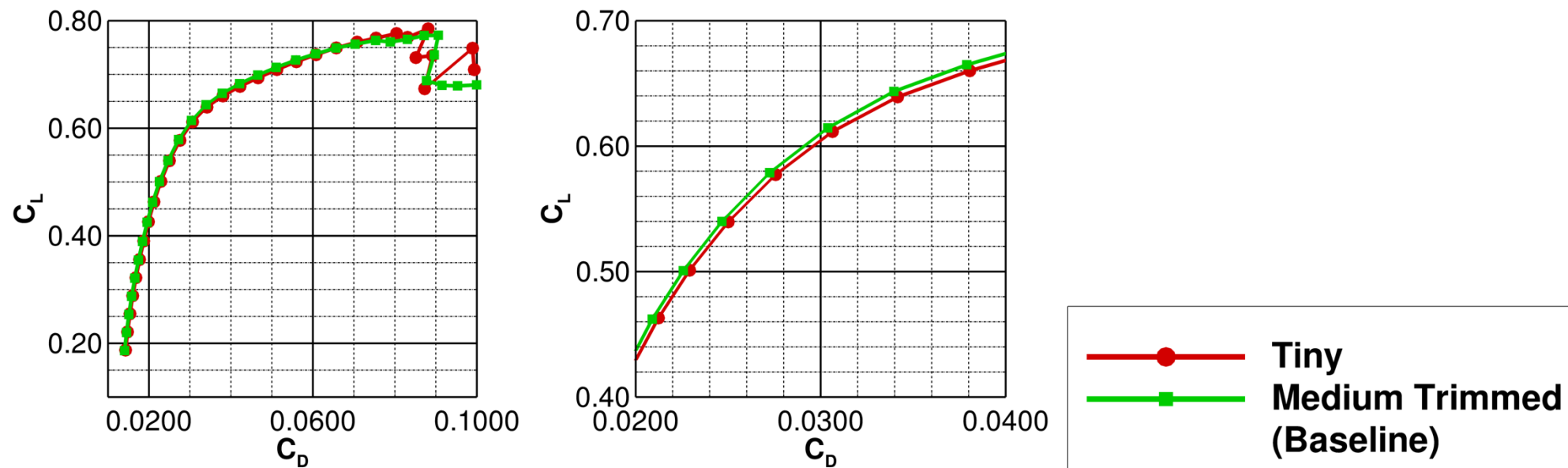
Case 1a: Trimmed Grid Visualization

- Selected 0.06
- Close trim distance can lead to erroneous results and solution instability
- Largely isotropic cell spacing at selected distance
- Trim distance held constant for subsequent solutions



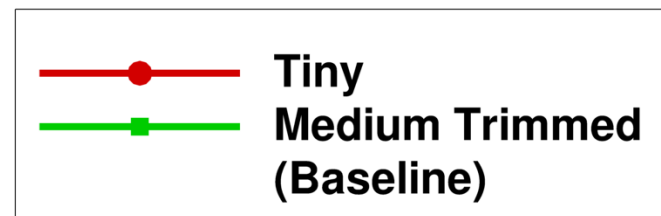
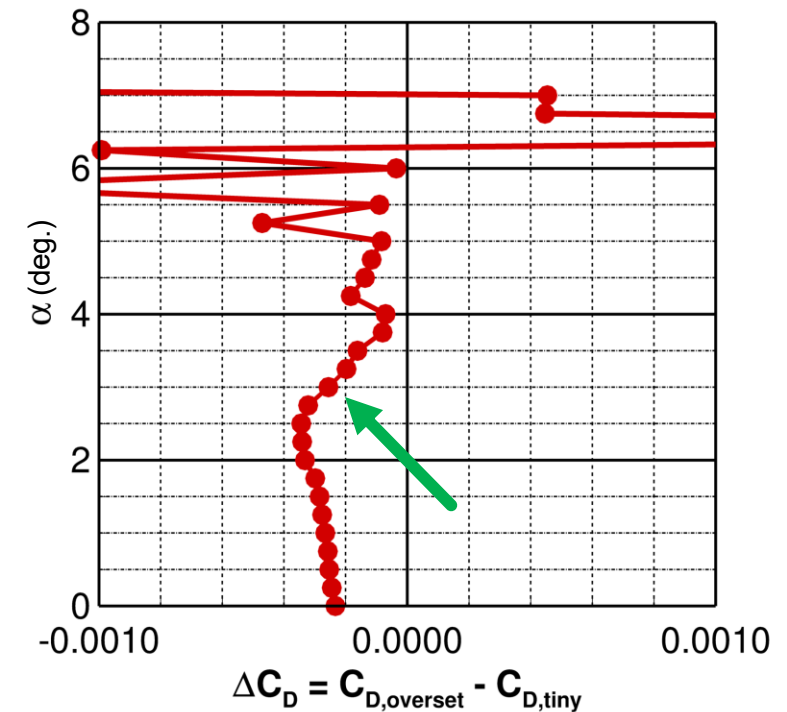
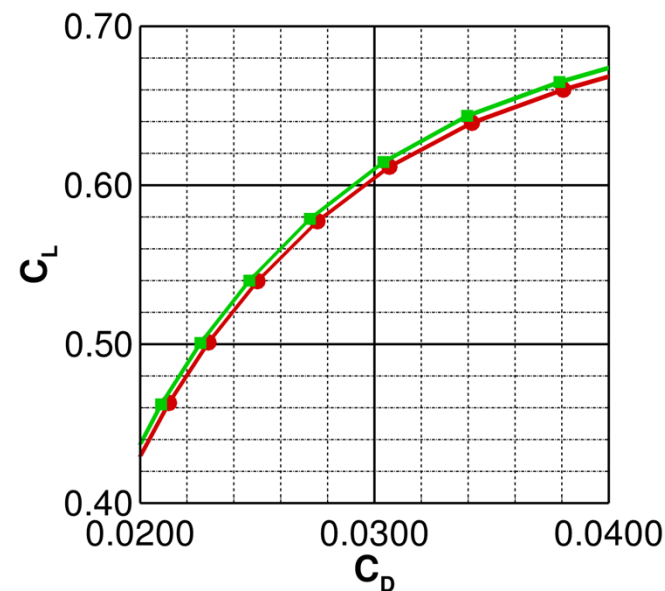
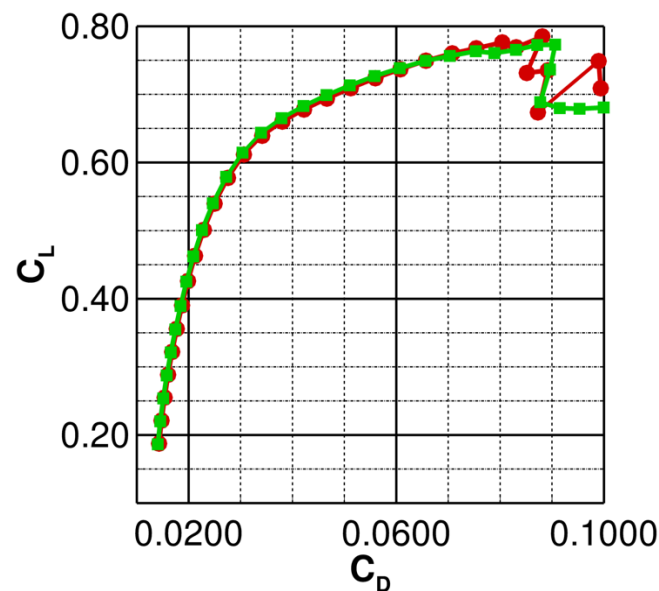
Case 1a: Aerodynamic Performance

- **Alpha sweep executed on tiny and medium/trimmed (baseline) grids**
 - Sweep from α of 0 to 8 deg. shown every 0.25 deg. (total of 86 jobs)
 - Tiny grid yields decreased α_{pitchup} and deeper C_M bucket (not shown)
- **Difference in inboard flow separation ~ 0.50 deg.**
- **Deviations observed in deep stall region**



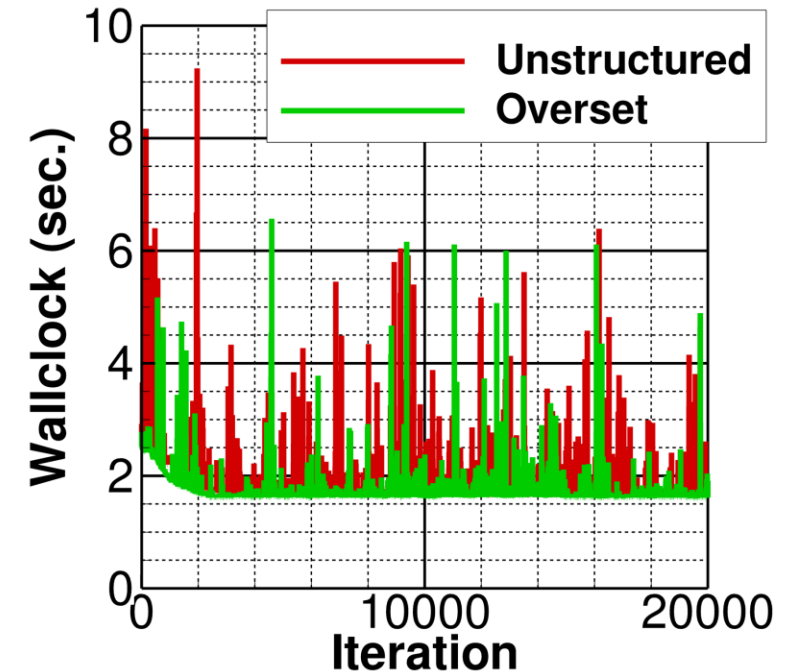
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- **Difference in inboard flow separation ~ 0.50 deg.**
- **Deviations observed in deep stall region**
- **C_D differences ~ 2.2 counts at α of 3.00 deg.**



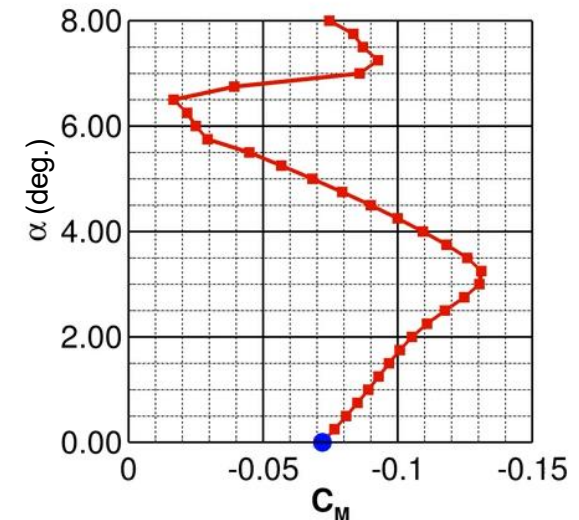
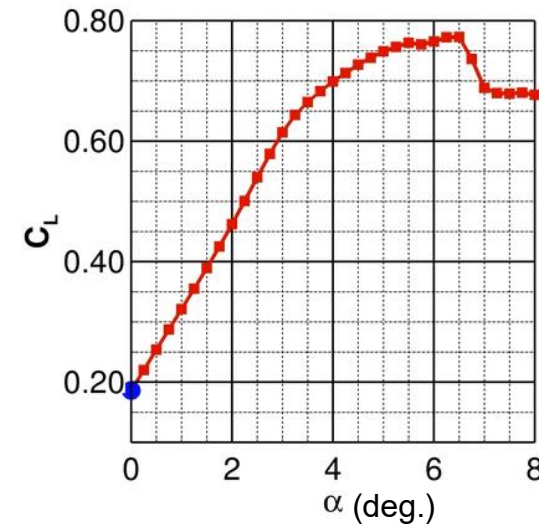
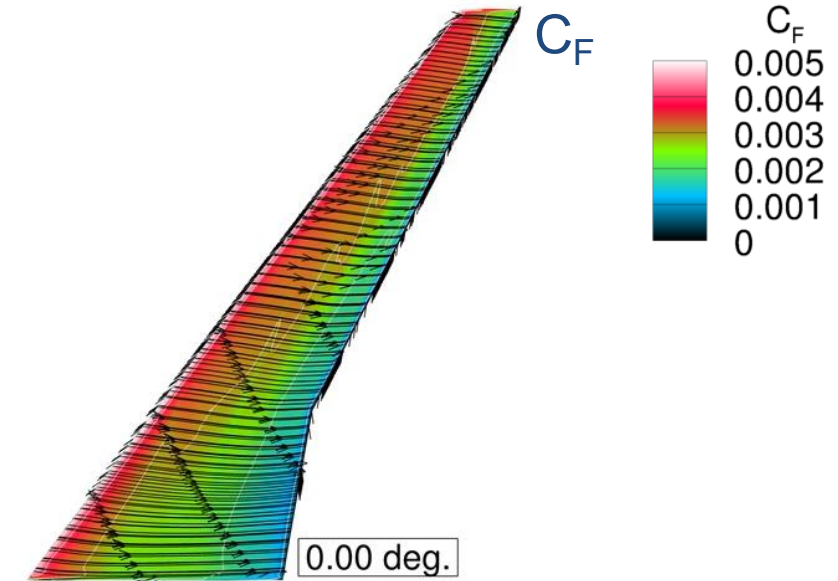
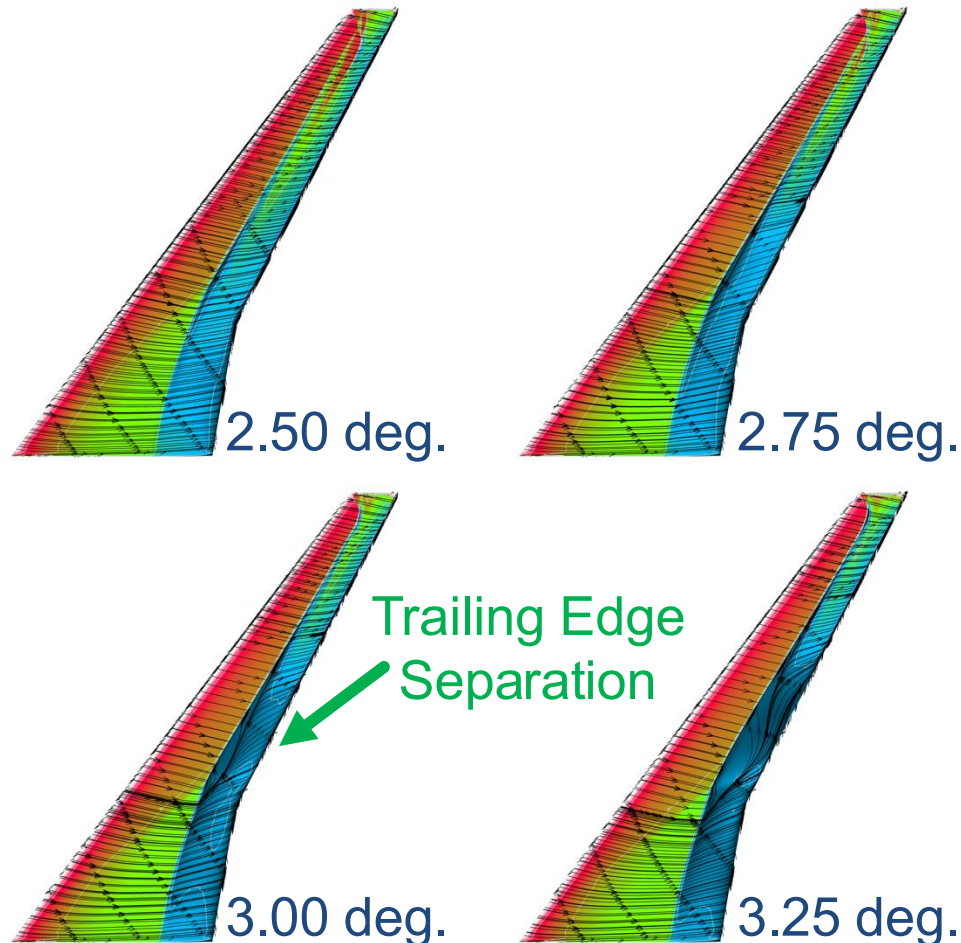
Case 1a: Computational Cost

- **Total cost for medium-density mesh**
 - Fully unstructured grid
 - Trimmed grid at 0.06
- **1600 CPUs (40 Skylake nodes)**
- **About 10.5 hours total for overset formulation**
- **Cost per iteration is primarily between 2 and 4 sec. (without refinement)**
- **Overset solution yields ~50% reduction in computational cost relative to unstructured**



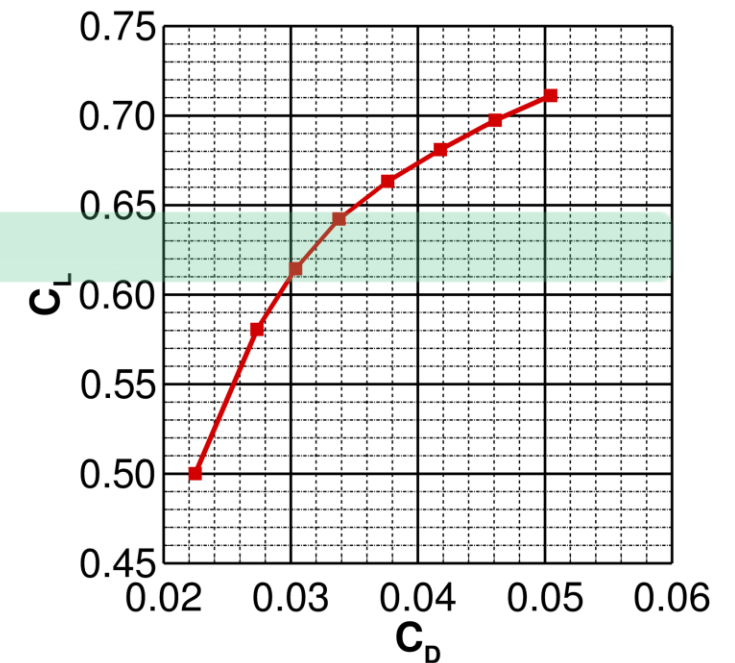
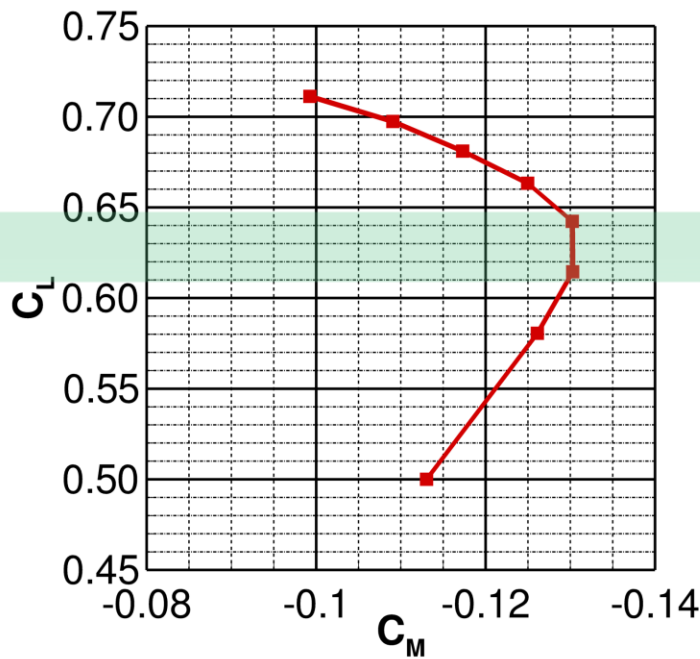
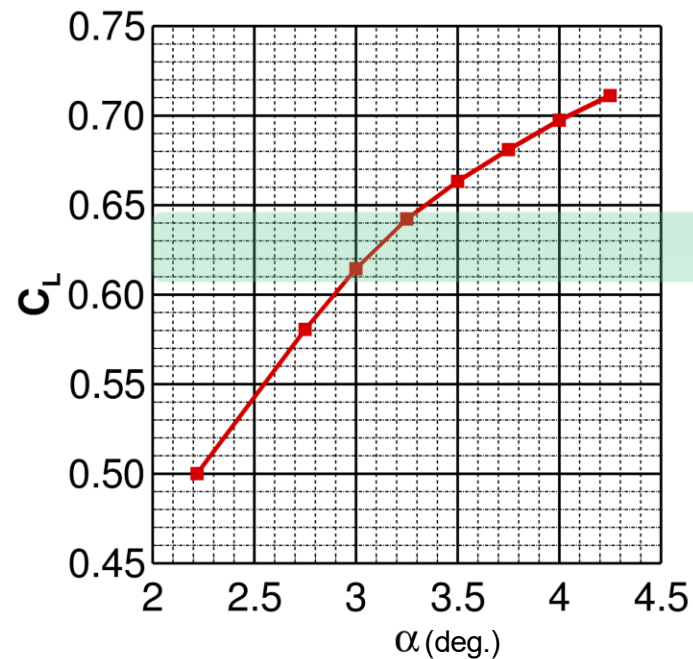
Case 1a: Medium Trimmed Grid Alpha Sweep

- Pitch break at ~3.0 deg. ($C_L \sim 0.62$)
- Inboard wing separation at ~7.25 deg.



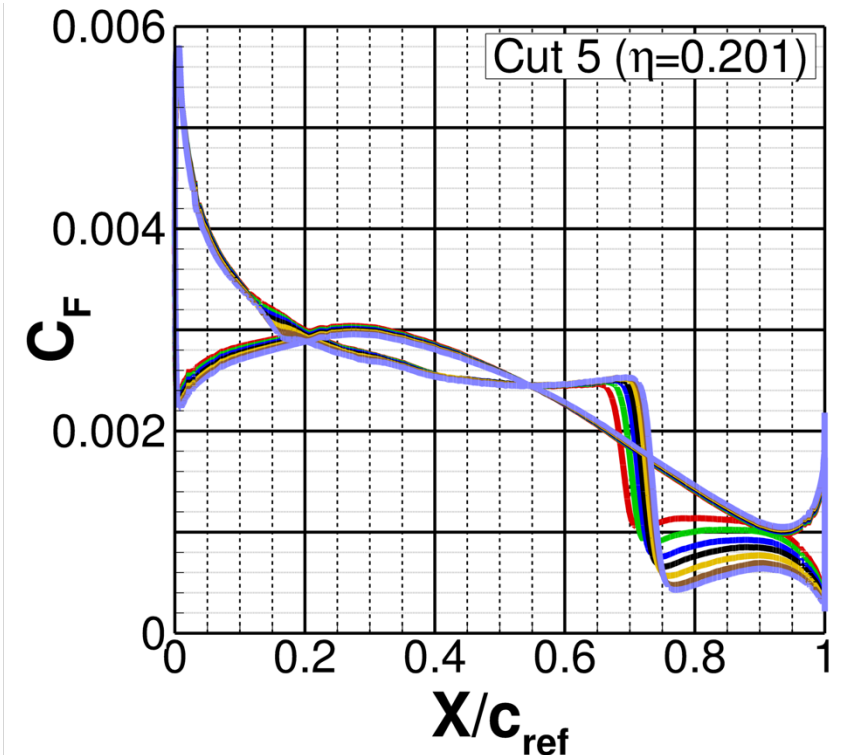
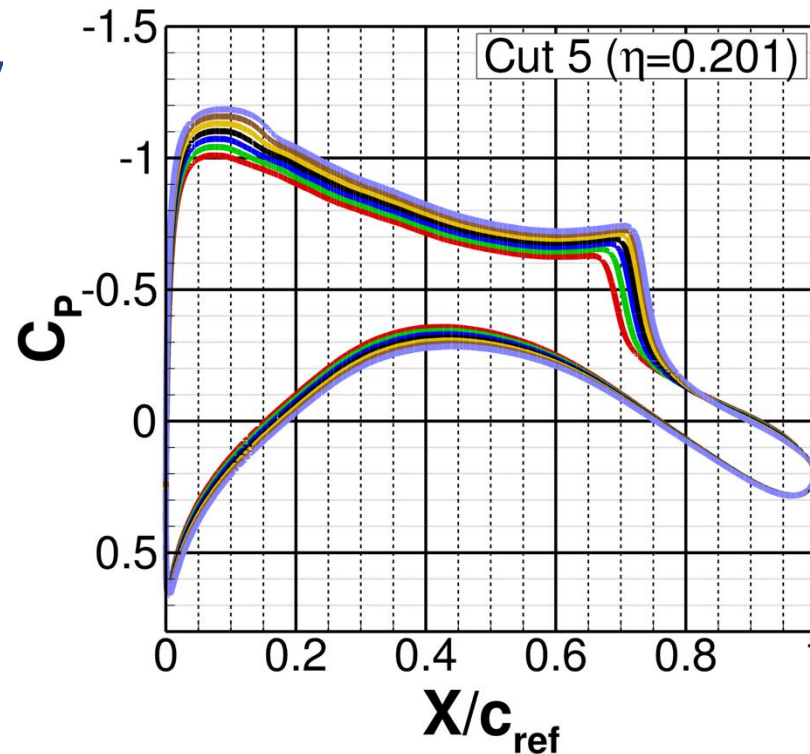
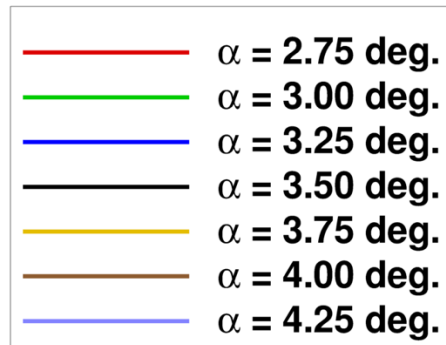
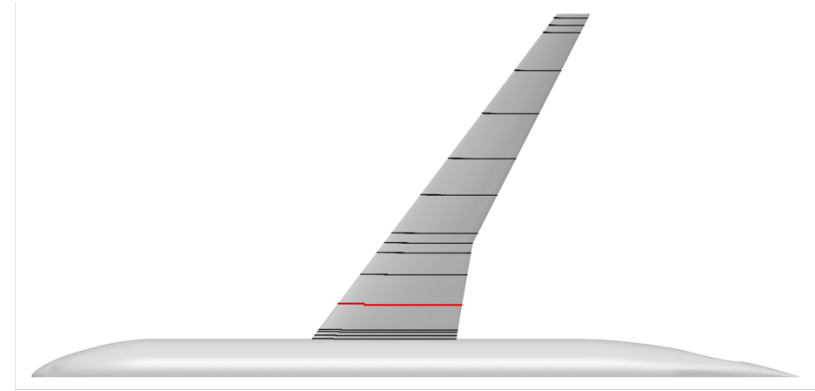
Case 2a: Polar

- Executed with medium grid and appropriate aeroelastic deformations
- Increasing flow separation observed for $\alpha > \sim 3.0$ deg.
- Progressive decambering leads to monotonically-decreasing $C_{L\alpha}$ slope
- Pitching moment break observed near $C_L \sim 0.62$



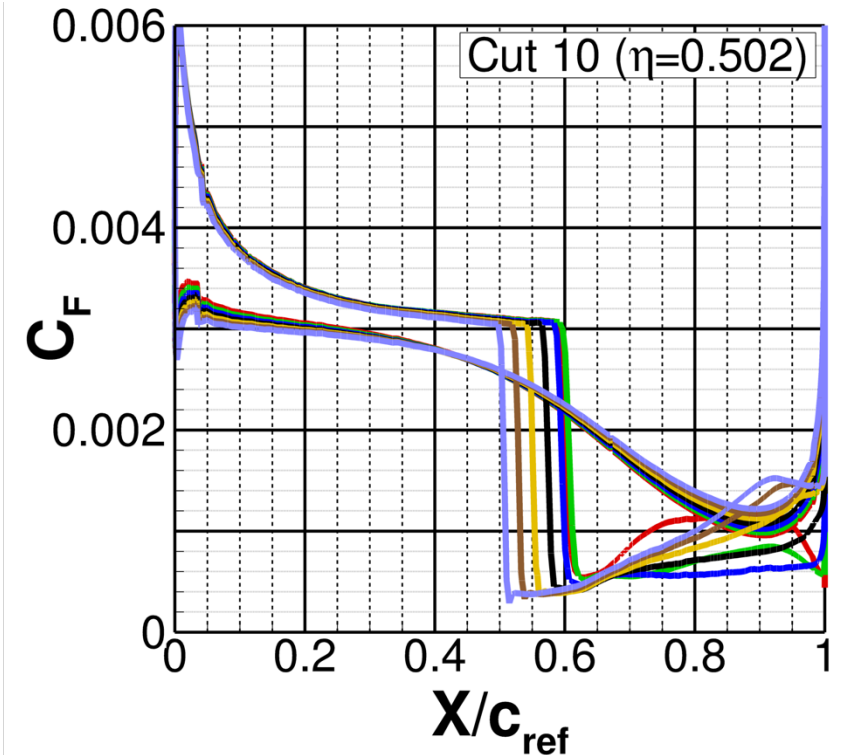
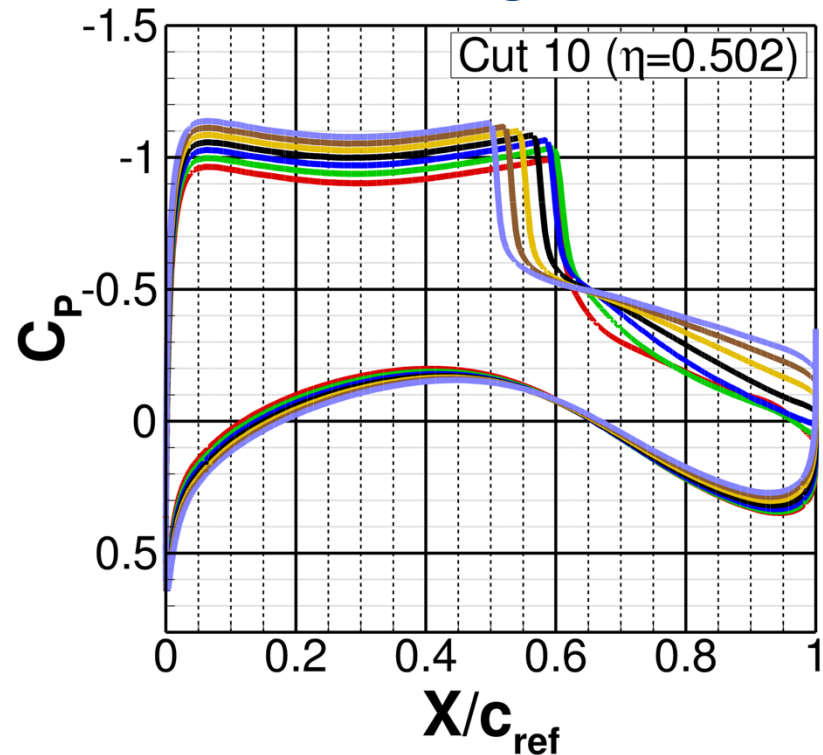
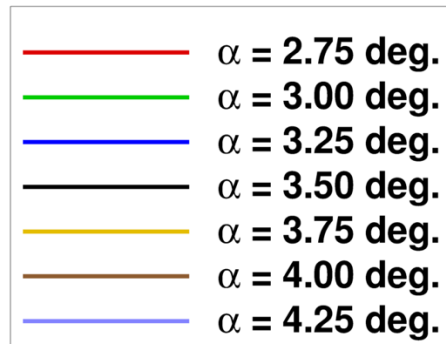
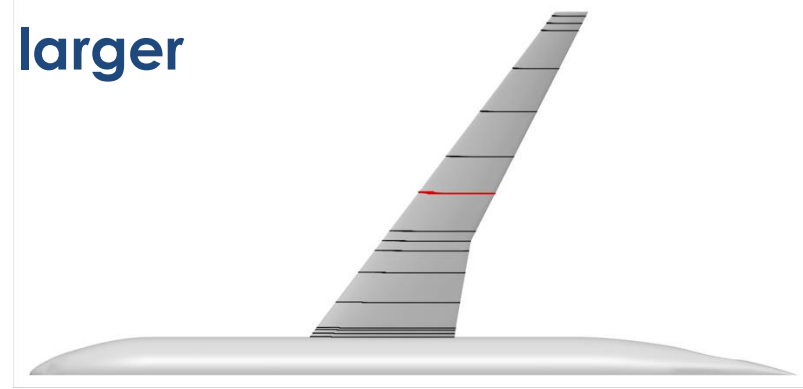
Case 2a: Inboard Surface Cuts

- Increasing angle of attack yields a downstream shift in shock location
- Shock clearly evidenced by C_p and C_f
- Flow nominally attached downstream of the shock
- Decelerated flow seen at trailing edge



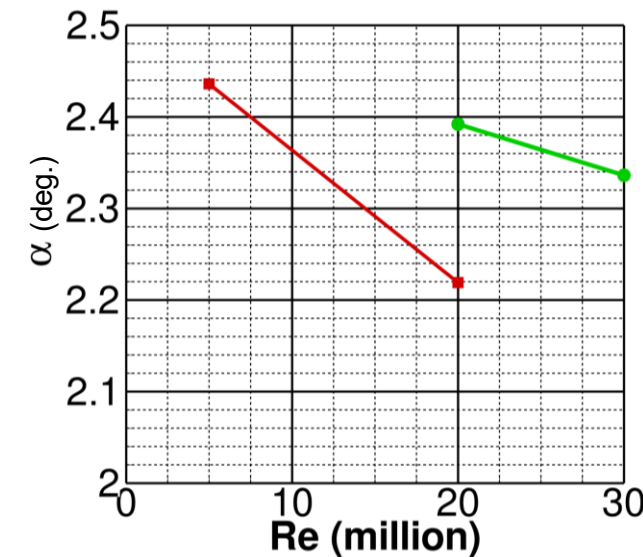
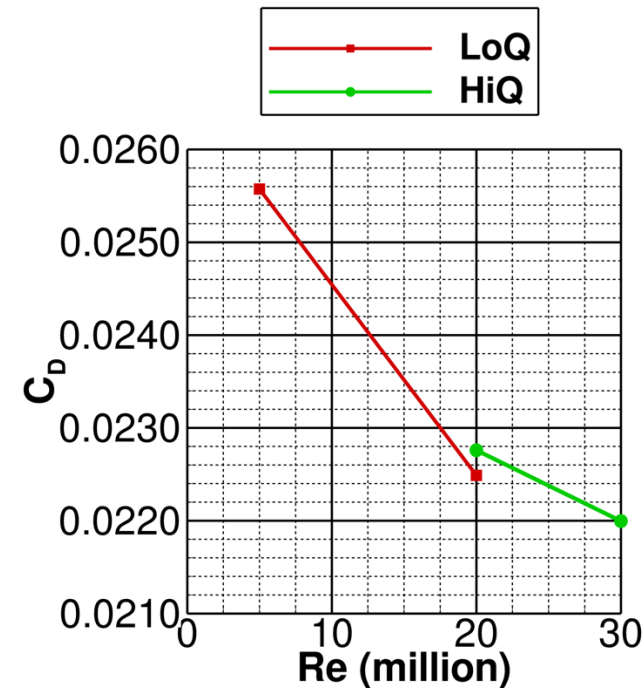
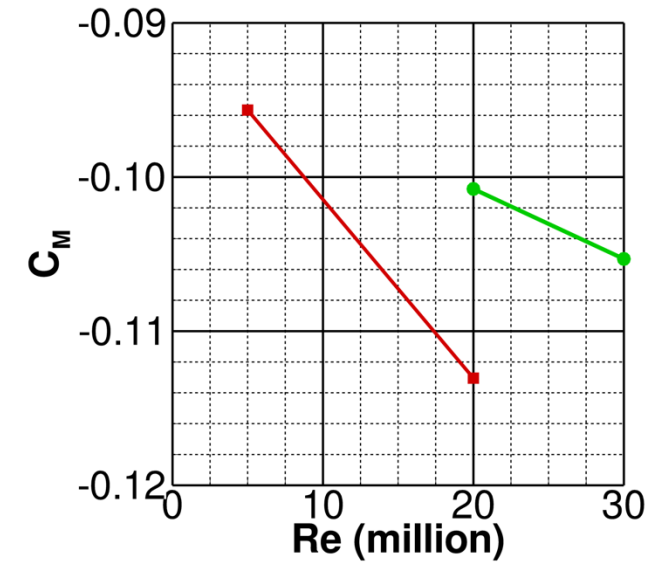
Case 2a: Mid-Span Surface Cuts

- Downstream shift in shock observed with larger angles of attack (expected)
- No double shocking at high angles
- Flow separates at shock location and fails to reattach above $\alpha = 3.25$ deg.



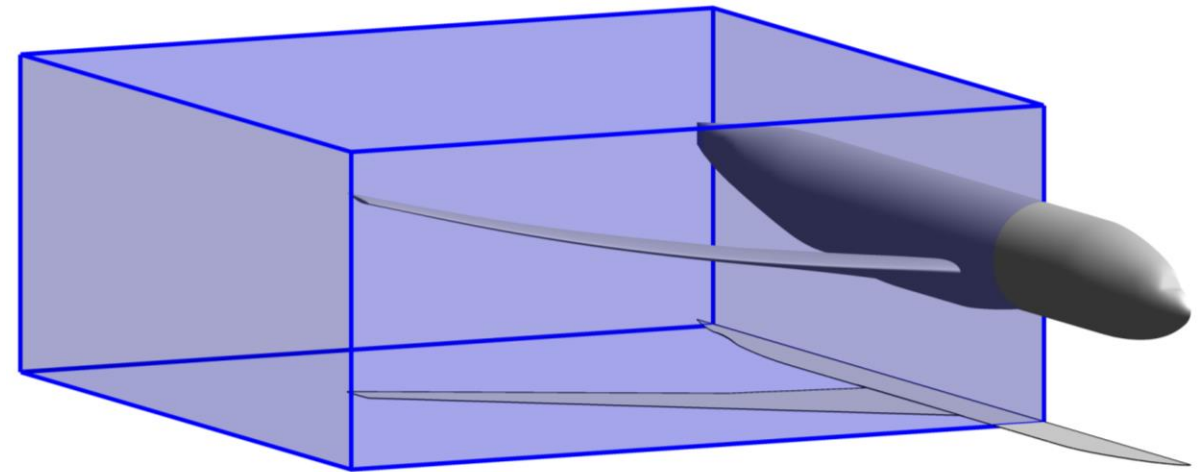
Case 3: Reynolds Number Sweep

- Executed on LoQ and HiQ lofts at $C_L = 0.50$
- Significant drag rise with decreased Re (expected)
- Large drag rise seen from Re of 20 million to 5 million (expected)



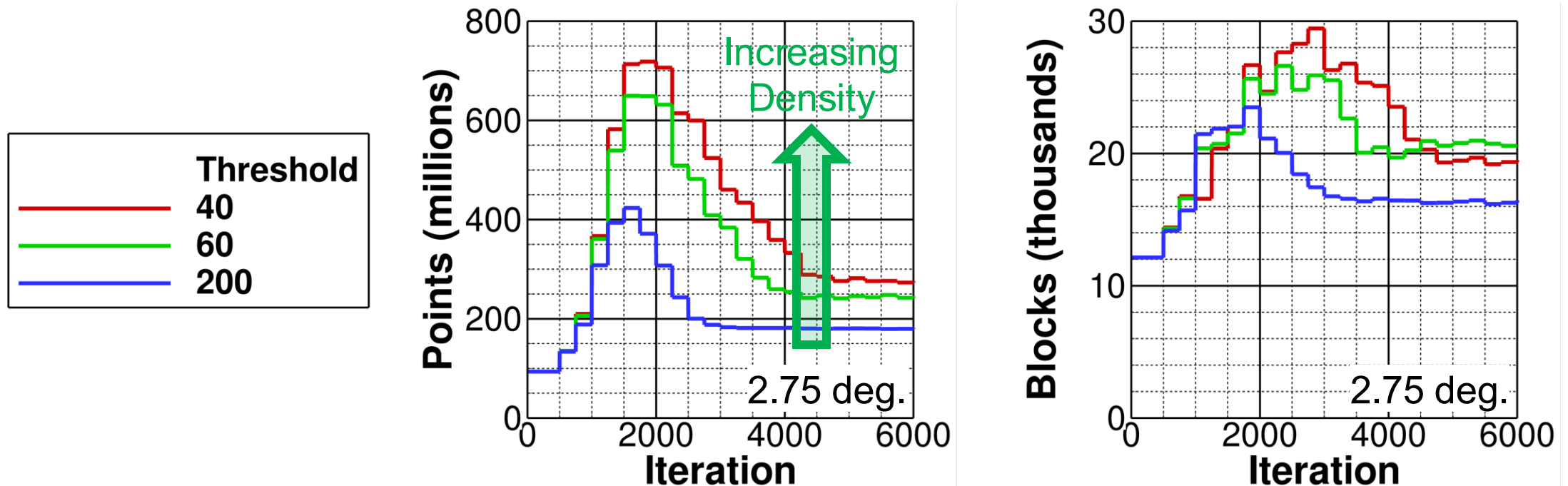
Case 4: RANS Adaptive Mesh

- **Adaptive mesh refinement performed in offbody Cartesian grid**
 - Nearbody-grid adaptation not yet available
 - User-specified region limits shown in blue box
 - Amount of refinement based upon a threshold value
 - Separated wake led to decision to refine based on ω
- **Refinement applied every 250 iterations**
- **Adaptation used over the entire simulation (not frozen)**
- **Grid density must be traded with computational cost**



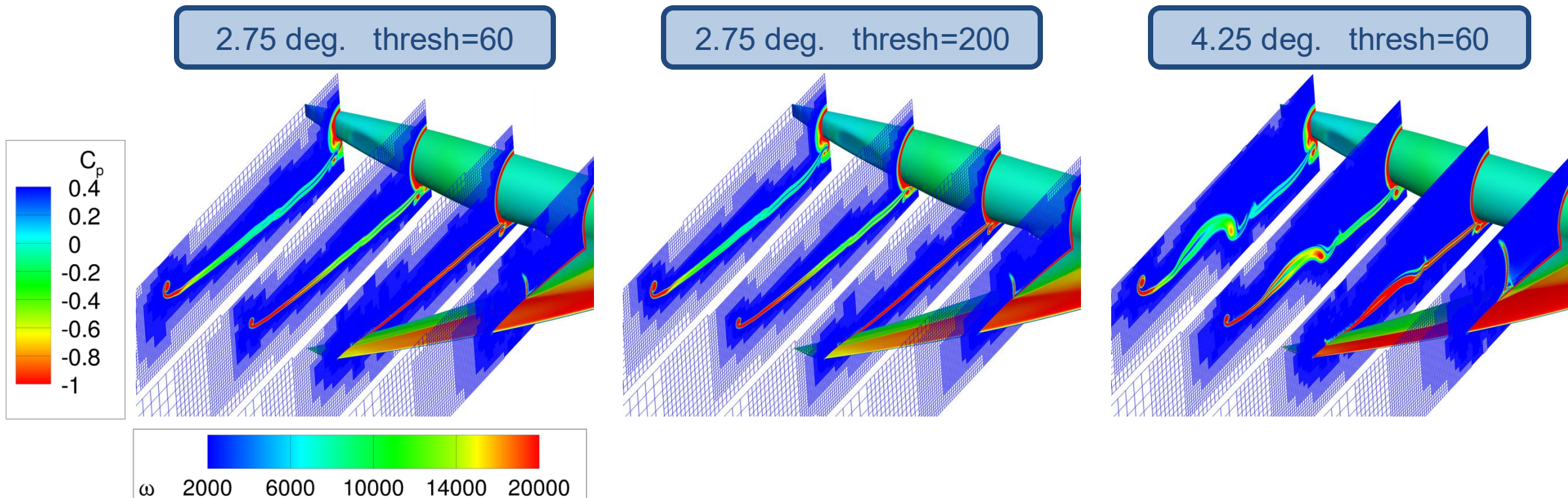
Case 4: Effect of Refinement Threshold (1/3)

- **Threshold value controls degree of grid refinement based on values of ω**
 - Decreased threshold yields increased grid density
 - Cases run at threshold values from 40 through 200 (12 jobs total)
 - Executed for 6,000 iterations – sufficient to understand grid resolution
 - Cartesian grid convergence observed after 5,000 iterations
- **Analysis performed at $\alpha = 2.75$ deg. (plotted) and 4.25 deg.**



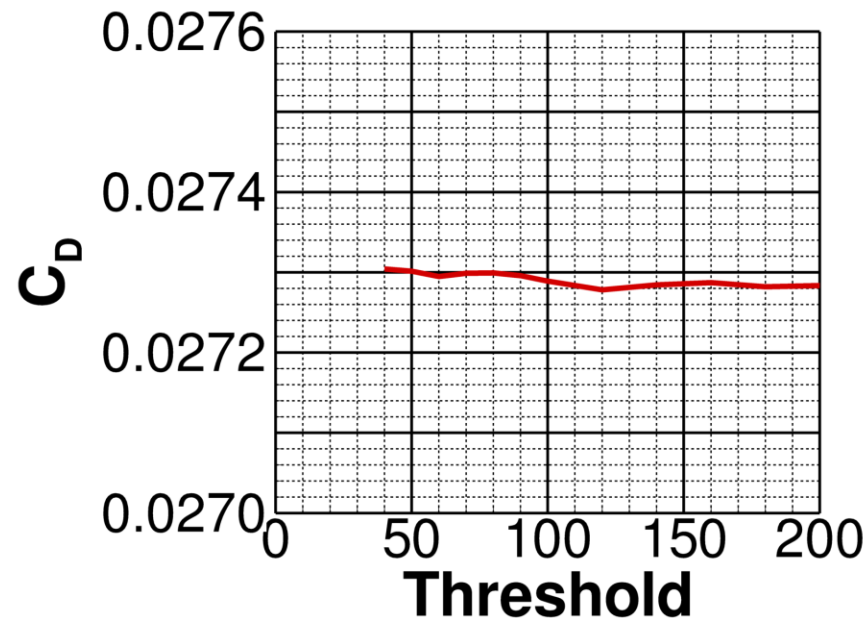
Case 4: Effect of Refinement Threshold (2/3)

- Selection of threshold significantly affects wake refinement
- Chose threshold value of 60 with ~280 million cells in Cartesian region
 - Minimal grid changes at $\alpha = 2.75$ deg.
 - Adequately captures wing tip vortex, mid-span separation, and fuselage vortex



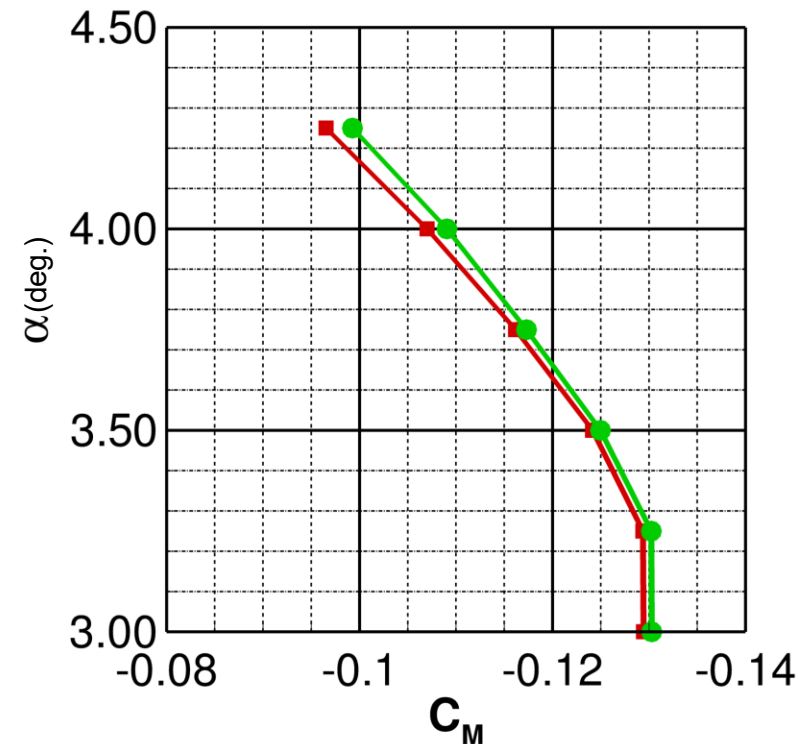
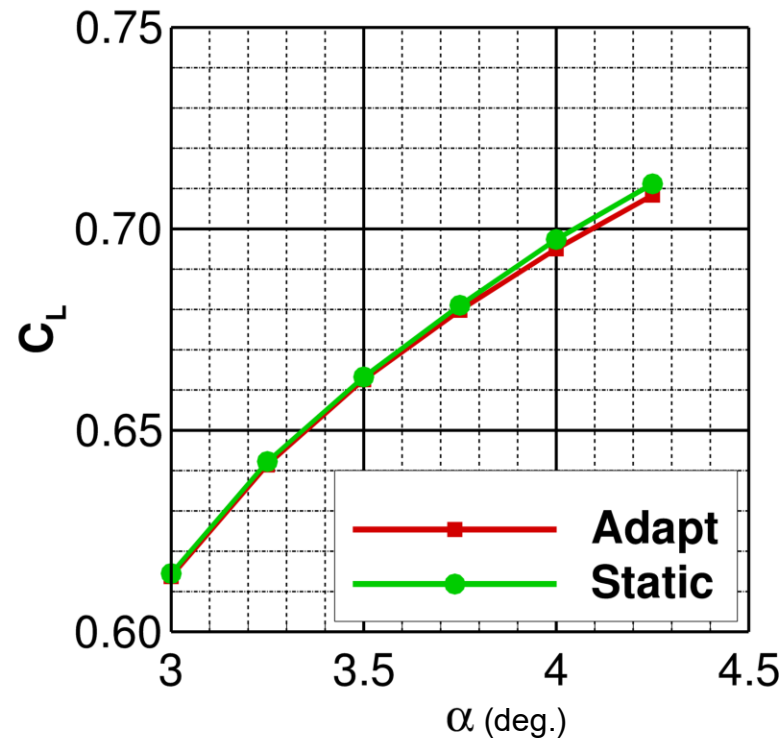
Case 4: Effect of Refinement Threshold (3/3)

- Range of thresholds analyzed at C_L of 0.58
- Threshold value has minimal effect on F&M at this condition
 - Consistent with expected results
 - Improved resolution of the wake and the shock
- **This observation does not mean that refinement has no effect on the global F&M (covered in next slides)**



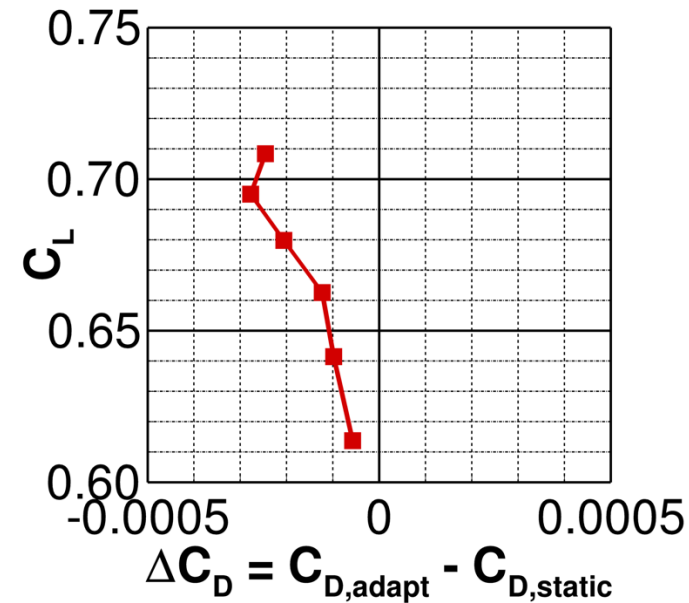
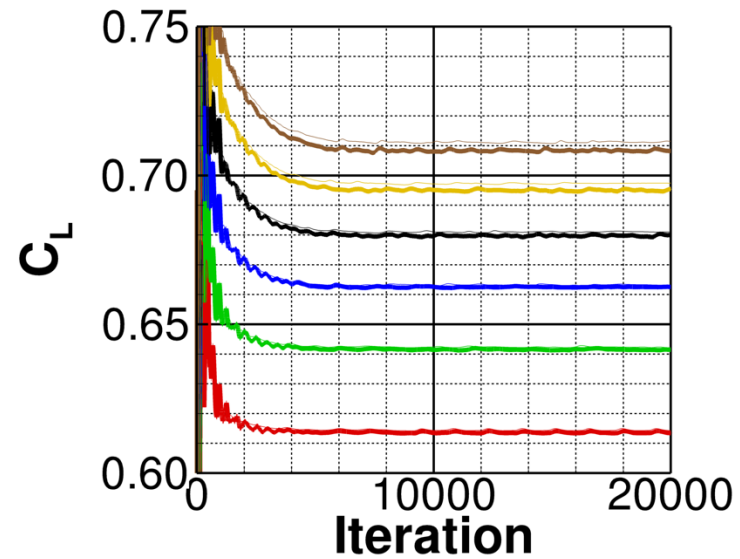
Case 4: Aerodynamic Performance

- Adapted grid yields only a slight reduction in lift and moment magnitude
- Pitch-up break point extremely similar for both formulations
- Observations consistent with typical Kestrel behavior



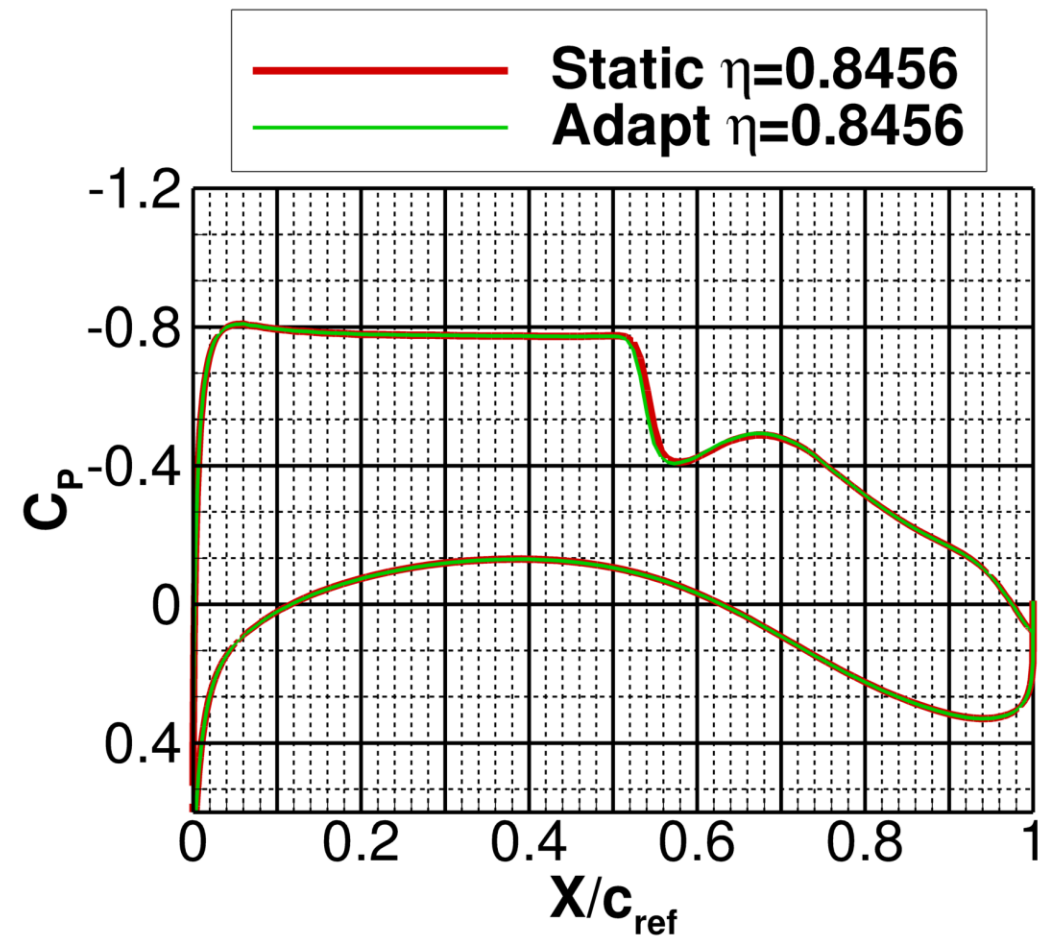
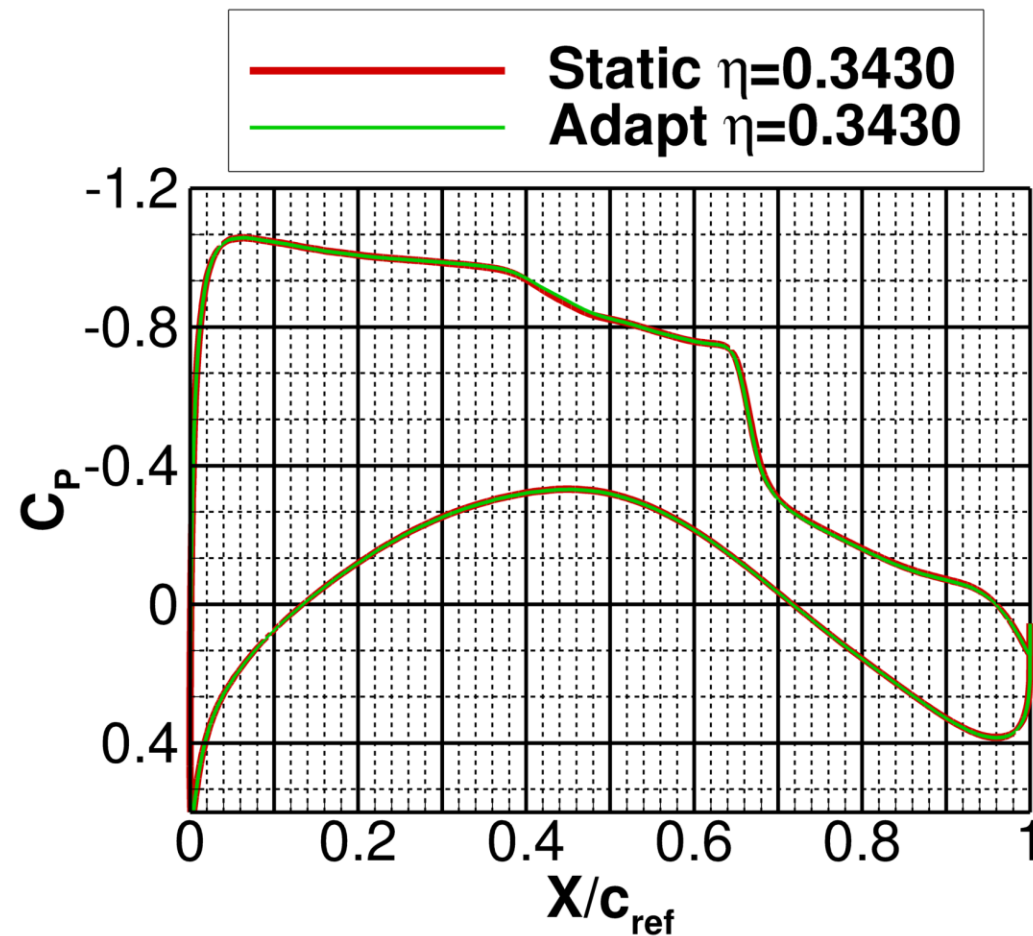
Case 4: Convergence History

- Similar convergence history across full range
- Differences in averaged values
 - Grid-adapted solutions yield decreased drag
 - $C_L \sim 0.001$
 - Maximum C_D delta ~ 3 counts



Case 4: Pressure Cuts (C_L 0.58)

- Overall, minimal changes observed in surface C_p data
- Slight forward movement of shock at outboard locations



Case 5: Beyond RANS (DDES Adaptive Mesh)

- **Similar setup to RANS cases**
 - Same refinement region and settings
 - SARC-QCR turbulence model
- **Averaging window**
 - Simulation run for 26,000 iterations (not 20,000)
 - Began averaging at 20,000 iterations
 - Averaged for 6,000 iterations (not 2,000)
- **Nondimensional time step set to 0.010, dimensional time step falls out**

$$\frac{V_{\infty} \times dt}{c_{ref}} = dt^*$$

$$dt = \frac{dt^* \times c_{ref}}{V_{\infty}}$$

$$dt = \frac{0.010 \times 1.0}{7239.725}$$

$$dt = 0.000001381$$

Case 5: Beyond RANS (DDES Adaptive Mesh)



Case 5: Opportunities for Investigation

- **A more thorough investigation is warranted**
- **Grid considerations**
 - Appropriateness of current grids for DDES need to be investigated
 - Possibility of modeled stress depletion should be analyzed
- **Computational settings**
 - Temporal damping may need to be considered
 - Examine impact of RC and QCR
 - Smaller time steps might be significant

Summary

- Analysis performed on Cases 1a, 2a, 3, 4, and 5
- Excellent unstructured grid convergence achieved
- Pitch break observed $C_L \sim 0.62$
- Offbody adaptive mesh refinement improved wake prediction, but minimal effect on integrated F&M
- Unsteady DDES yielded earlier separation than RANS

Questions?

