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# **Drag Prediction for the CRM model using the Edge solver**

by

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# Overview

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- Calculations with Edge solver
  - Hybrid unstructured grids
- Two families of grids computed
  - Provided by DLR, results delivered to DPW
  - In-house grids generated, not delivered yet
    - Grid generation delayed, results only just finalized
- Mandatory Case1
  - Grid convergence study
  - Downwash study

## Selected grids

- Two families of unstructured grids used, from DLR and FOI
- DLR grids generated with SOLAR grid generator

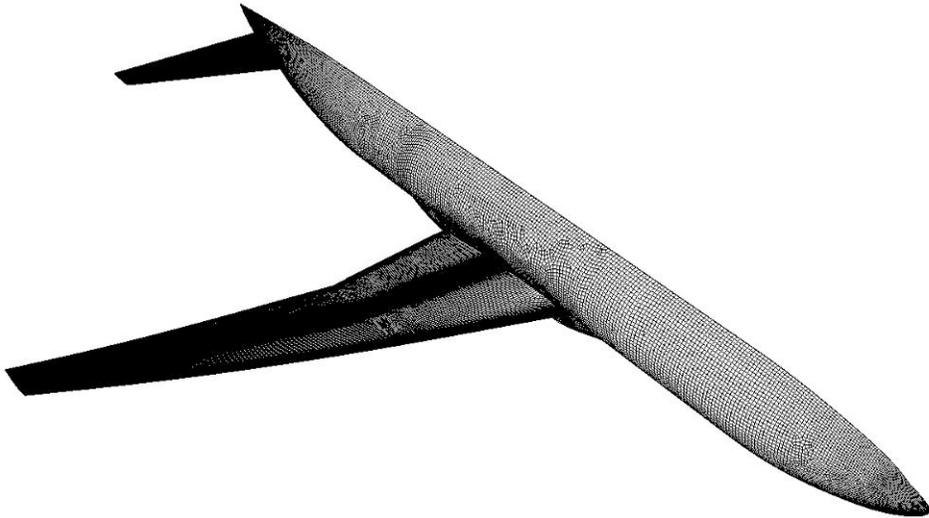
<b>DLR grids, tail 0</b>	<b>Coarse</b>	<b>Medium</b>	<b>Fine</b>
# nodes	$4.1 \times 10^6$	$11.7 \times 10^6$	$34.1 \times 10^6$
# boundary nodes	$108 \times 10^3$	$226 \times 10^3$	$470 \times 10^3$
# hexahedral elements	$3.1 \times 10^6$	$9.2 \times 10^6$	$72.7 \times 10^6$
# prisms	$1.8 \times 10^3$	$3.4 \times 10^3$	$3.4 \times 10^3$
# tetrahedral elements	$5.3 \times 10^6$	$14.3 \times 10^6$	$38.6 \times 10^6$

- FOI grid generated with in-house grid generator Tritet

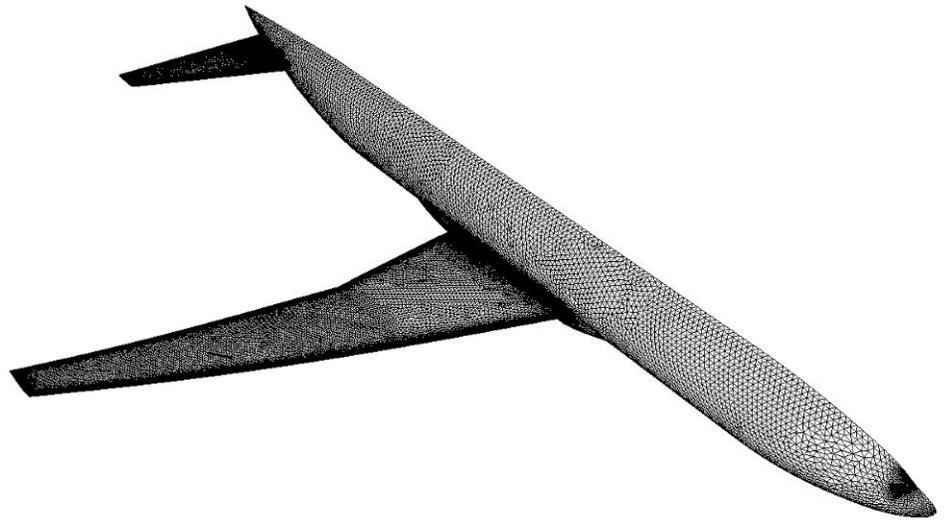
<b>FOI grids, tail 0</b>	<b>Coarse</b>	<b>Medium</b>	<b>Fine</b>
# nodes	$3.2 \times 10^6$	$10.1 \times 10^6$	$32.1 \times 10^6$
# boundary nodes	$153 \times 10^3$	$336 \times 10^3$	$734 \times 10^3$
# hexahedral elements	0	0	0
# prisms	$5.5 \times 10^6$	$18.3 \times 10^6$	$59.1 \times 10^6$
# tetrahedral elements	$1.7 \times 10^6$	$4.1 \times 10^6$	$10.9 \times 10^6$

# Grid pictures

DLR medium grid, tail 0

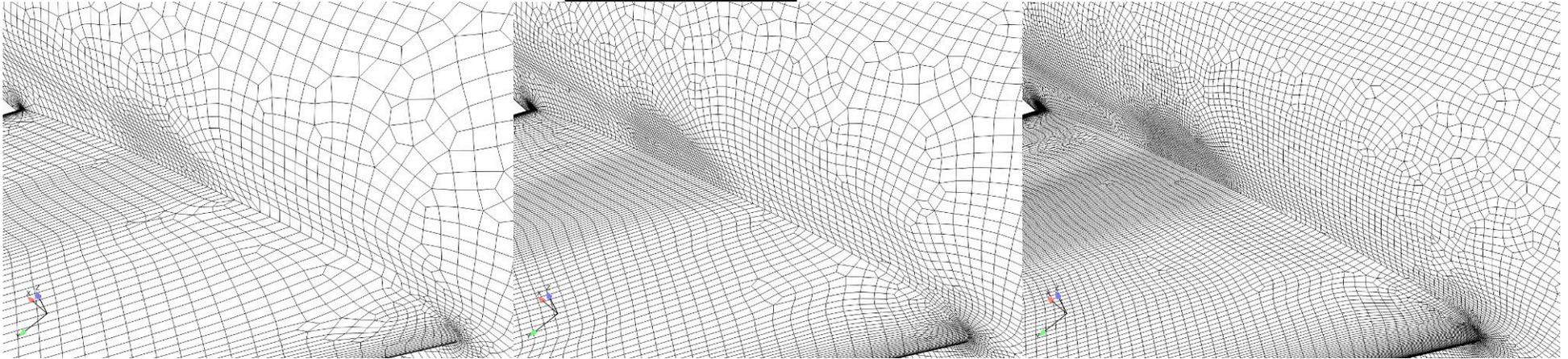


FOI medium grid, tail 0

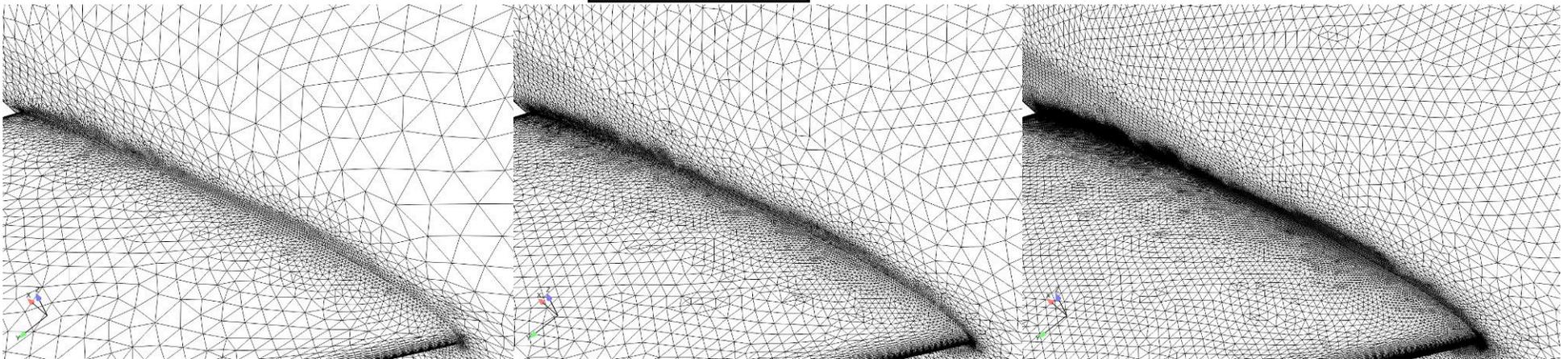


# Grid pictures, WB junction

DLR grids, tail 0

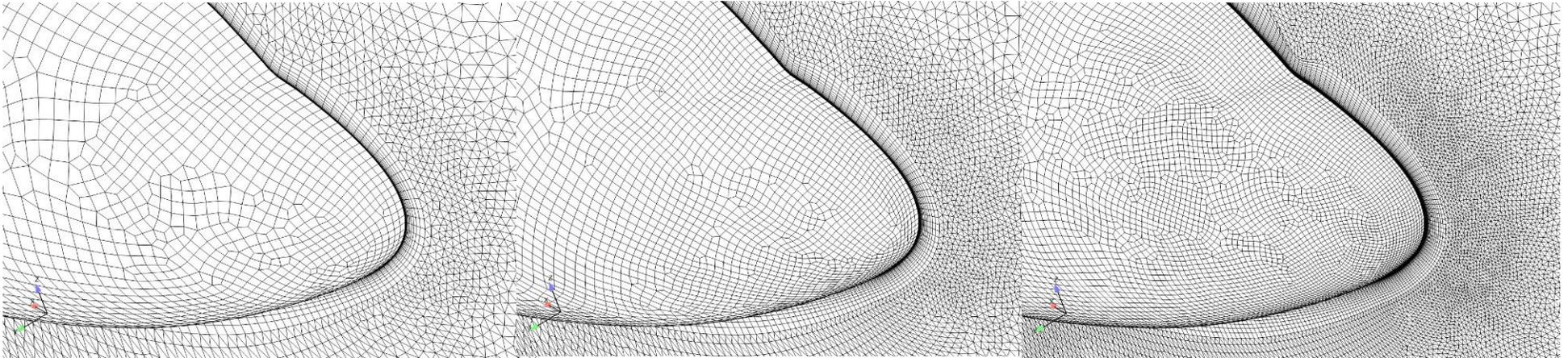


FOI grids, tail 0

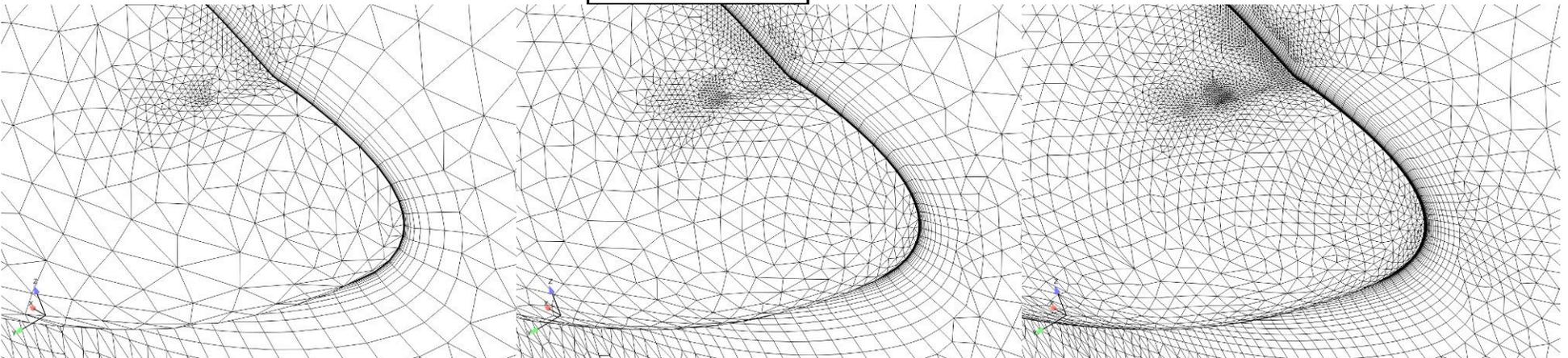


# Grid pictures, nose

DLR grids, tail 0

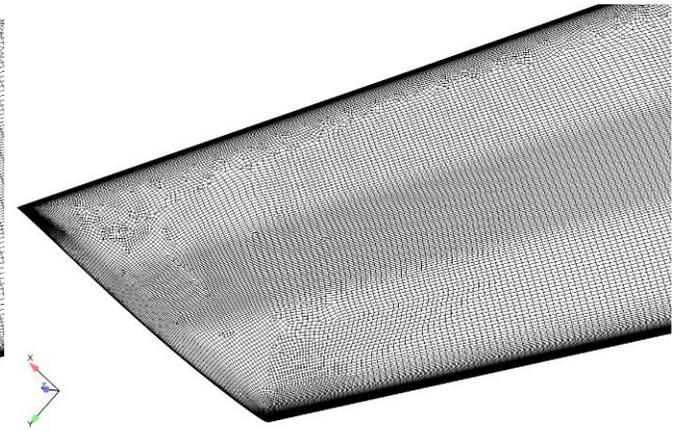
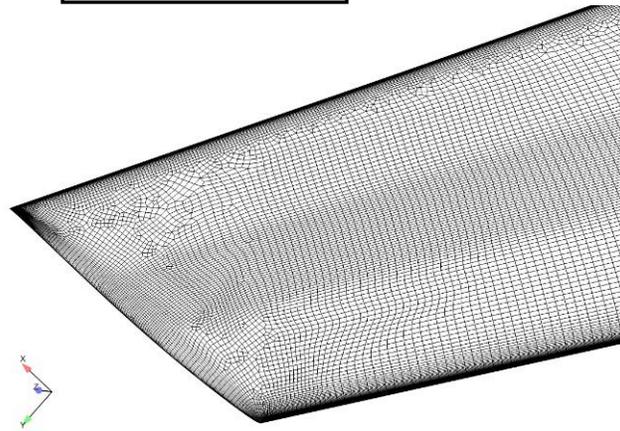
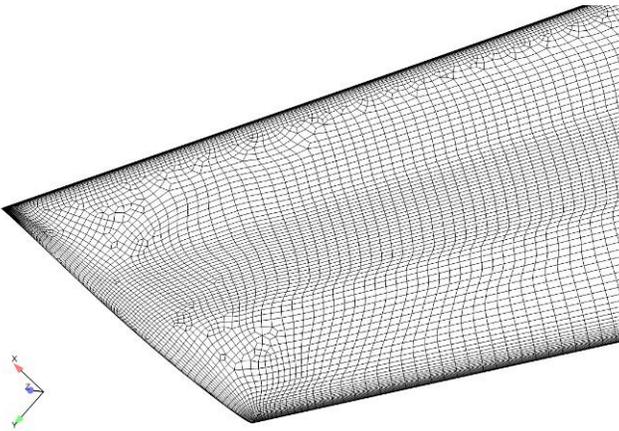


FOI grids, tail 0

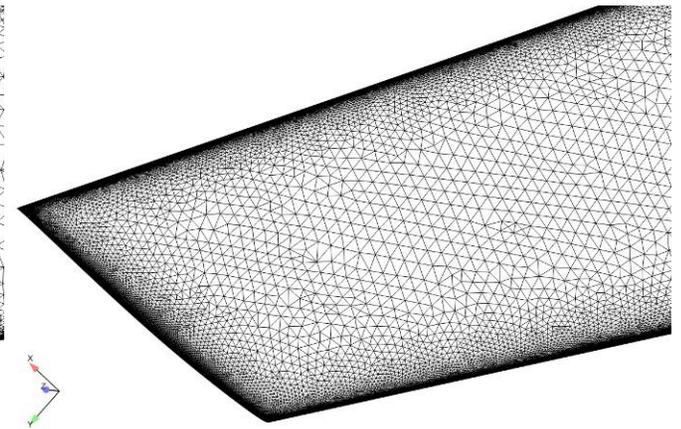
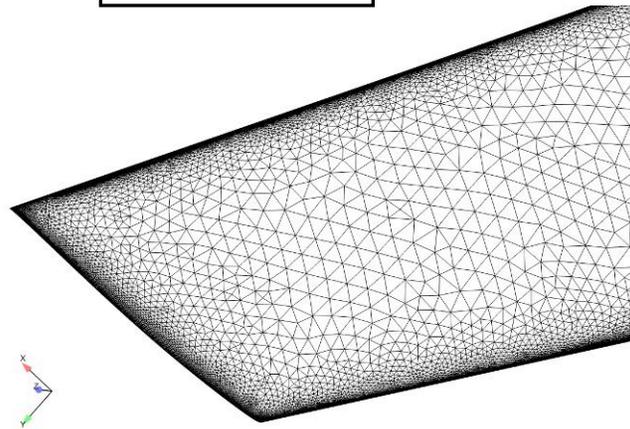
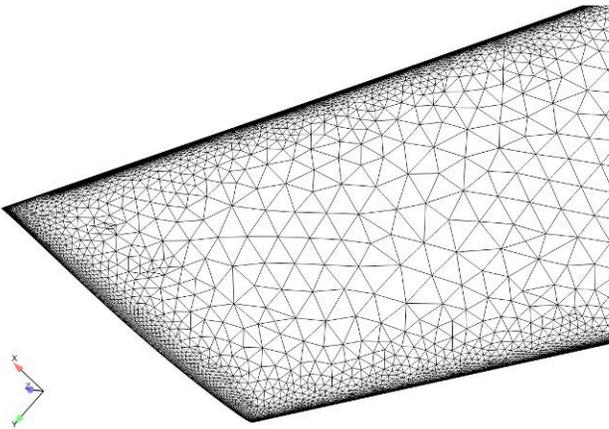


# Grid pictures, wing tip

DLR grids, tail 0

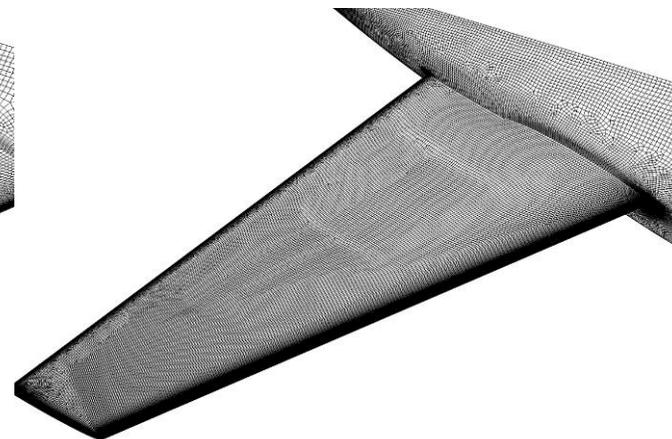
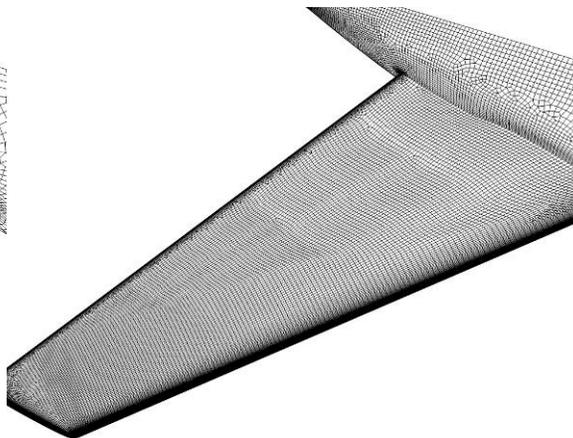
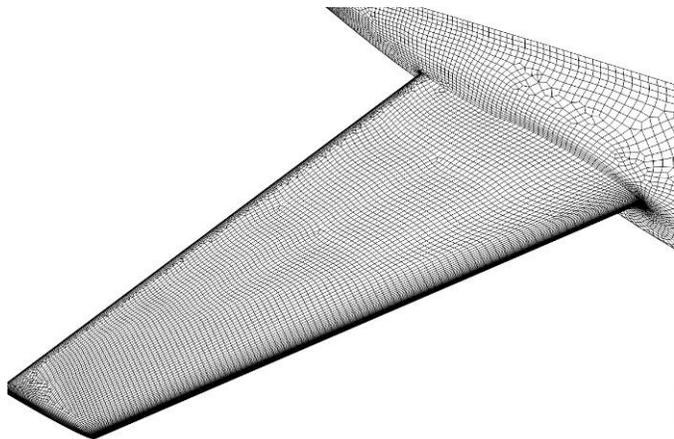


FOI grids, tail 0

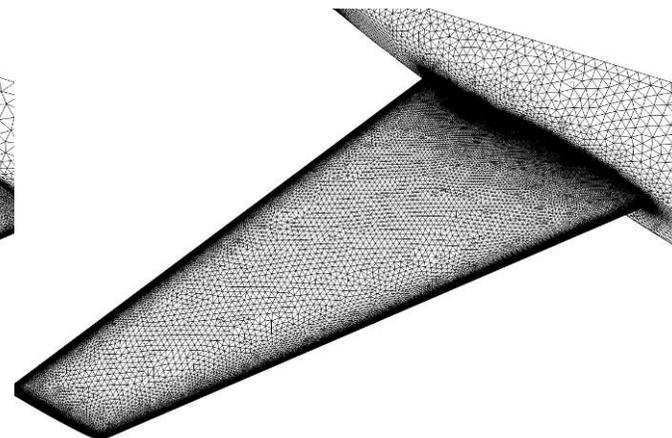
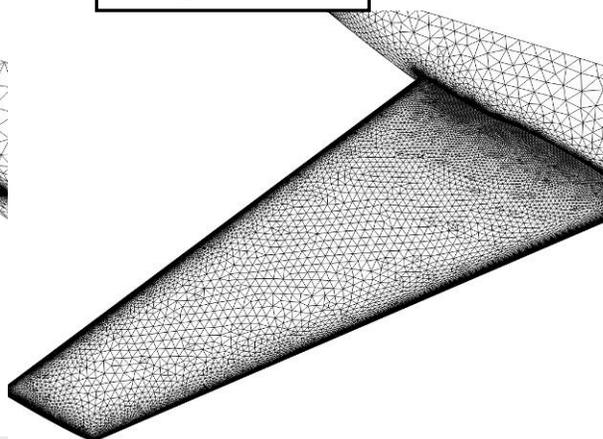
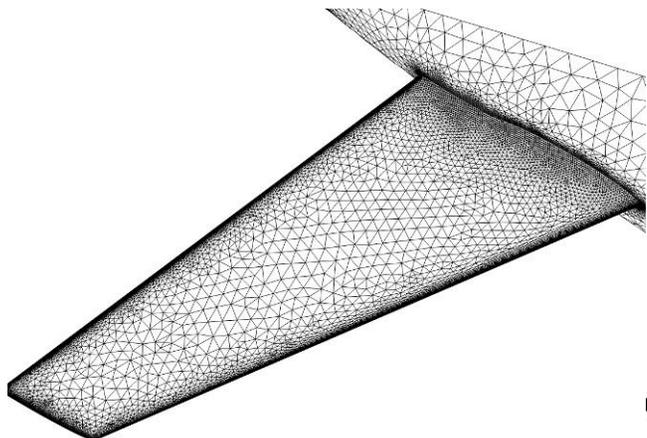


# Grid pictures, tail

DLR grids, tail 0



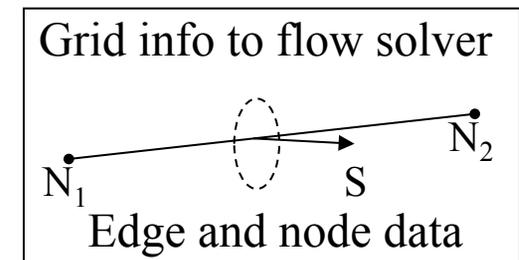
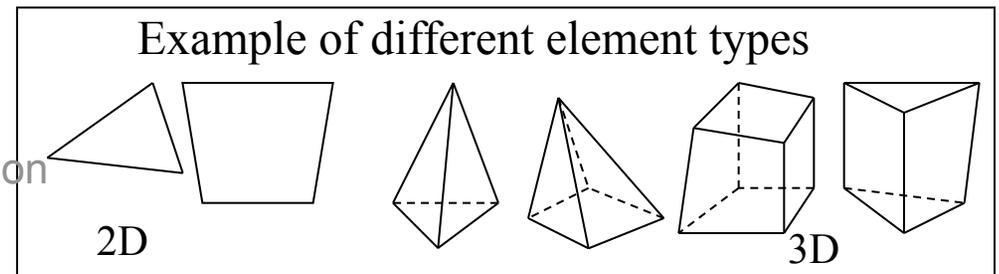
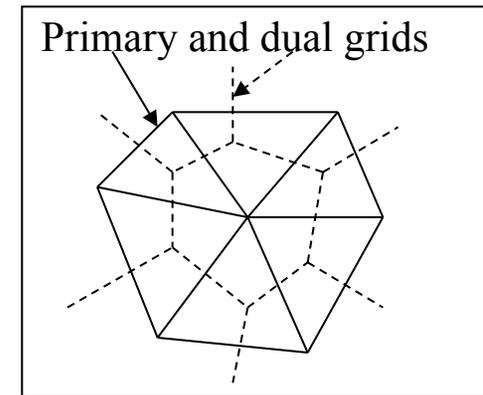
FOI grids, tail 0



# Edge solver

Edge – a Navier-Stokes solver for unstructured grids

- Solves the compressible NS equations
- RANS/RANS-LES/LES solver
- Node-centered/ finite-volume formulation
- Edge based formulation with median dual grids
- Runge-Kutta time integration
- Agglomeration multigrid
- Parallel with MPI
- Dual time stepping for unsteady extension
- High temperature extension
- Low speed preconditioning
- Aeroelastic capability
- Grid adaptation
- Adjoint solver for shape optimization



# Computational information

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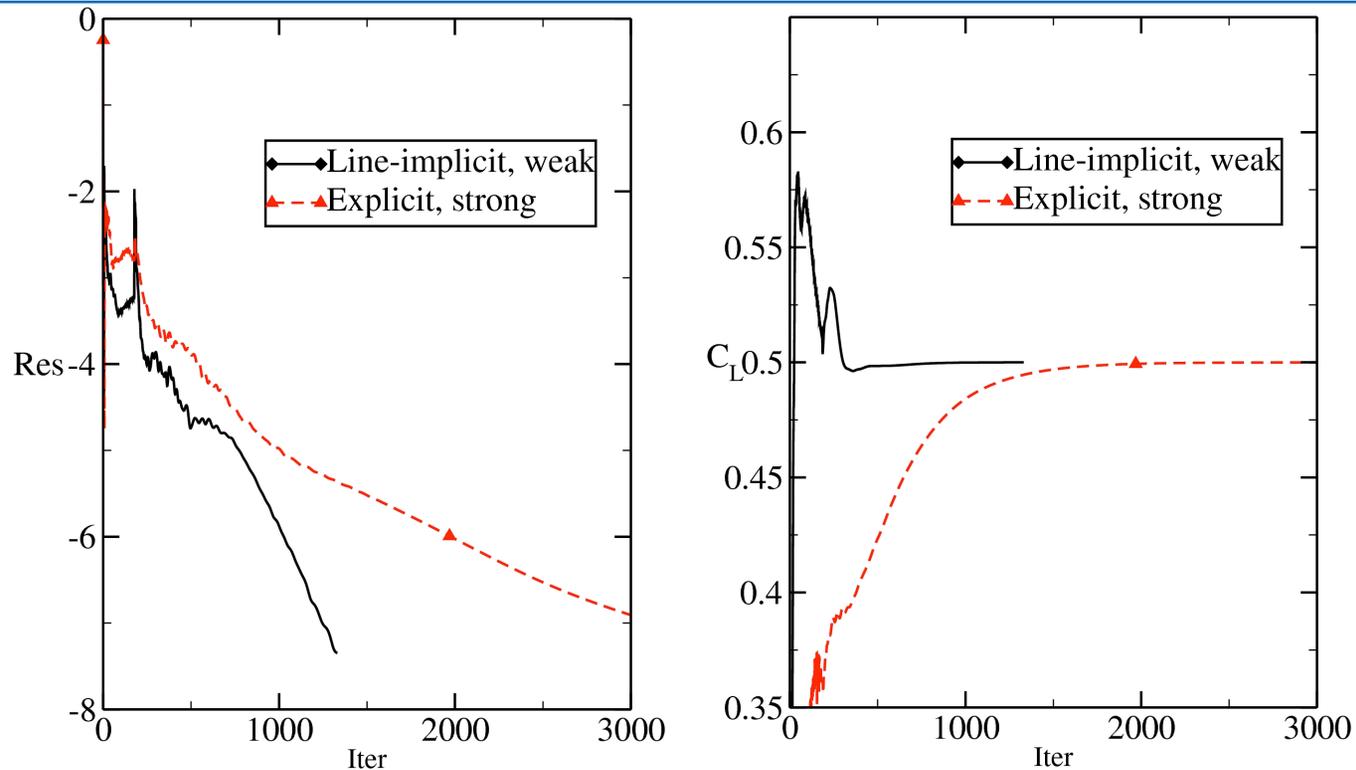
## Computational settings

- Hellsten k- $\omega$  EARSM for the turbulence (AIAA Journal, Vol. 43, 2005)
  - Grid convergence calculations with k- $\omega$  SST
- 3-4 level W-cycles, full multigrid
  - Semi coarsening, 1:4
- 3-stage Runge-Kutta scheme, CFL=1.25
- Central scheme with artificial dissipation for mean flow and turbulence
- Full NS, compact discretization of normal derivatives
- Linux cluster used, up to 64 processors
  - Computing time  $\sim$  (64\*) 6 hours for finest grids ( $\sim$ 33 M nodes)

## New since previous workshop

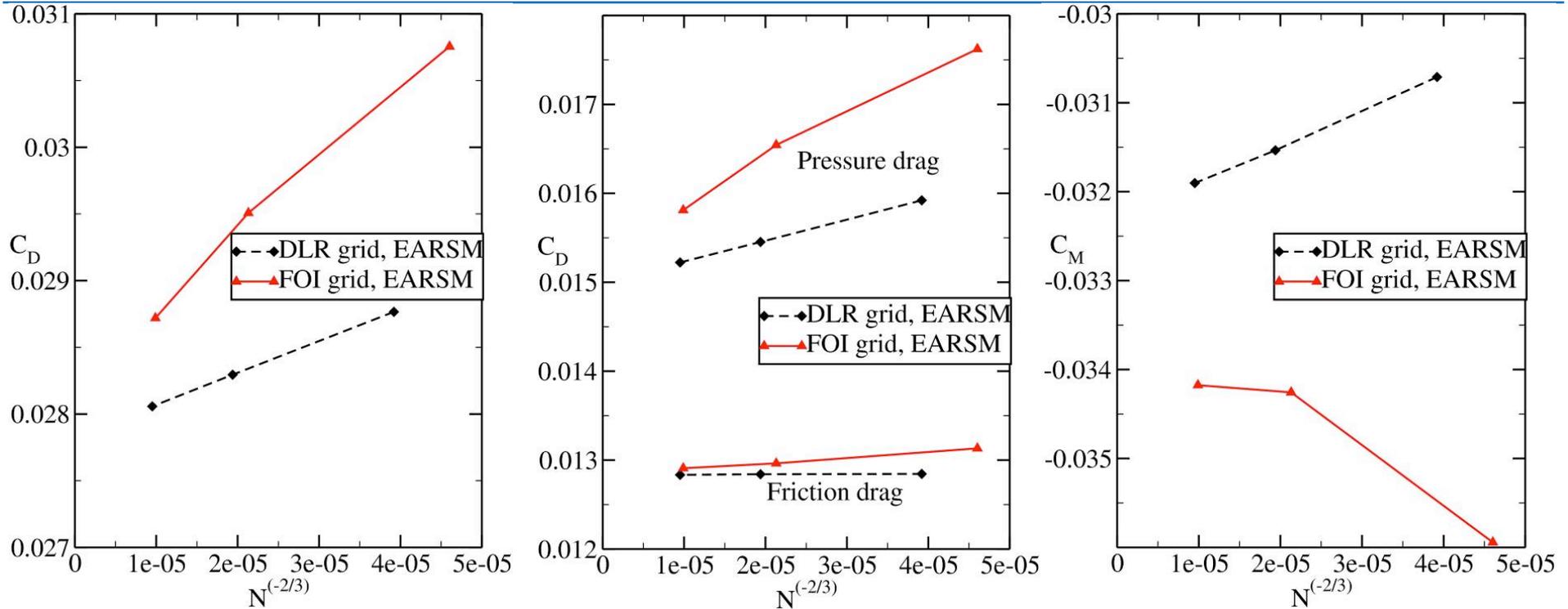
- Line-implicit time integration
- Weak boundary conditions on all variables including no-slip velocity
  - AIAA 2009-3551, presented on Monday June 22, 9.30
- Central discretization of turbulent equations

# Steady state convergence



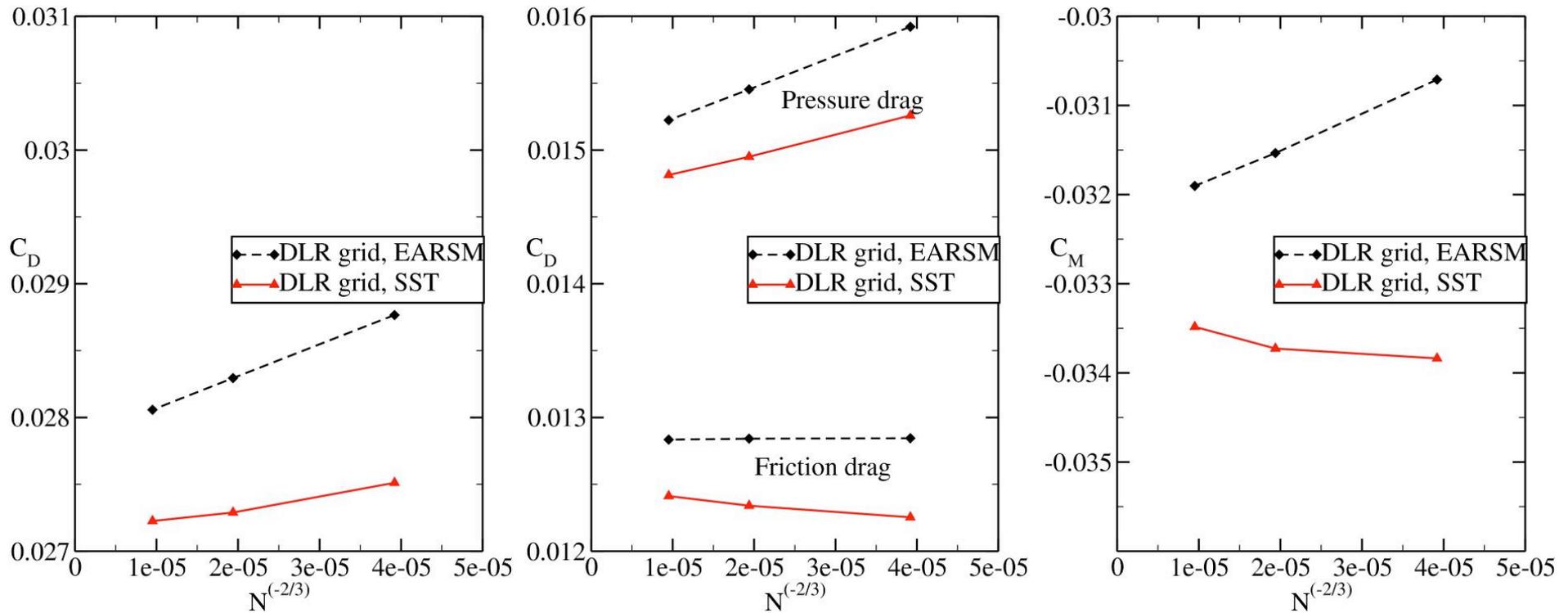
- Convergence (density res. and lift) on DLR medium grid, tail 0,  $C_L=0.5$
- 3 levels full multigrid W cycles
- Convergence  $|\Delta C_L| < 0.1\%$  requires:
  - $\leq 600$  fine grid iterations line implicit
  - $\leq 2000$  fine grid iterations explicit
  - Specified  $C_L$  requires some extra iterations

# Grid convergence, $C_L=0.5$



- Comparison between DLR and FOI grids
- Excellent grid convergence with DLR grids
  - Acceptable with FOI grids
- Grid converged drag: DLR grids  $C_D=278.3$ , FOI grids  $C_D=280.3$

# Grid convergence, $C_L=0.5$



- Comparison between EARSM and  $k-\omega$  SST, DLR grids
- Good grid convergence, slightly worse grid convergence with SST
- Converged drag: EARSM  $C_D=278.3$ , SST  $C_D=271.6$

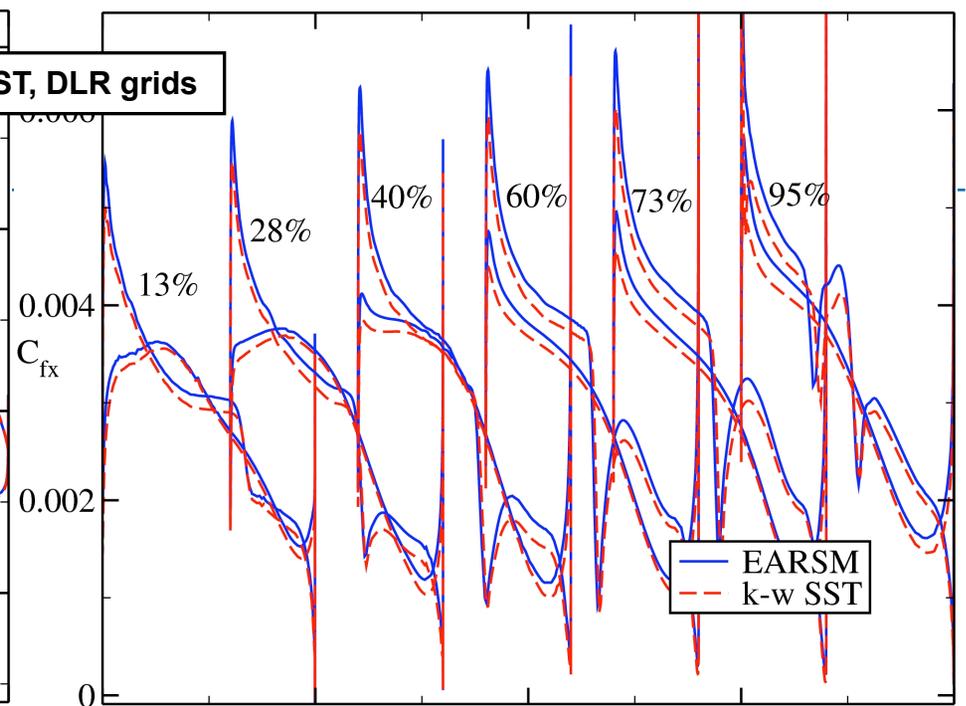
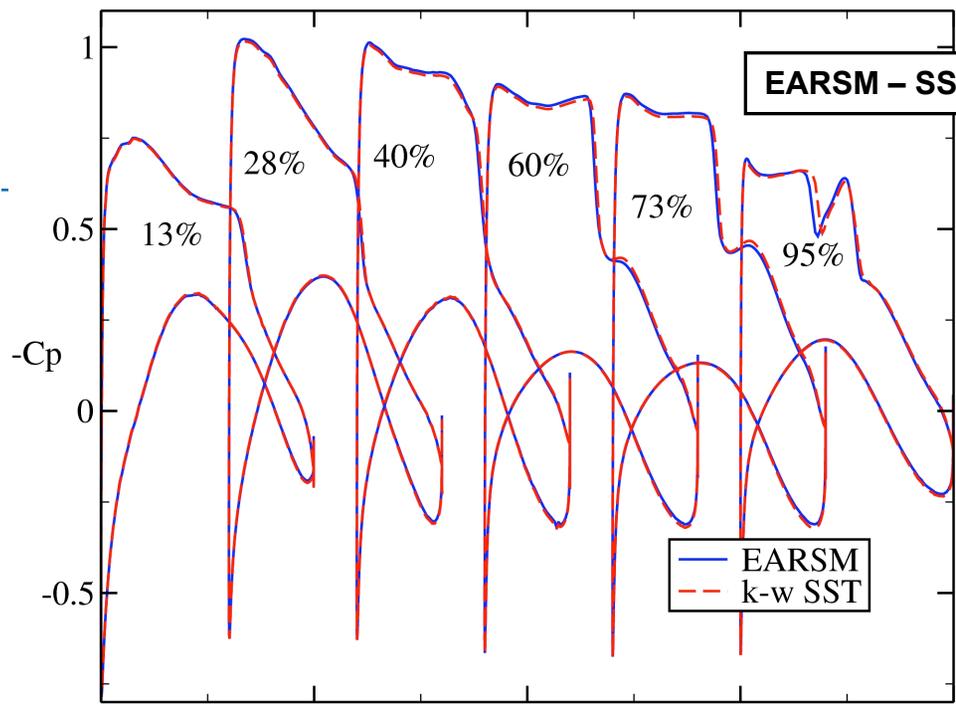
# Grid convergence, $C_L=0.5$

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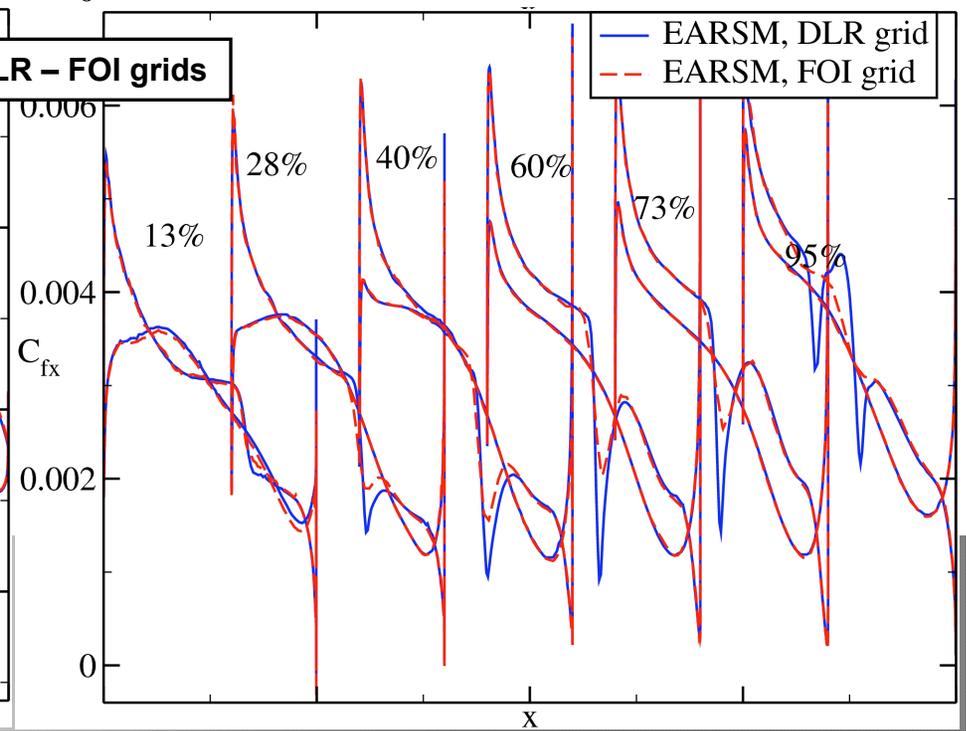
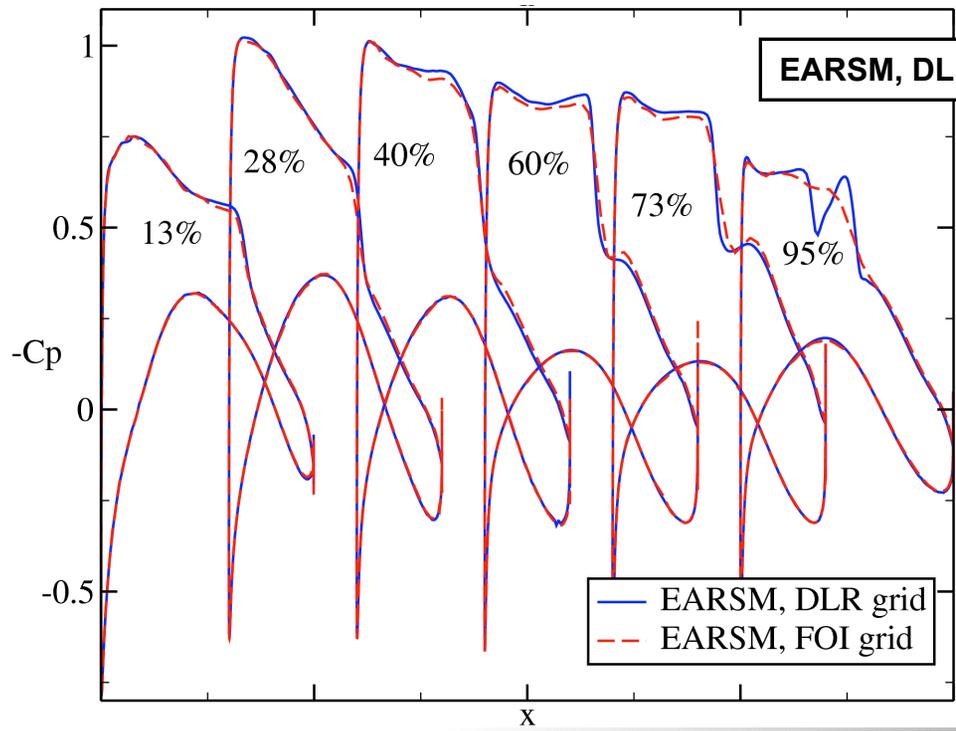
	<b>EARSM</b>	<b>k-<math>\omega</math> SST</b>
<b>DLR grids</b>	$0.18 \times 10^{-4}$	$0.93 \times 10^{-4}$
<b>FOI grids</b>	$5.0 \times 10^{-4}$	-

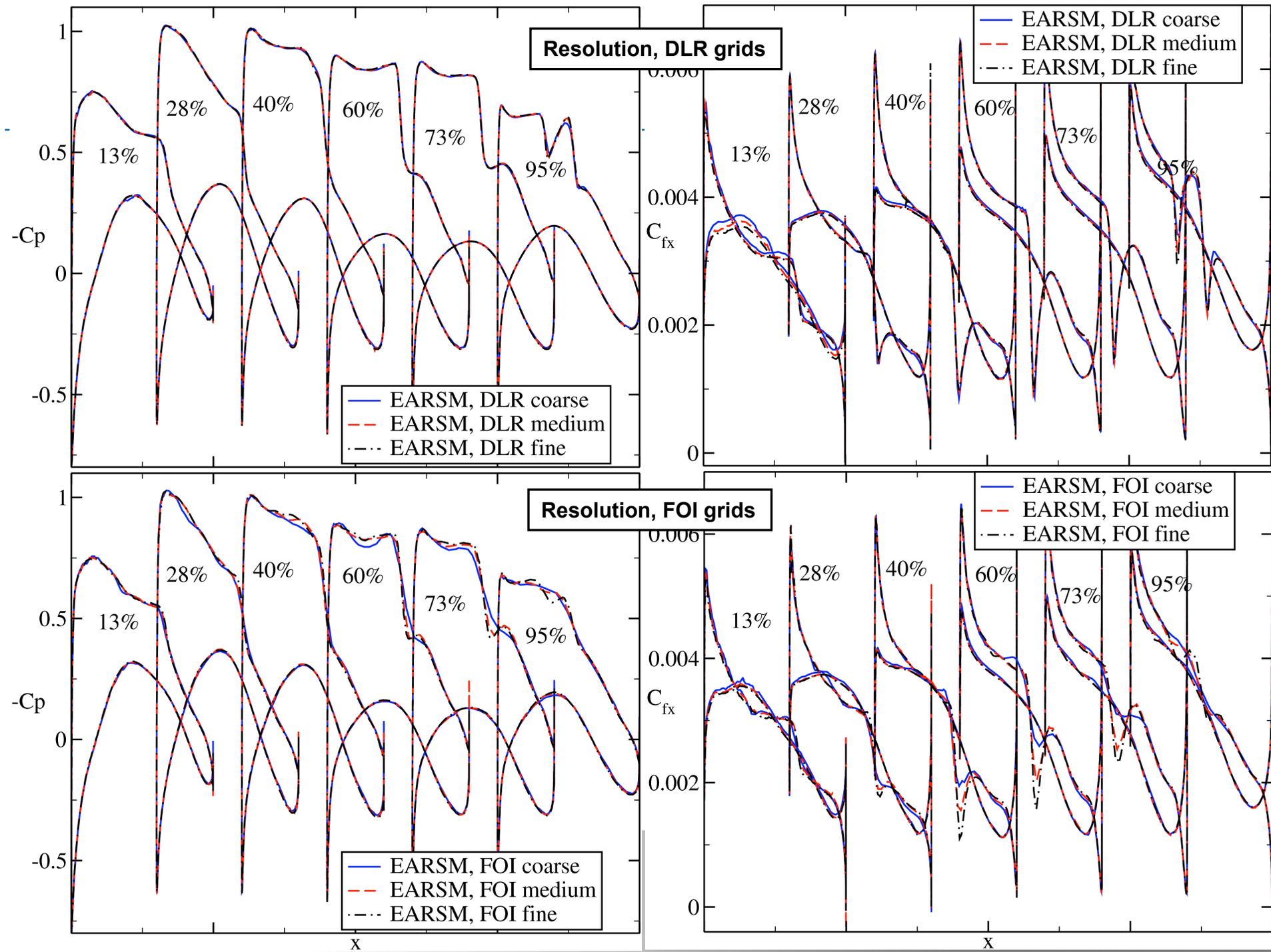
- Measure of Merit, as defined in DPW3
  - Measures the linearity of the slope of drag grid convergence
  - Based on Richardson extrapolation from coarse-medium and medium-fine grids
  - Low value = good value

**EARSM – SST, DLR grids**

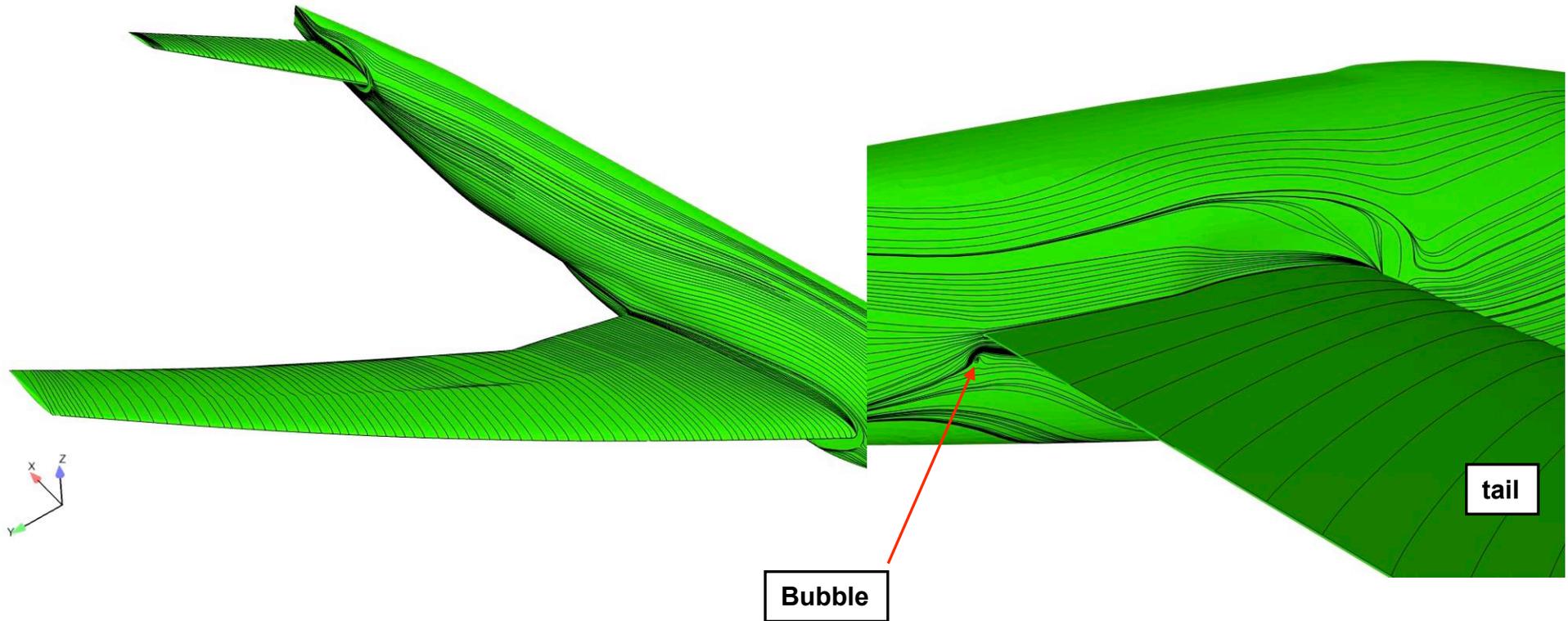


**EARSM, DLR – FOI grids**





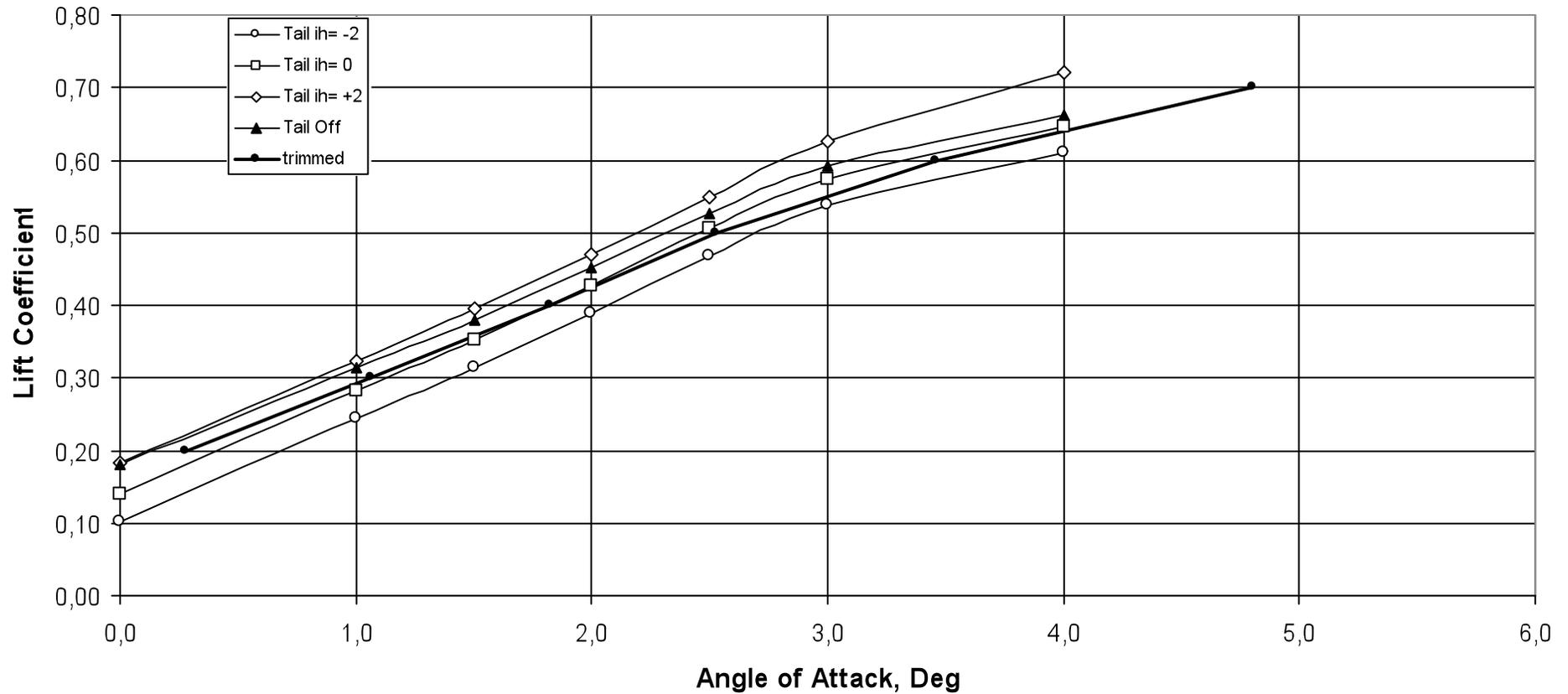
# Skin friction, tail 0°, $C_L=0.5$



- DLR grid, EARSM
- Attached flow on wing and tail
- Separation on fuselage behind and below tail

# Polars, $C_L$

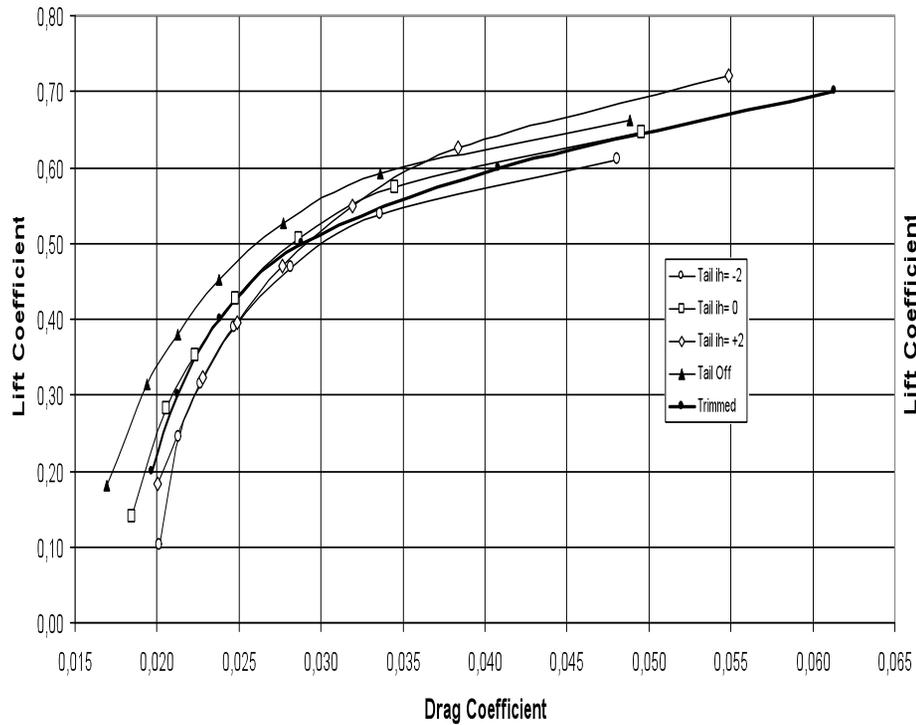
## DPW4/NASA CRM Effect of Stabilizer Angle on $C_L$



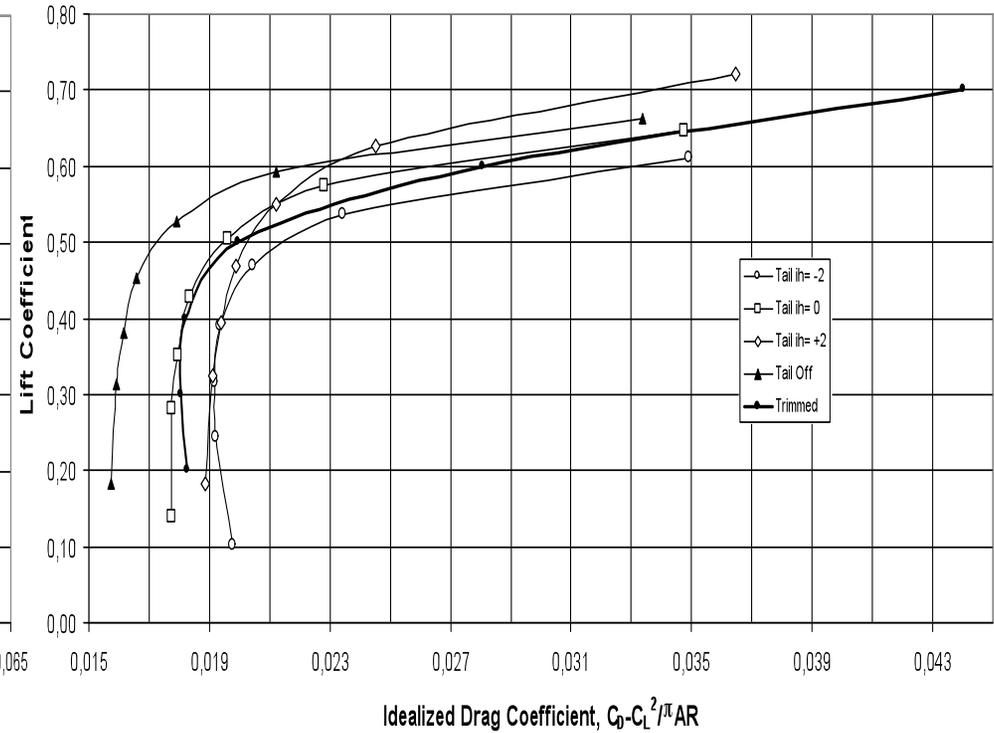
■ DLR grids, EARSM

# Polars, $C_D$

DPW4/NASA CRM Effect of Stabilizer Angle on  $C_D$



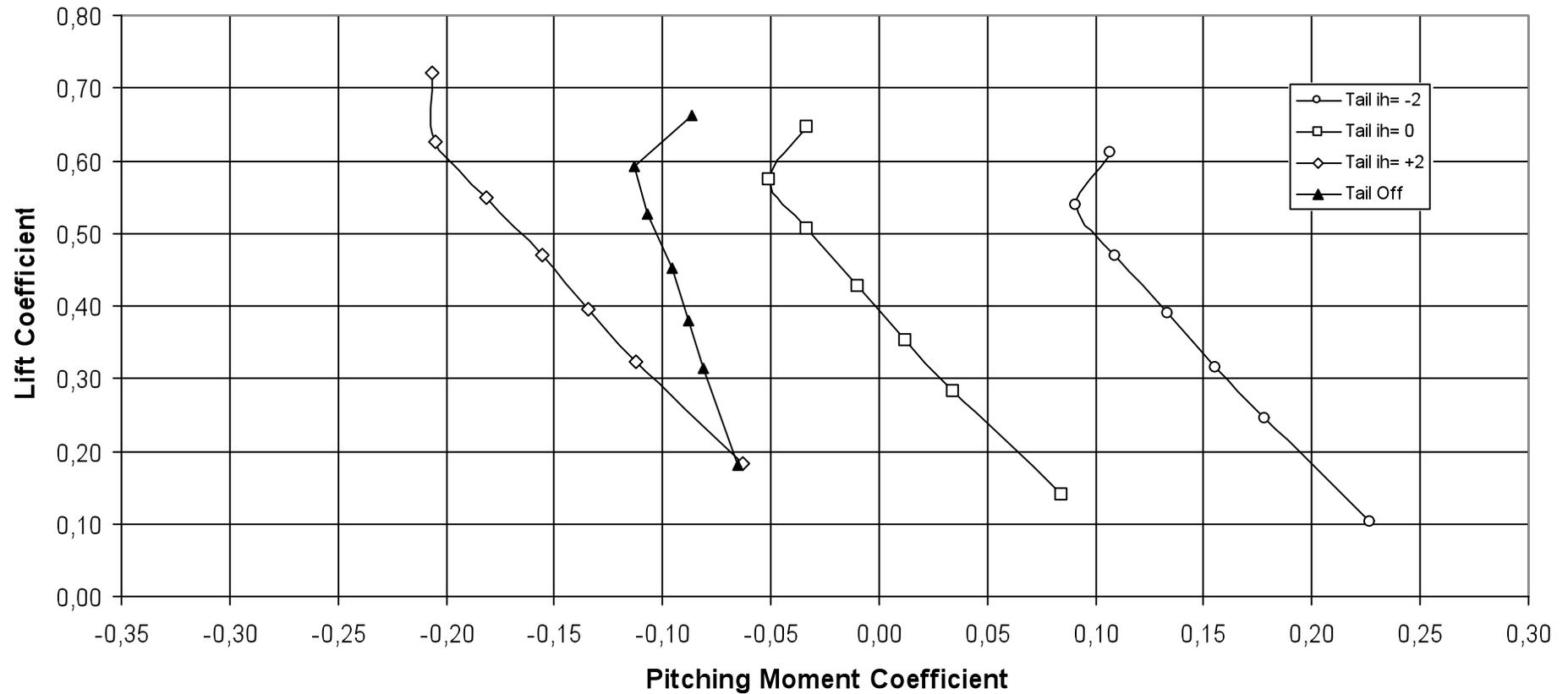
DPW4/NASA CRM Effect of Stabilizer on  $C_D - C_L^2/\pi AR$



- DLR grids, EARSM
- $\Delta C_D = 26$  cts at  $C_L=0.5$  (trimmed vs. tail off)

# Polars, $C_M$

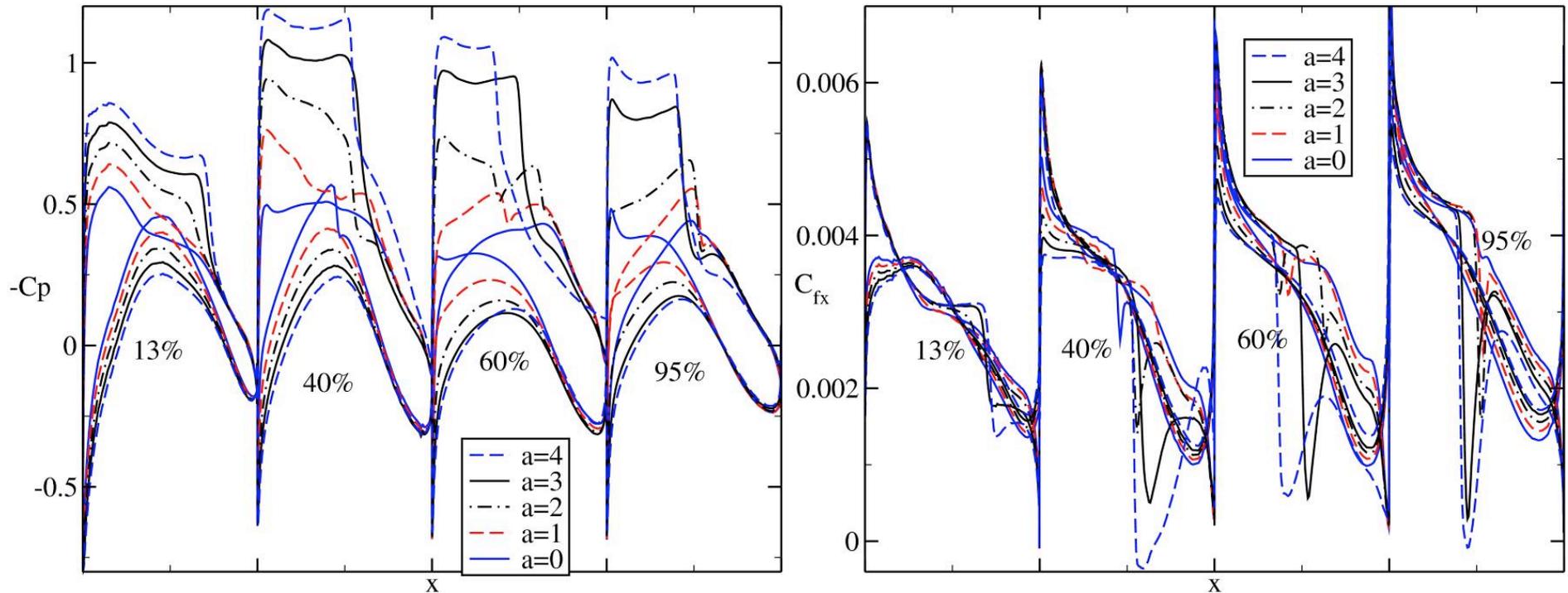
## DPW4/NASA CRM Effect of Stabilizer Angle on $C_M$



■ DLR grids, EARSIM

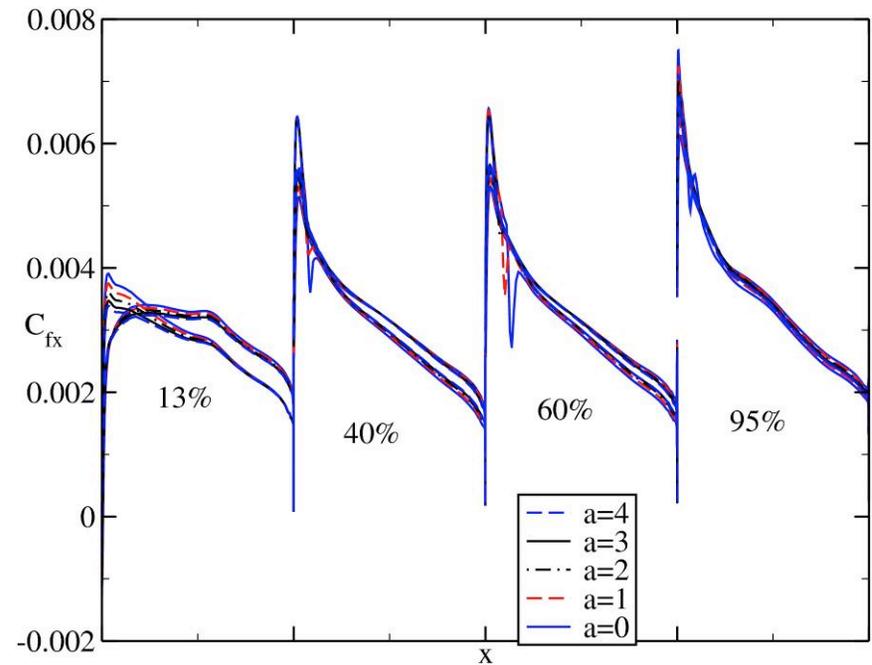
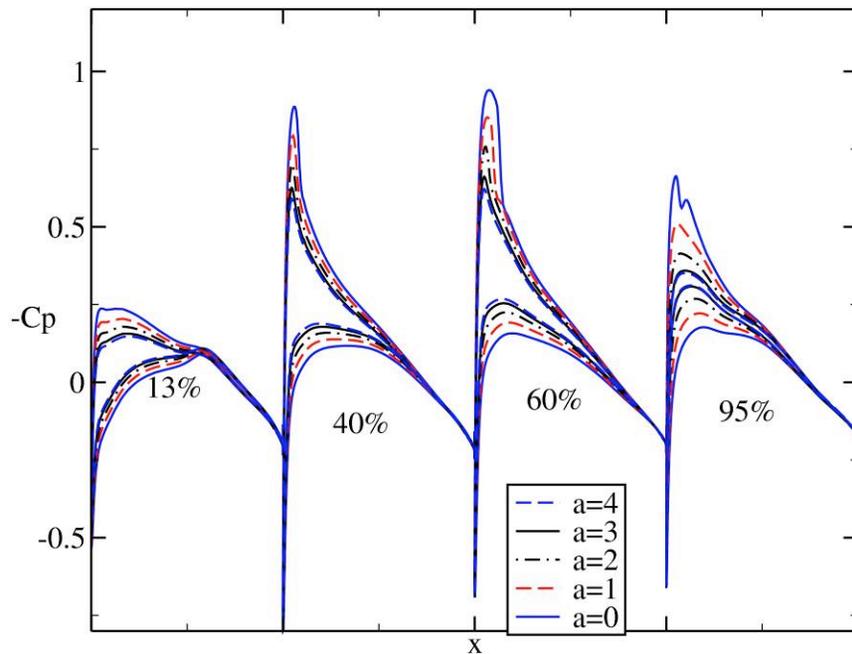


# $C_p$ on wing, tail $0^\circ$



- 4 span wise cuts
- DLR grids, EARSM, 5 angles of attack
- Attached flow although small area with  $C_{fx} < 0$  at about 40% span

# $C_p$ on tail, tail $0^\circ$



- 4 span wise cuts
- DLR grids, EARSM, 5 angles of attack
- Attached flow

# Summary

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## ■ Grid convergence

- Very good results with DLR grids
- Acceptable with FOI grid, 2 cts difference
- k- $\omega$  SST gives slightly lower drag than EARSM , 7 cts difference
- $\Delta C_M = 1.9 \times 10^{-3}$  DLR-FOI grids,  $\Delta C_M = 1.0 \times 10^{-3}$  EARSM - SST
- Attached flow on wing and tail, fuselage separation behind/below tail

## ■ Downwash study

- Linear lift increase up to about  $\alpha = 3^\circ$
- Tendency to separate at highest  $\alpha = 4^\circ$