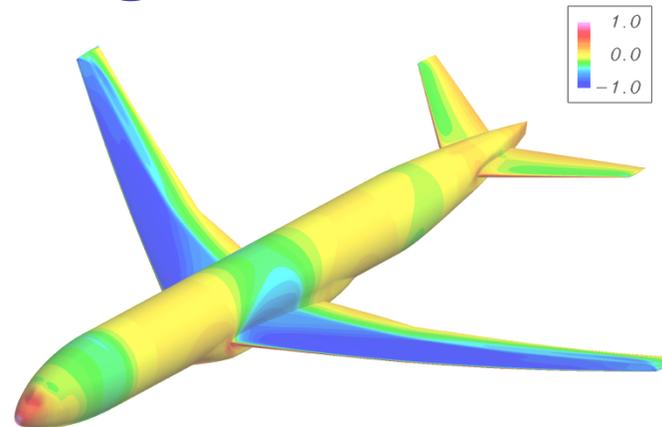


4th AIAA CFD Drag Prediction Workshop

Computational Results using UPACS & TAS



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Objective and Outline

- Evaluation of CFD codes used in APG/JAXA through DPW.
 - Multi-block structured mesh code, UPACS
 - Unstructured mesh code, TAS

- Outline of Presentation
 - Self-made computational grids
 - Codes
 - Case 1.1 Grid convergence study
 - Case 1.2 Downwash study
 - Case 2: Mach sweep
 - Case 3: Reynolds number study

- Points of discussion
 - Comparison of calculated aerodynamic force between two methods
 - Large flow separation at wing-body corner

Grid information

CRM WING/BODY/TAIL ($i_H = 0$)

Multi-Block Structured Grid (Gridgen)

	Cells	Surf. Faces	BL 1st-Cell Size [inch]	BL Growth Rate	TE Cells
Coarse	2.8M	127K	0.001478	1.31	14
Medium	9.0M	276K	0.000985	1.20	20
Fine	30.4M	620K	0.000657	1.13	30

Coarse & Fine grids ← Based on interpolation of Medium grid

Multi-grid “unfriendly”

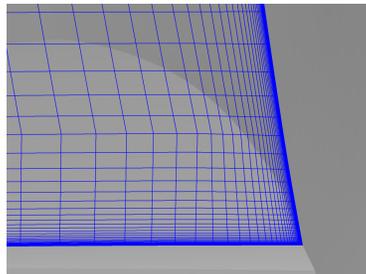
Hybrid unstructured Grid (MEGG3D)

	Nodes	Surf. Nodes	BL 1st-Cell Size [inch]	BL Growth Rate	TE Cells
Coarse	5.9M	213K	0.001478	1.31	1 - 4
Medium	13.5M	370K	0.000985	1.20	2 - 5
Fine	31.3M	589K	0.000657	1.13	3 - 7

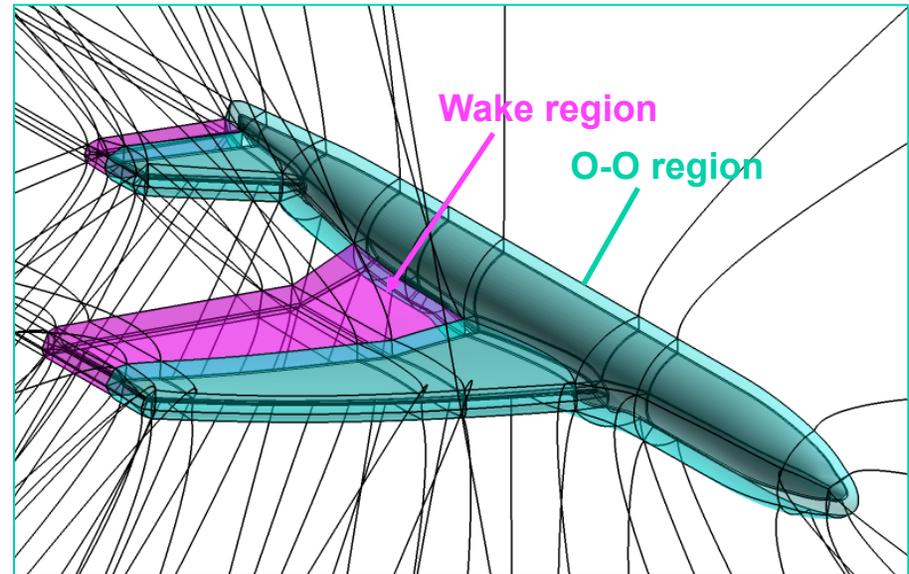
 Different from the grid guideline

Point-matched multi-block structured grids

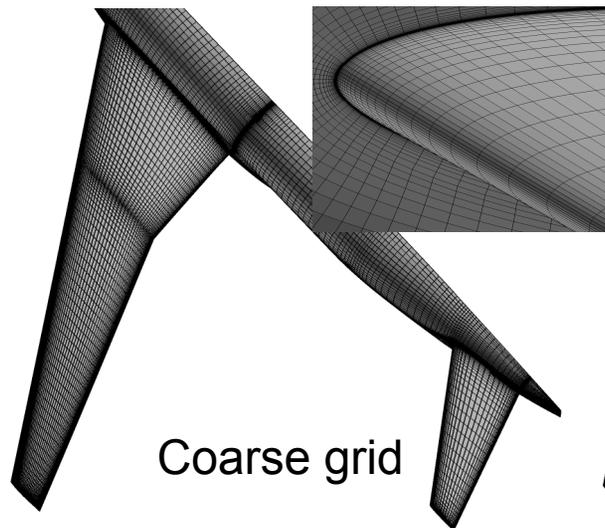
- Near the model surface:
 - O-O grid topology to guarantee better orthogonality within the boundary layer
- Outward:
 - C-O grid topology



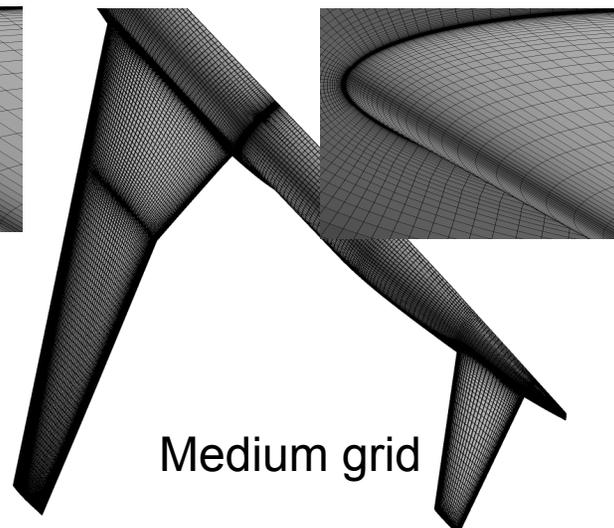
Wing-body juncture corner



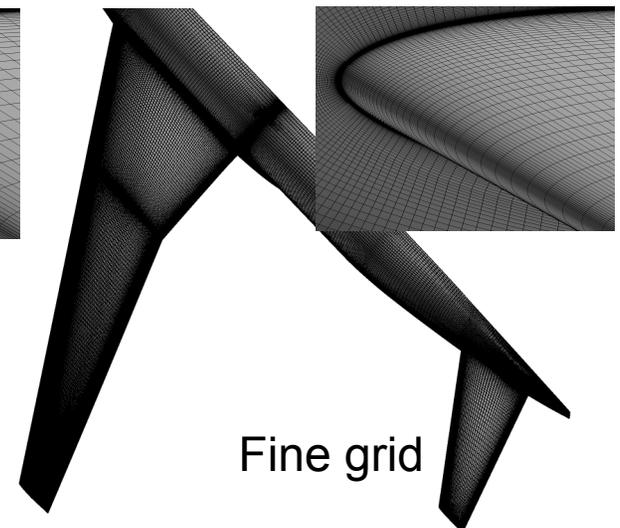
Block wire frame for NASA CRM



Coarse grid



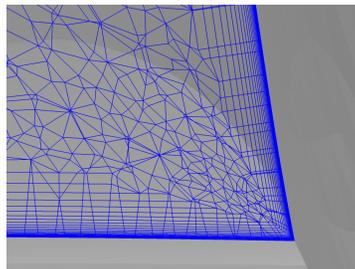
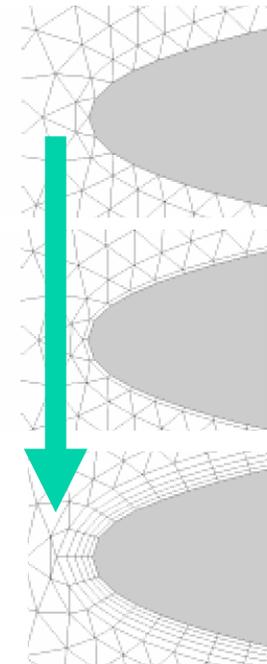
Medium grid



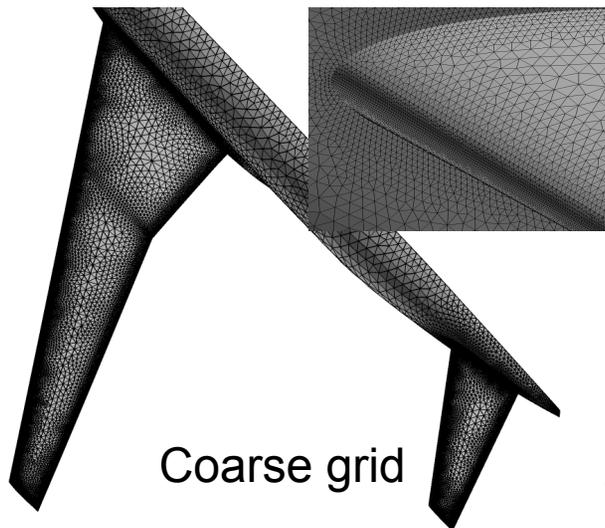
Fine grid

Mixed-element, hybrid-unstructured grids

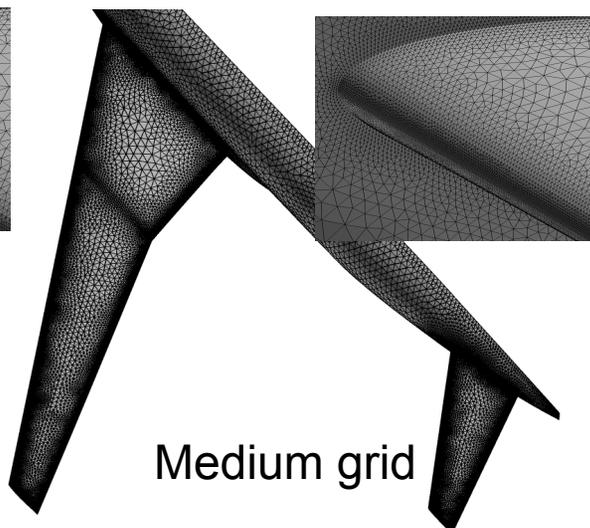
- Surface grid (Triangles)
 - Direct advancing front method
 - Use of triangles that are not so stretched
- Volume grid (Tetrahedra, Prisms, Pyramids)
 - Delauney (tetra) → insertion of prismatic layer (prism)



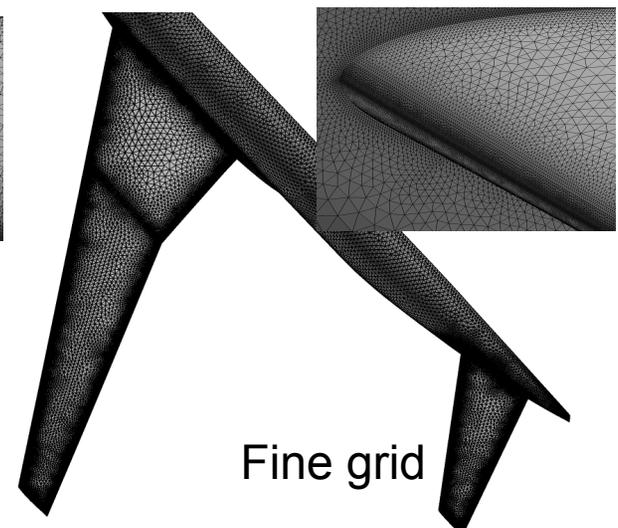
Wing-body juncture corner



Coarse grid



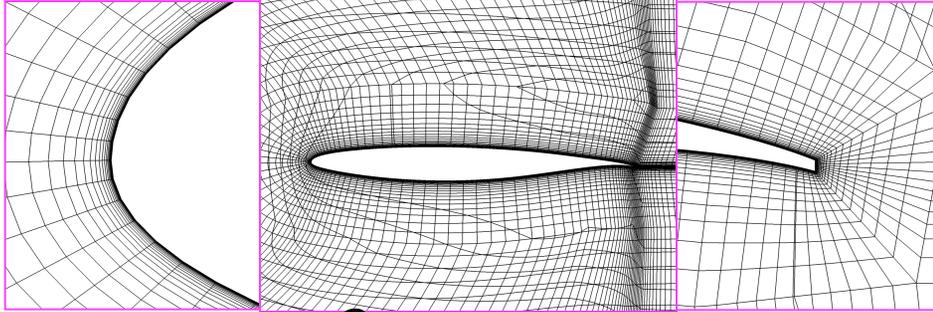
Medium grid



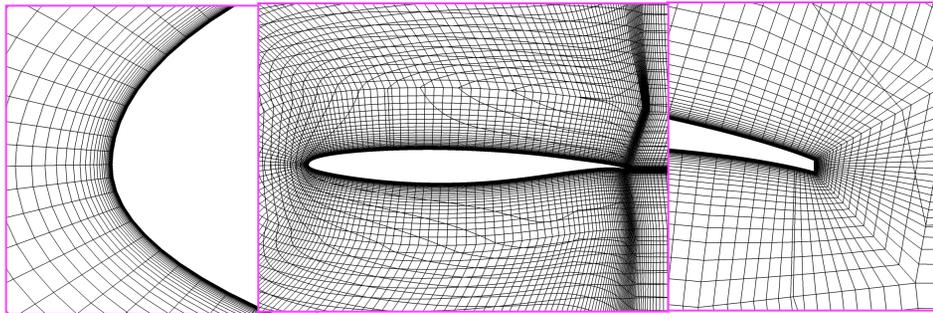
Fine grid

Comparison of cross-sectional view at kink location

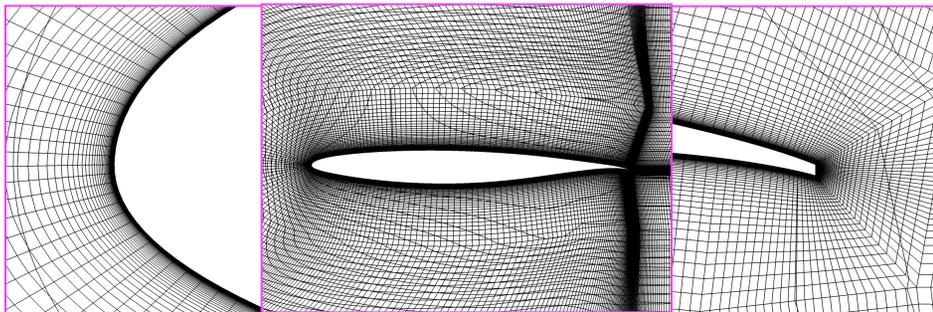
Multi-Block Structured Grid



Coarse

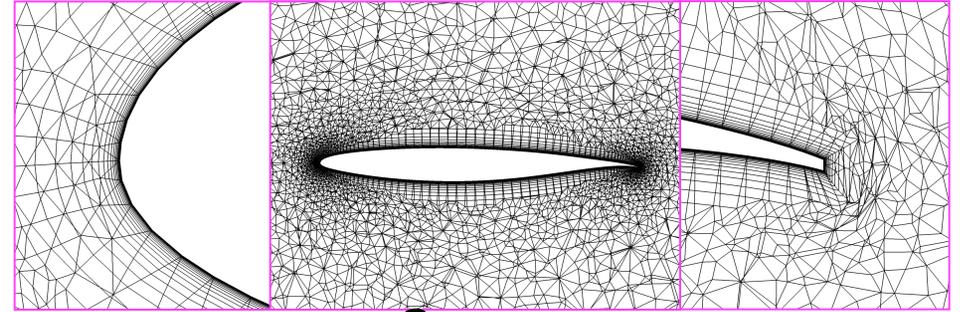


Medium

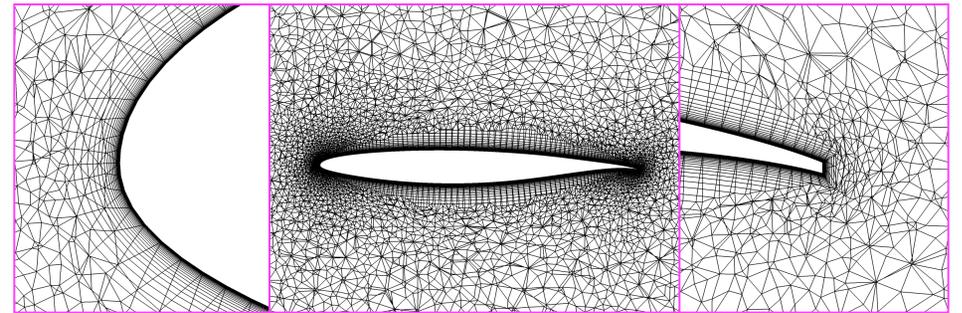


Fine

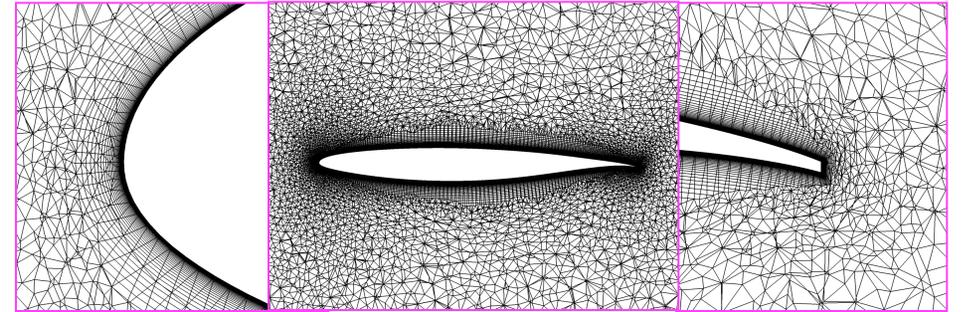
Unstructured Grid



Coarse



Medium



Fine

Numerical methods: UPACS & TAS

	UPACS	TAS
Mesh type	Multi-block structured	Unstructured
Discretization	Cell-centered finite volume	Cell-vertex finite volume
Convection Flux	Roe 2nd-order with van Albada's Limiter	HLLW 2nd-order with Venkatakrishnan's limiter
Time integration	Matrix-Free Gauss-Seidel	LU-Symmetric Gauss-Seidel
Turbulence model	Spalart-Allmaras model	Spalart-Allmaras model

- Modification to the S-A model

- without trip related terms
- with a modification of production term: $S = \min(\sqrt{2\Omega^2}, \sqrt{2S^2})$

- Computer Platform: JSS - Fujitsu FX1 (SPARC64 VII 2.5GHz,3008cpu)

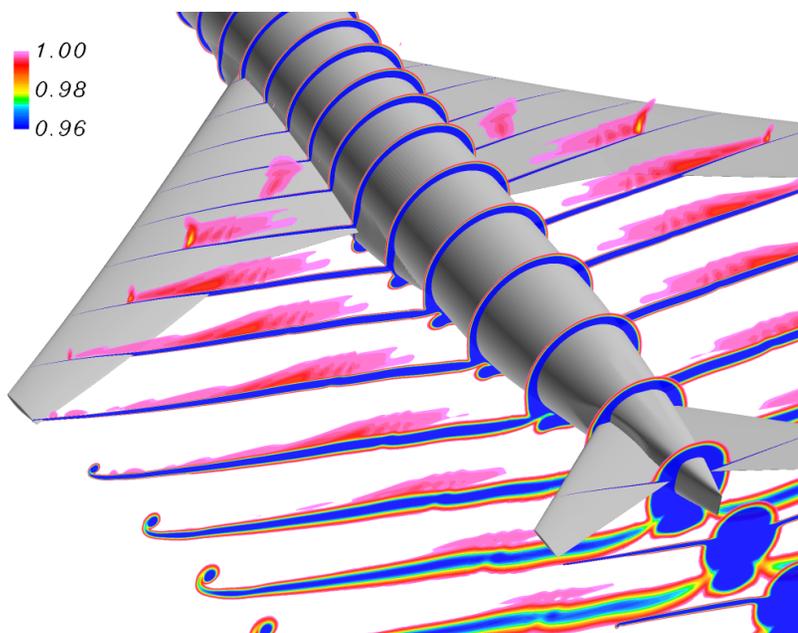
- UPACS: # Processors: 32 (172cores)
- TAS: # Processors: 43 (172cores)

Wake resolution

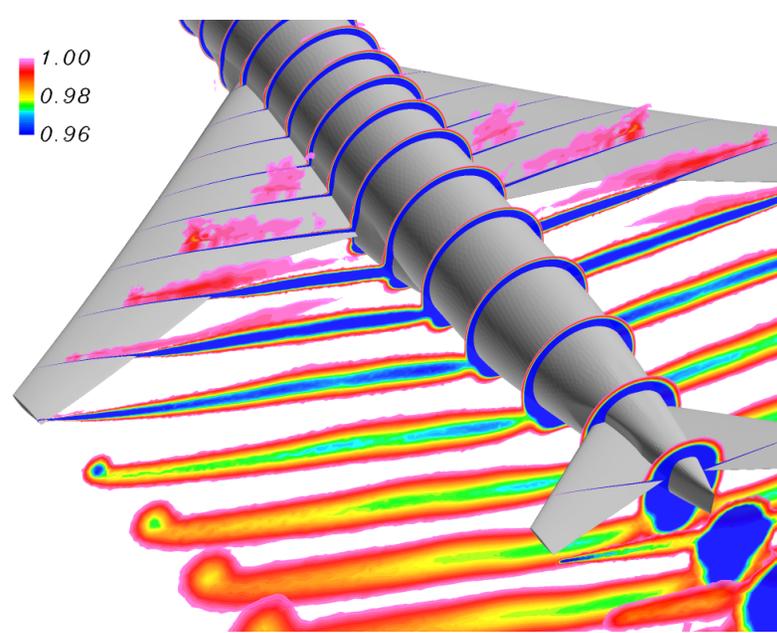
- $Re=5M$, $CL=0.5$, $i_H=0$, Fine grid

Total Pressure

UPACS



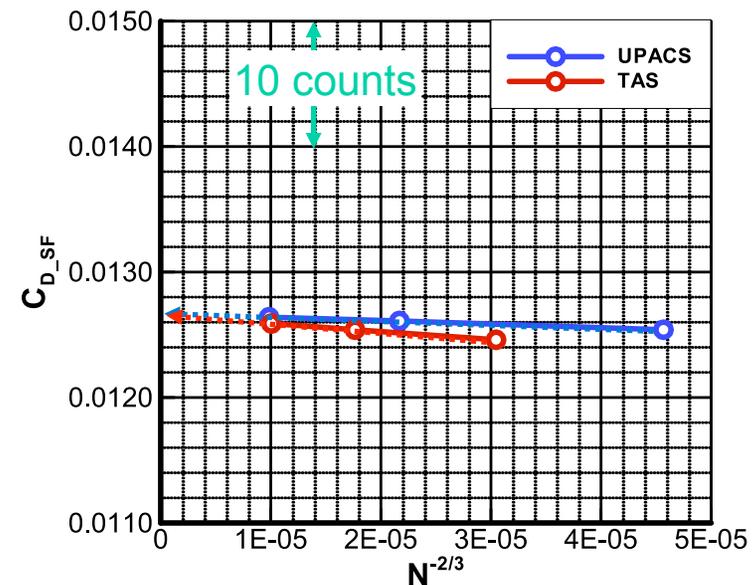
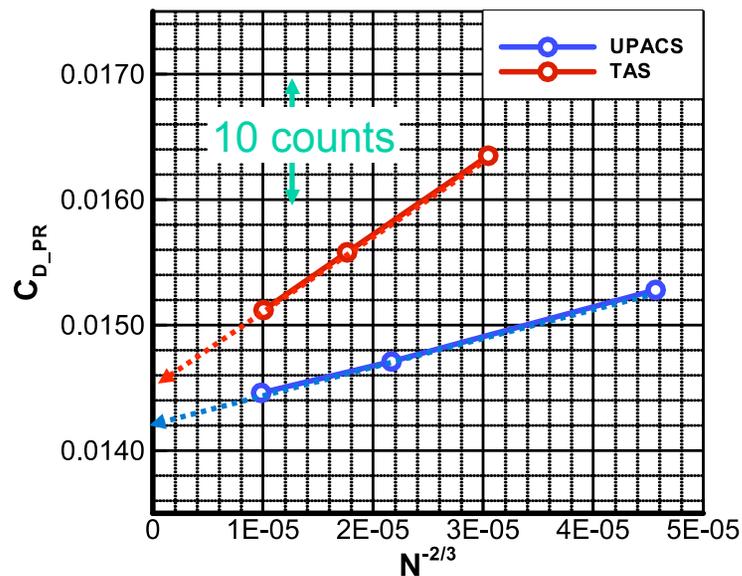
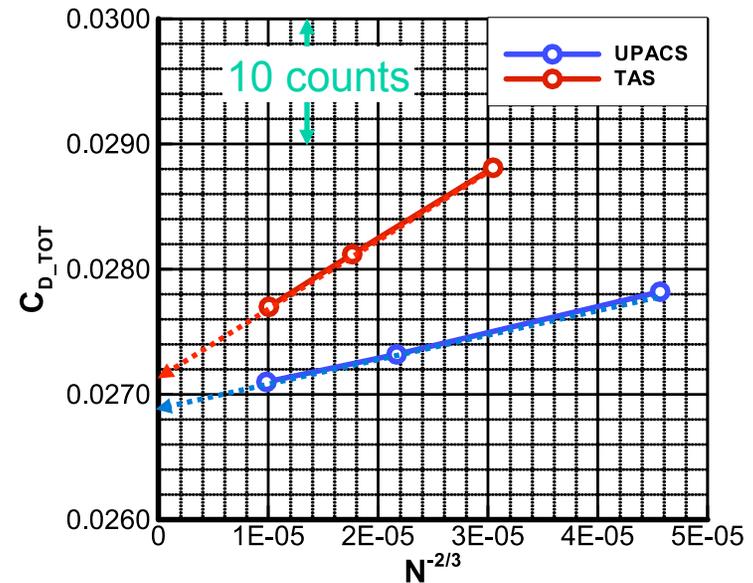
TAS



Case 1.1: Grid Convergence at Mach 0.85, $C_L=0.5$



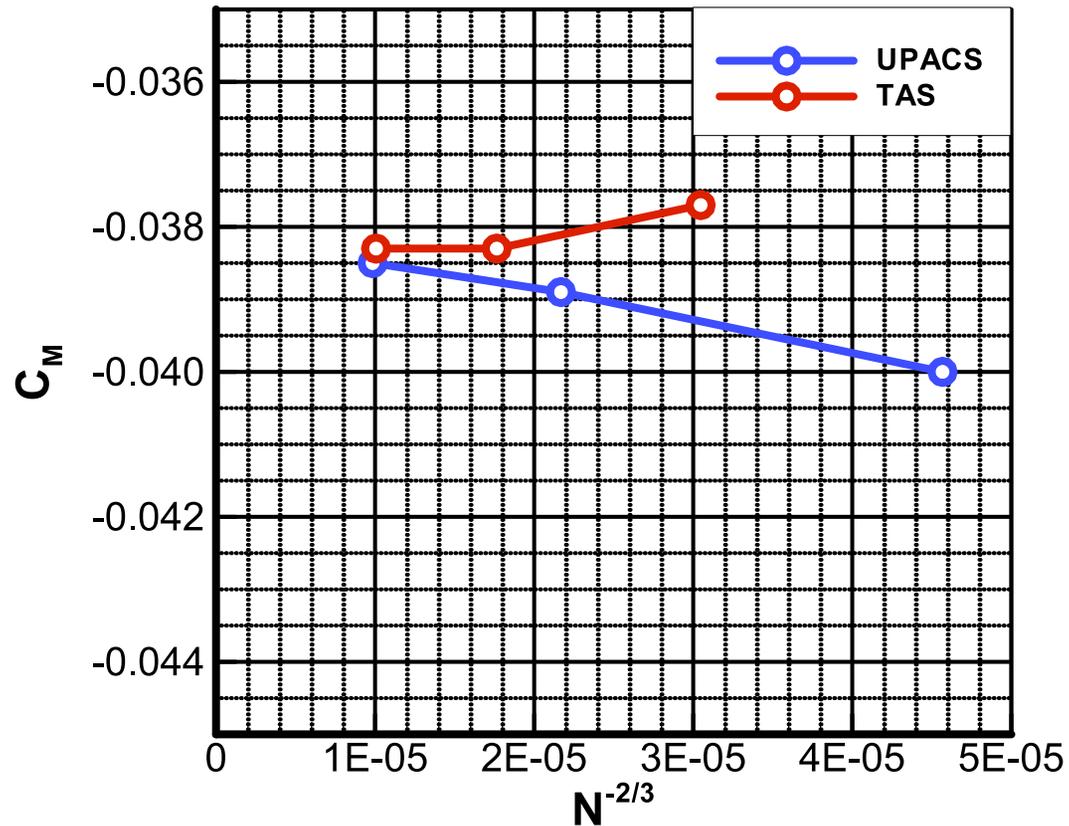
- Both methods obtained good convergence.
- Unstructured method shows higher C_{D_PR} and more variation with grid size.
- C_{D_SF} varies about 1 count.
- 2 to 3 counts difference at converged value?



Case 1.1: Grid Convergence at Mach 0.85, $C_L=0.5$

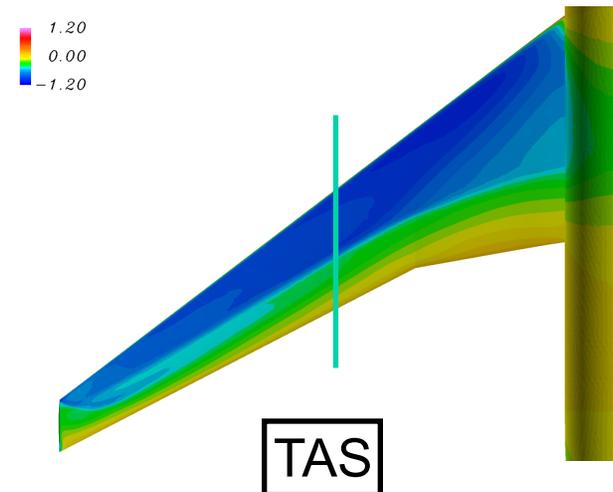
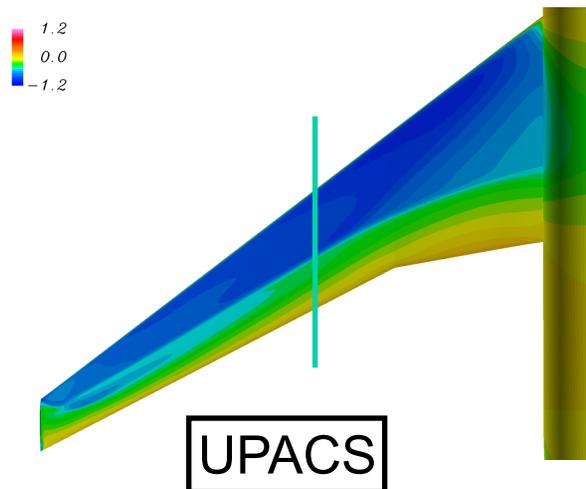
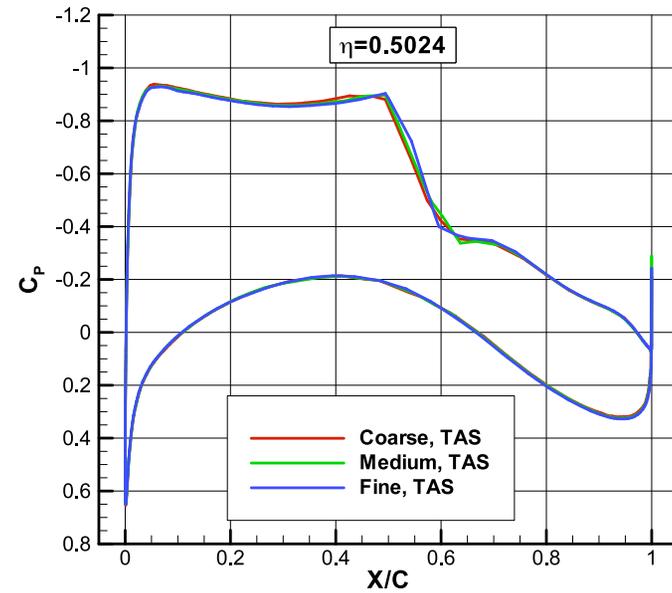
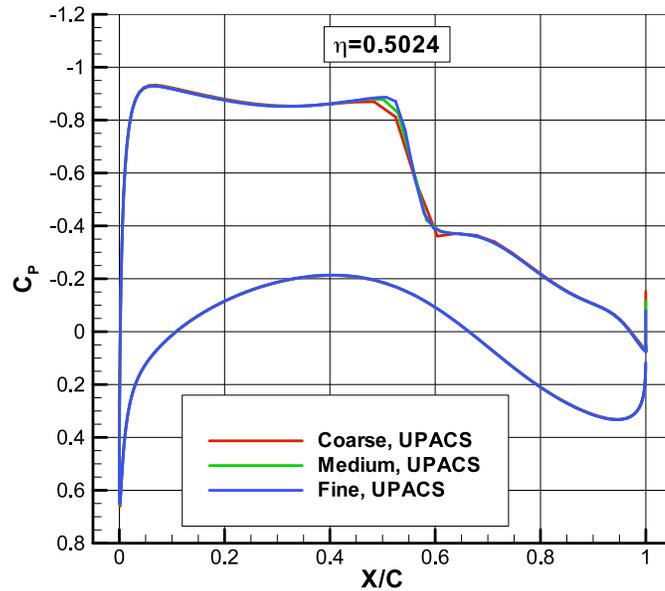


■ Pitching Moment



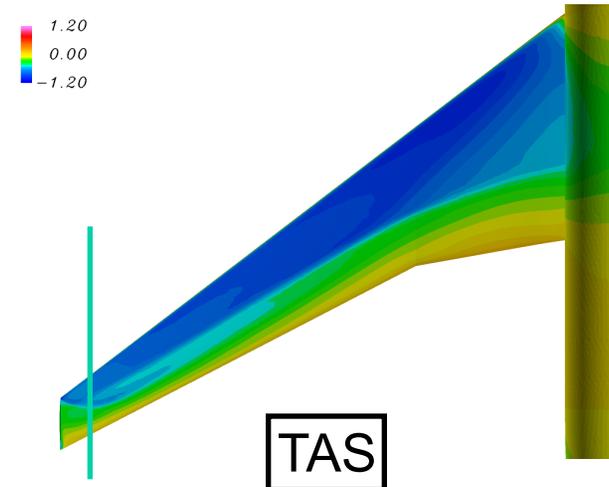
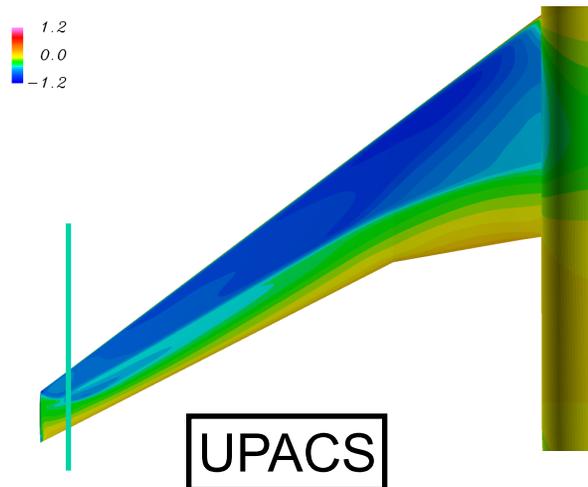
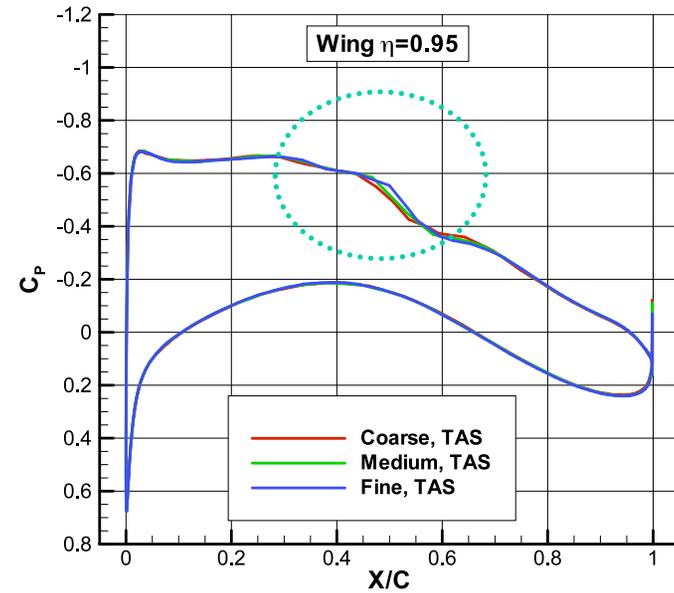
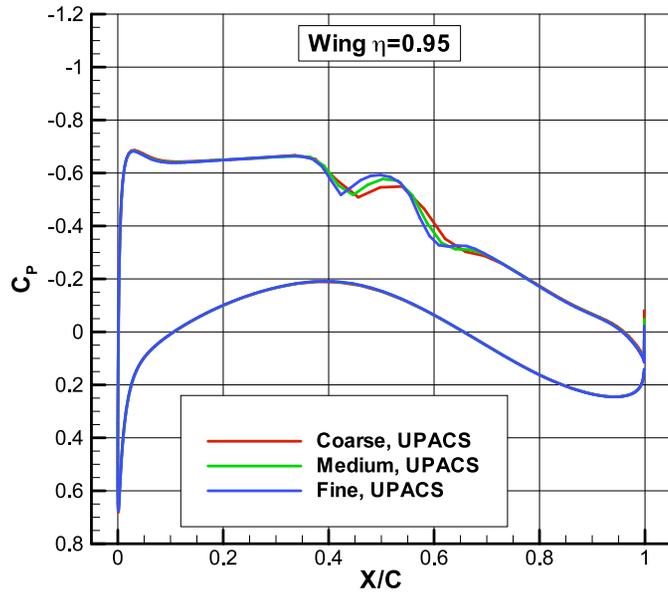
Case 1.1: Grid Convergence at Mach 0.85, $C_L=0.5$

Wing C_p at $\eta=0.5$



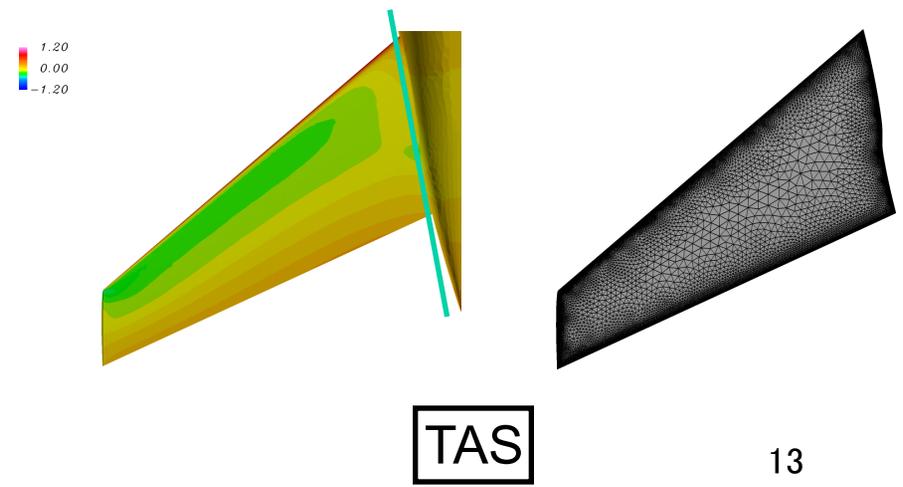
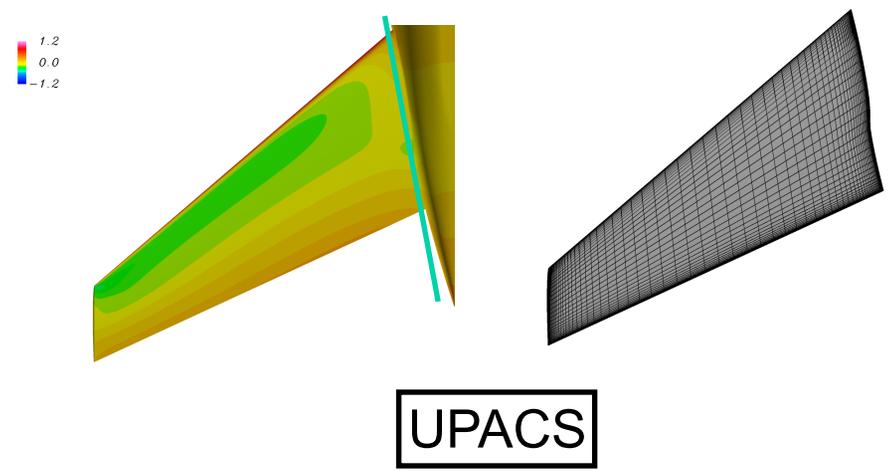
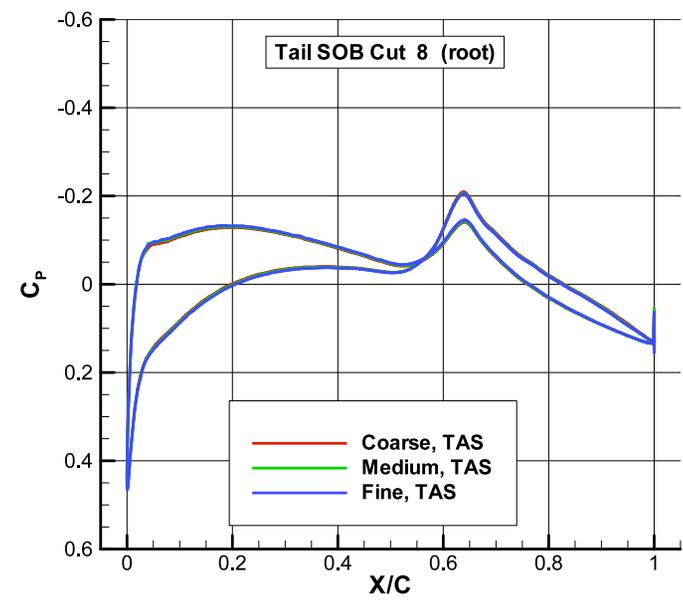
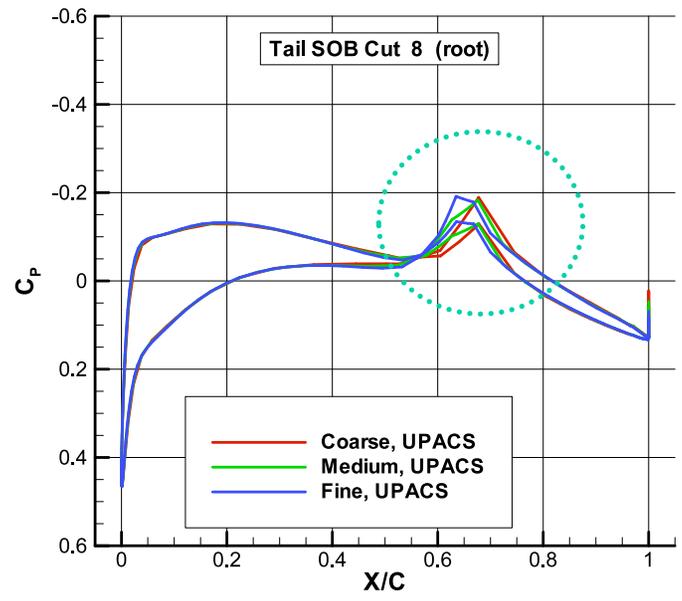
Case 1.1: Grid Convergence at Mach 0.85, $C_L=0.5$

Wing C_p at $\eta=0.95$



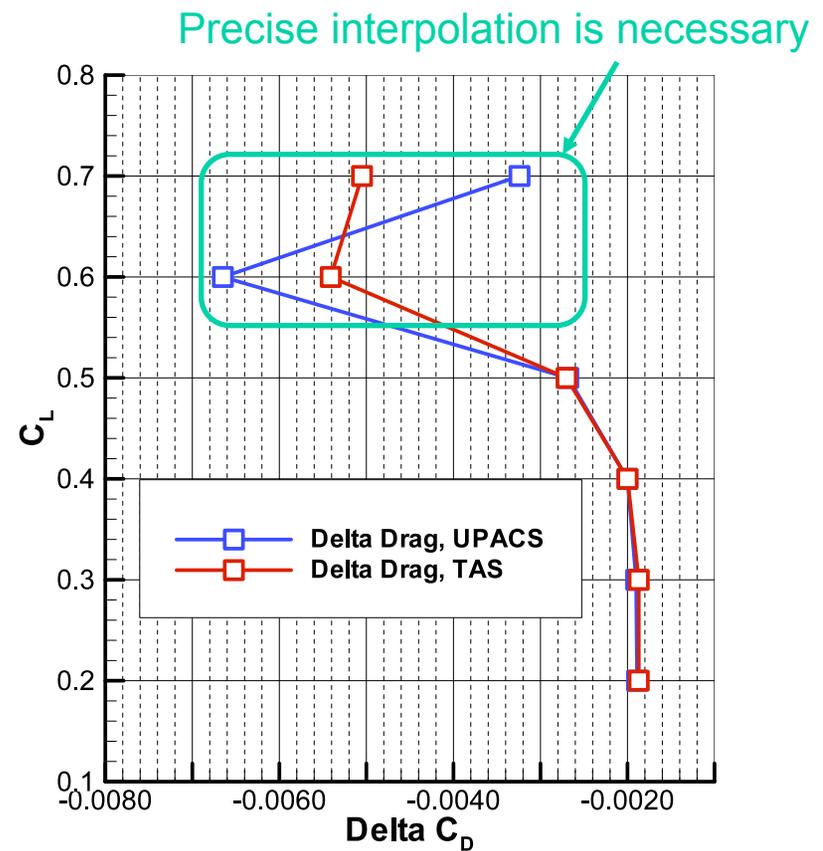
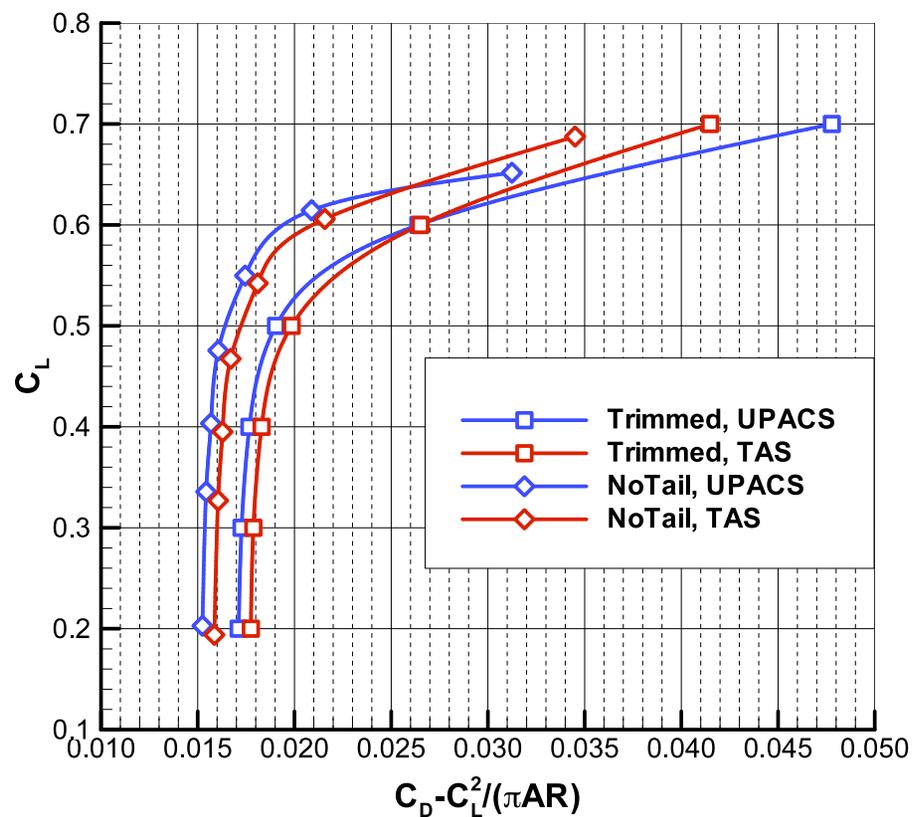
Case 1.1: Grid Convergence at Mach 0.85, $C_L=0.5$

■ Tail Cp near root



Case 1.2: Trimmed Drag at Mach=0.85

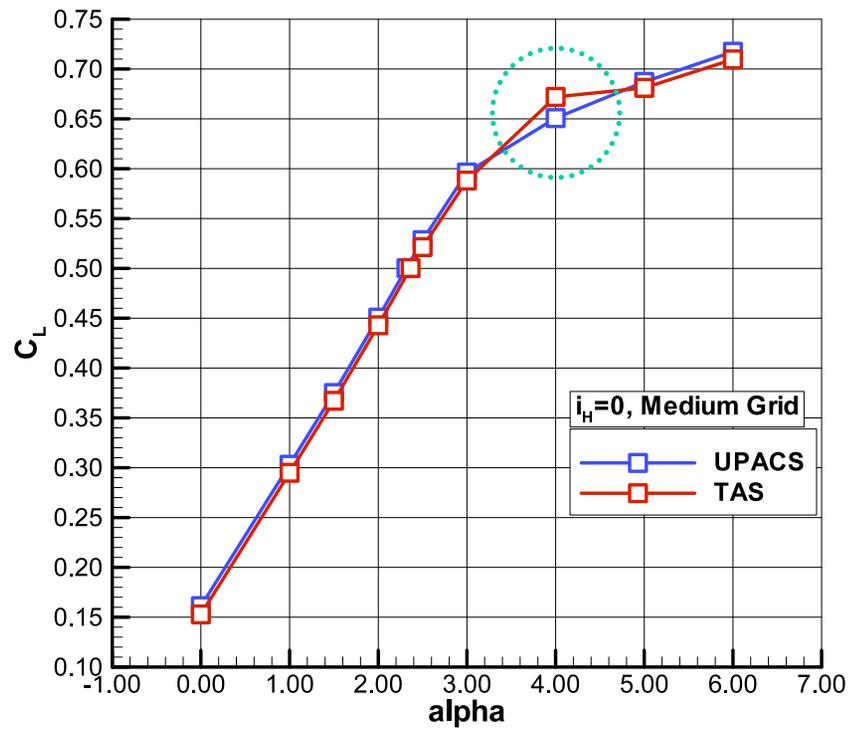
- Difference in drag polar is consistent for $CL < 0.6$.
- Delta drag varies from 19 counts to 67 counts with alpha.
- Delta drag by two methods agree well up to $CL=0.5$.



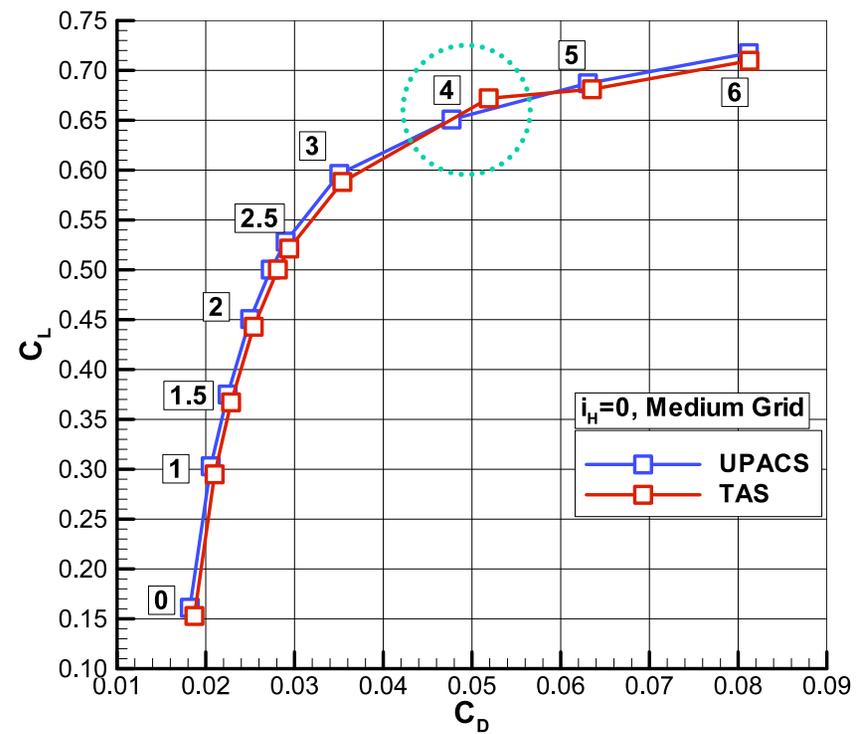
C_L and C_D

- $i_H=0$, $Re=5M$, Medium grid

C_L -alpha



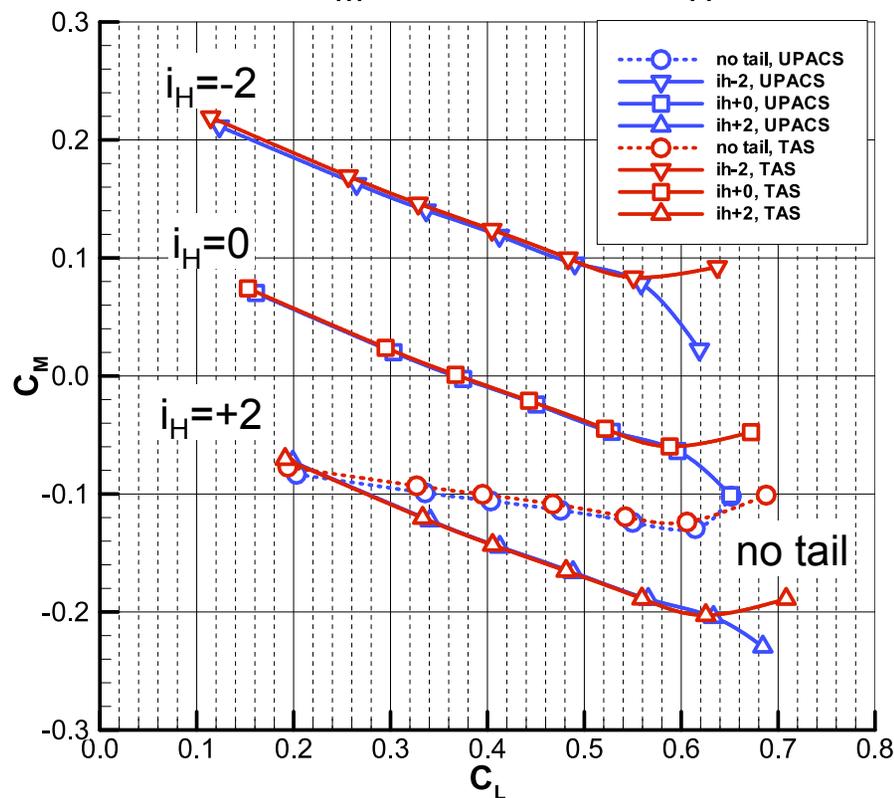
C_L - C_D



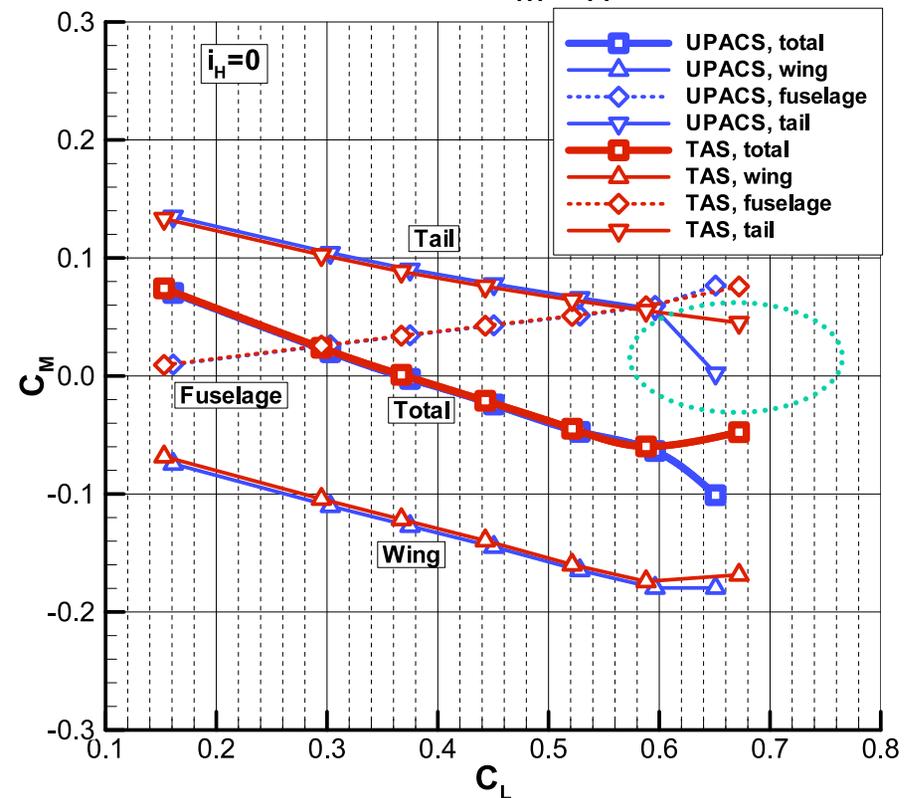
Effect of i_H on Pitching Moment

- Re=5M, Mach=0.85, Medium grid
- Very good agreement in the range $\alpha < 4\text{deg}$
- Tail C_M by UPACS shows sudden change at $\alpha=4\text{deg}$

Total C_M change with i_H

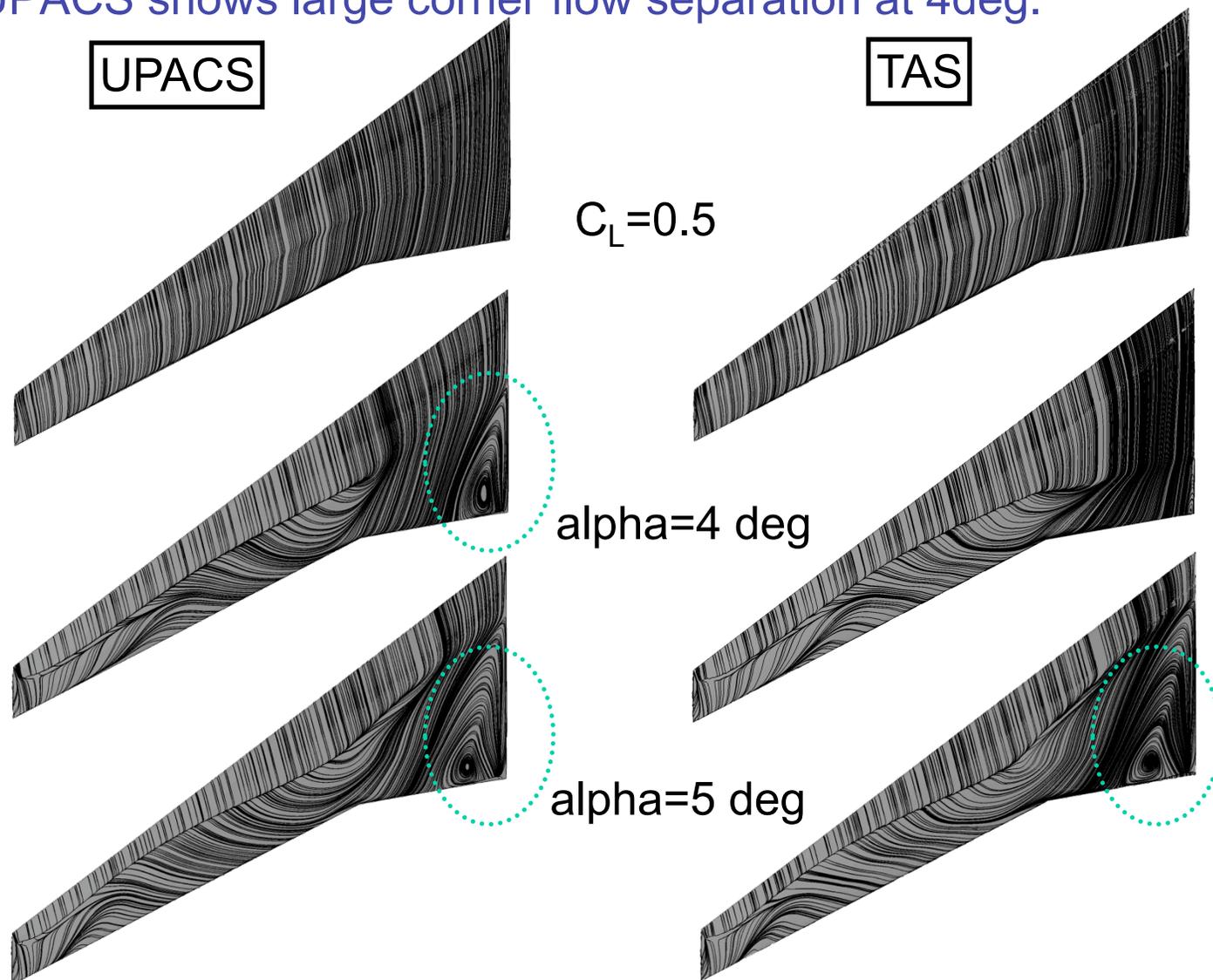


Component C_M , $i_H=0$



Oilflow on wing upper surface

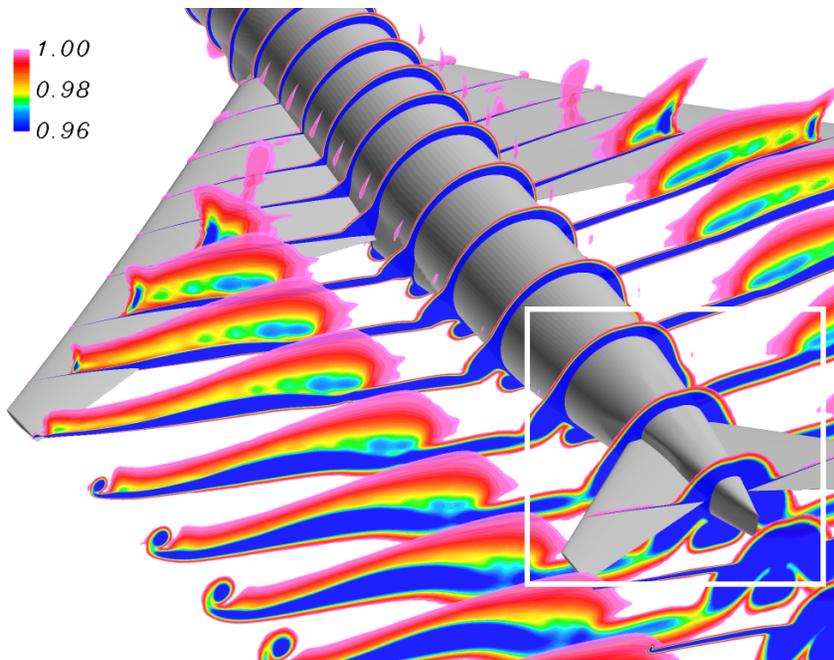
- UPACS shows large corner flow separation at 4deg.



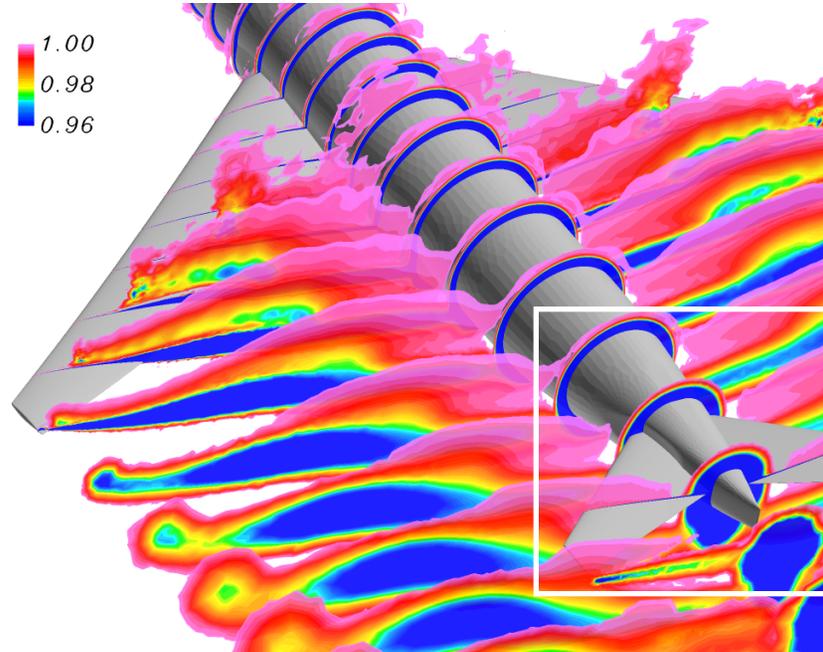
Influence of the corner separation on tail

Total Pressure, $\alpha=4\text{deg}$

UPACS

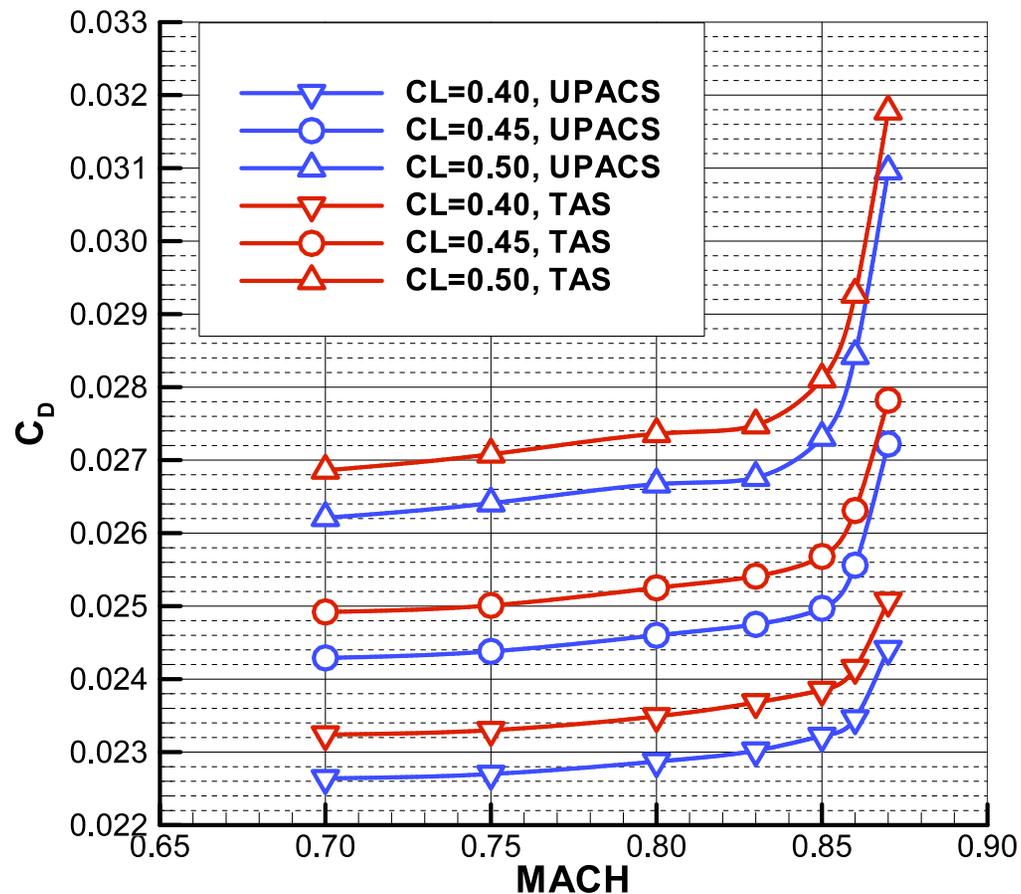


TAS

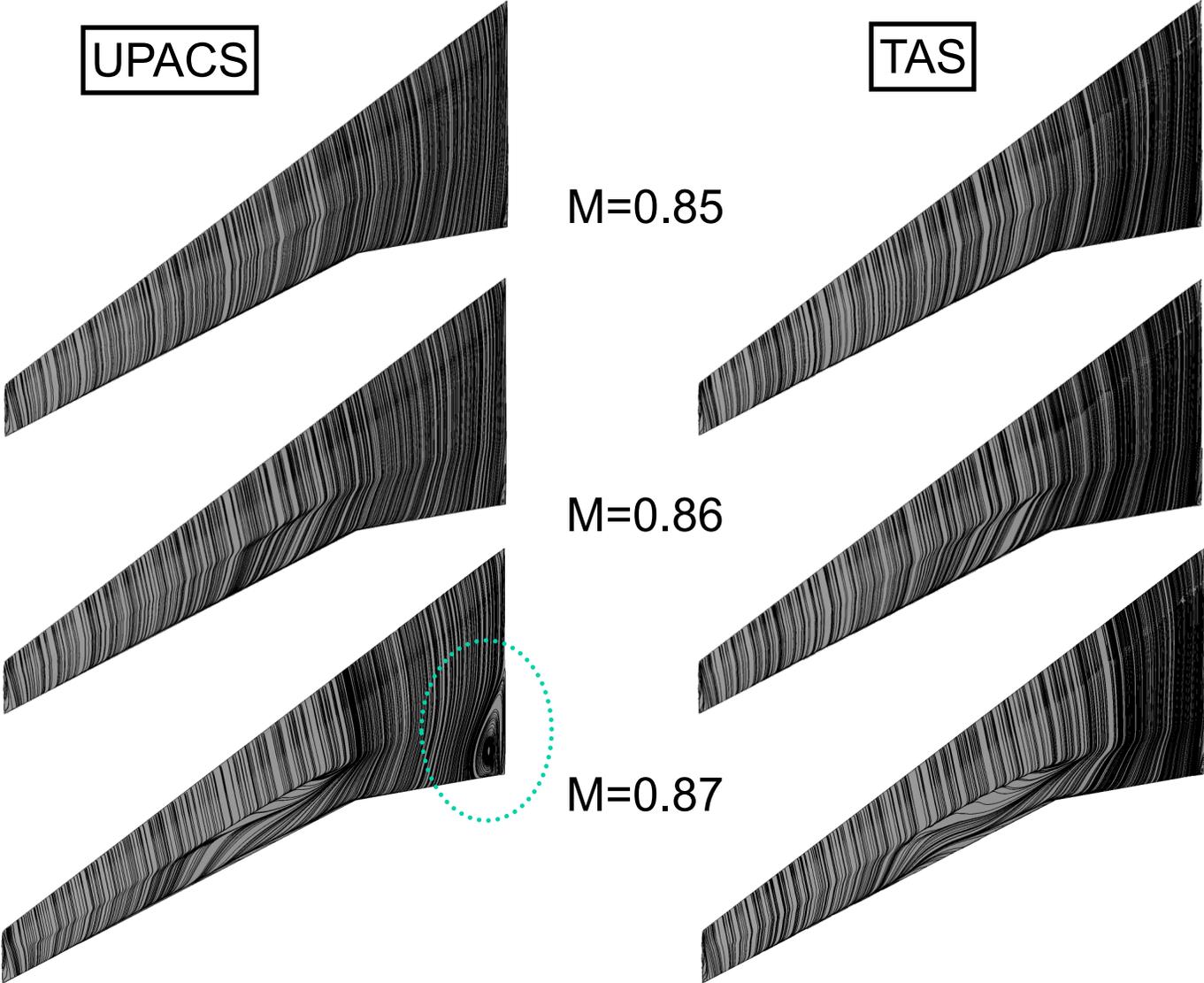


Case 2: Mach sweep

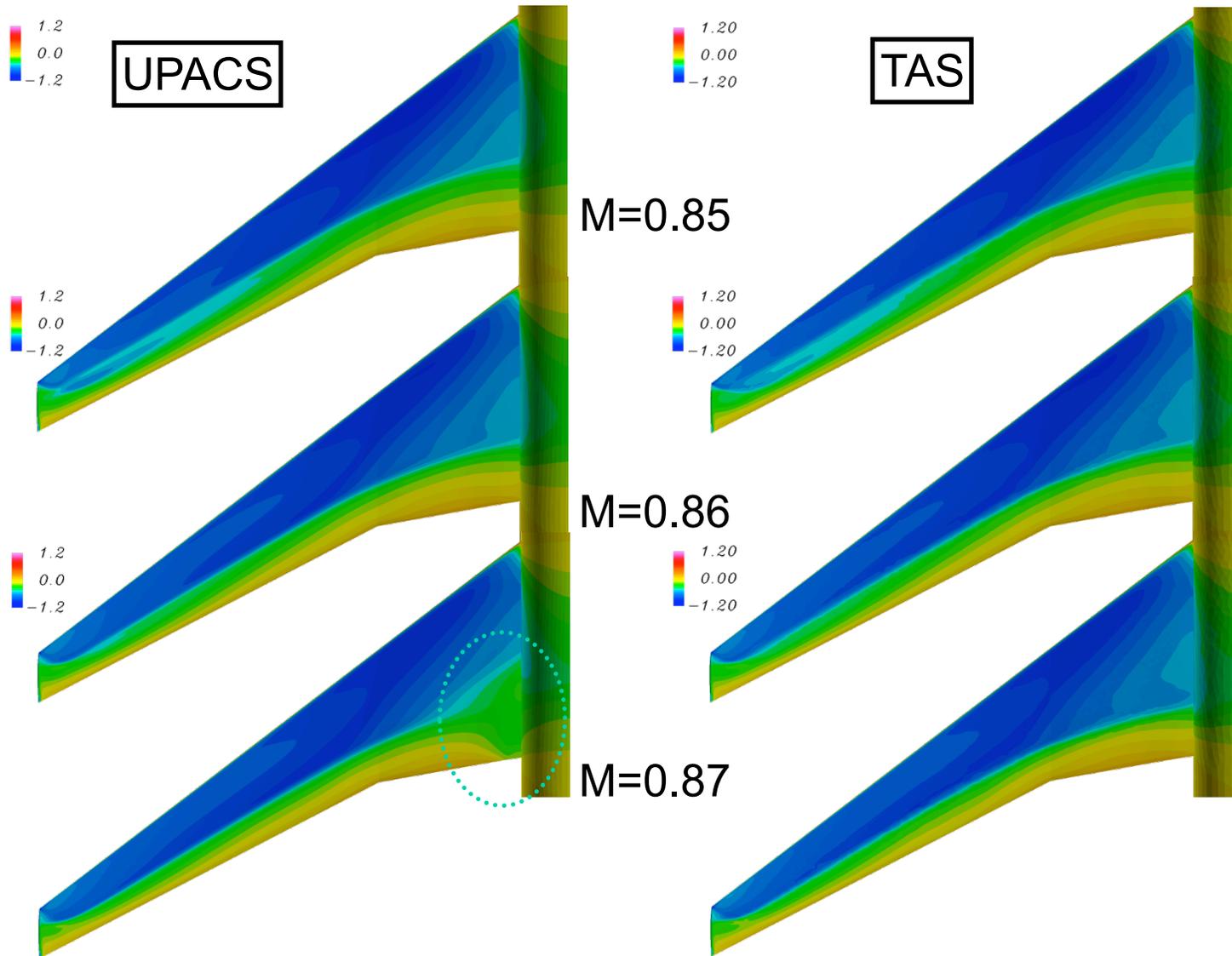
- $M < 0.85$: Obtained by interpolation of fixed alpha computations
- $M > 0.85$: specified C_L solutions when error (>0.5 cnts) is estimated
- Both methods show the same characteristics of drag divergence
- Consistent difference through the Mach number range



Oilflow on Wing Upper Surface

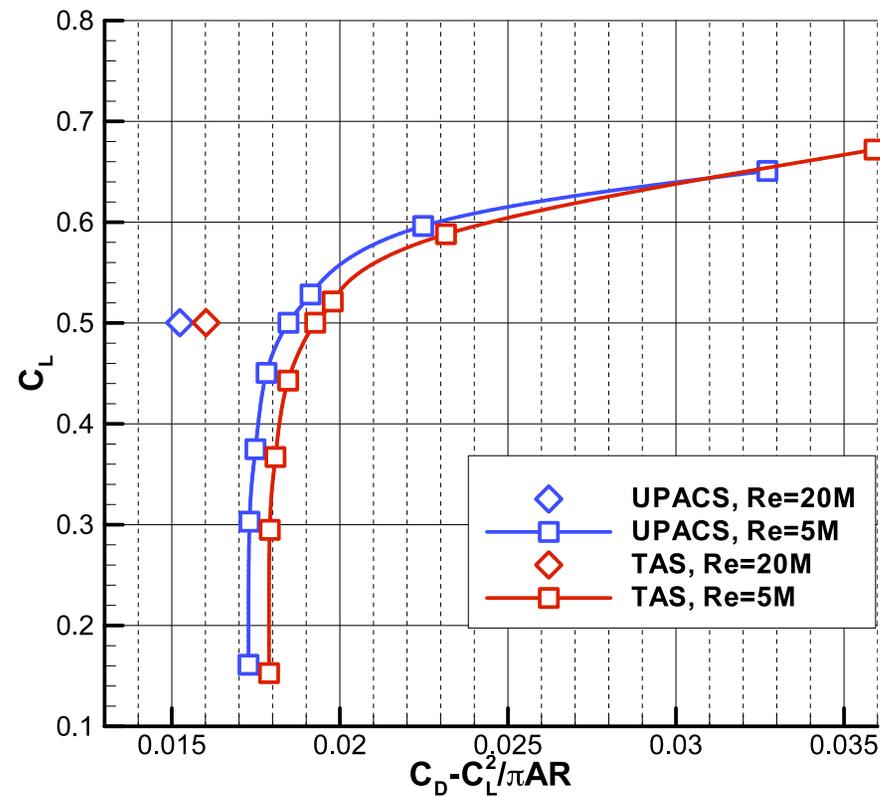


Cp on wing upper surface



Case 3: Reynolds number study

	Re=5M			Re=20M			Diff.		
	C_D	$C_{D_{PR}}$	$C_{D_{SF}}$	C_D	$C_{D_{PR}}$	$C_{D_{SF}}$	C_D	$C_{D_{PR}}$	$C_{D_{SF}}$
UPACS	0.0273	0.0147	0.0126	0.0241	0.0136	0.0105	0.0032	0.0011	0.0021
TAS	0.0281	0.0156	0.0125	0.0249	0.0144	0.0105	0.0033	0.0012	0.0021
Diff.	-0.0008	-0.0009	0.0001	-0.0008	-0.0008	0.0000	-0.0001	-0.0001	0.0000



Summary

■ Case1 (1) Grid convergence

- Both methods show good grid convergence.
 - 2 to 3 counts difference in the converged value?
- Unstructured method has 8 counts higher drag than structured method with Medium grid.
- This difference is consistent throughout the following studies except the case large flow separation is existing at wing root.
- Variation of skin friction drag is very small.

■ Case 1 (2) Downwash study

- Lower than $\alpha=4\text{deg.}$ or $C_L=0.6$, difference of trimmed drag between two methods is very small.
- Structured method shows large flow separation at $\alpha=4\text{ deg.}$ This changes the pitching moment of tail.
- Beyond 4 deg., Unstructured method also shows the same characteristics

■ Case 2 Mach sweep study

- Both method show the same characteristics of drag divergence.
- Start divergence around $\text{Mach}=0.85$ for $C_L=0.5$.
- Structured method shows large flow separation at wing root at $M=0.87$, $C_L=0.5$.

■ Case 3

- $\Delta C_{D_PR}=11$ counts, $\Delta C_{D_SF}=21$ counts with both methods.

Questions?