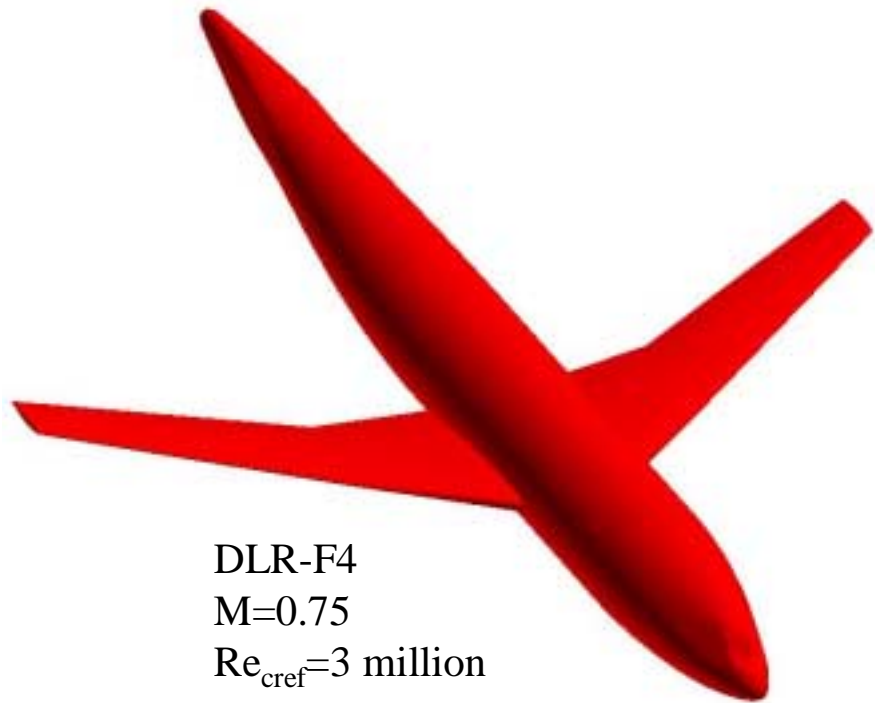


Drag Workshop Results Using CFL3D

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DLR-F4
 $M=0.75$
 $Re_{\text{cref}}=3 \text{ million}$

Issues addressed

- Effect of grid (1-to-1 vs. overset)
- Comparison of 3 turbulence models
- Issue of transition for supposedly “fully turbulent” computations
- Effect of different versions of SA model

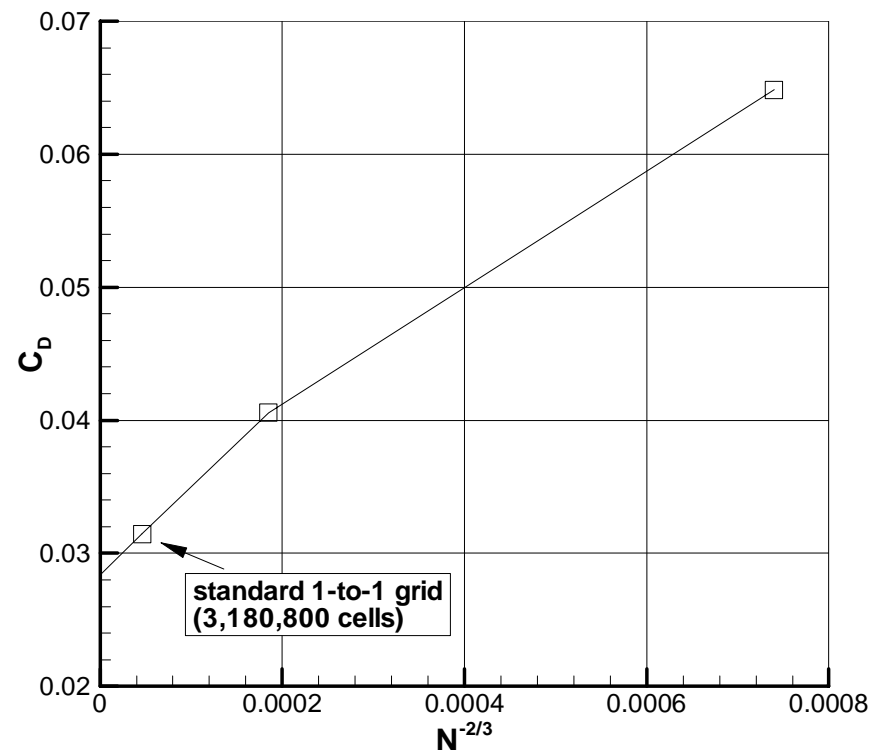
CFL3D V6.0

- Upwind, implicit 3-factor AF
- Finite volume, multigrid
- FDS (Roe)
- Globally 2nd order spatially accurate
- Multi-block capabilities, including 1-to-1, patched, and overset
- Parallel (MPI)

Grid convergence

1-to-1 grid, $M=0.75$, $C_L=0.5$

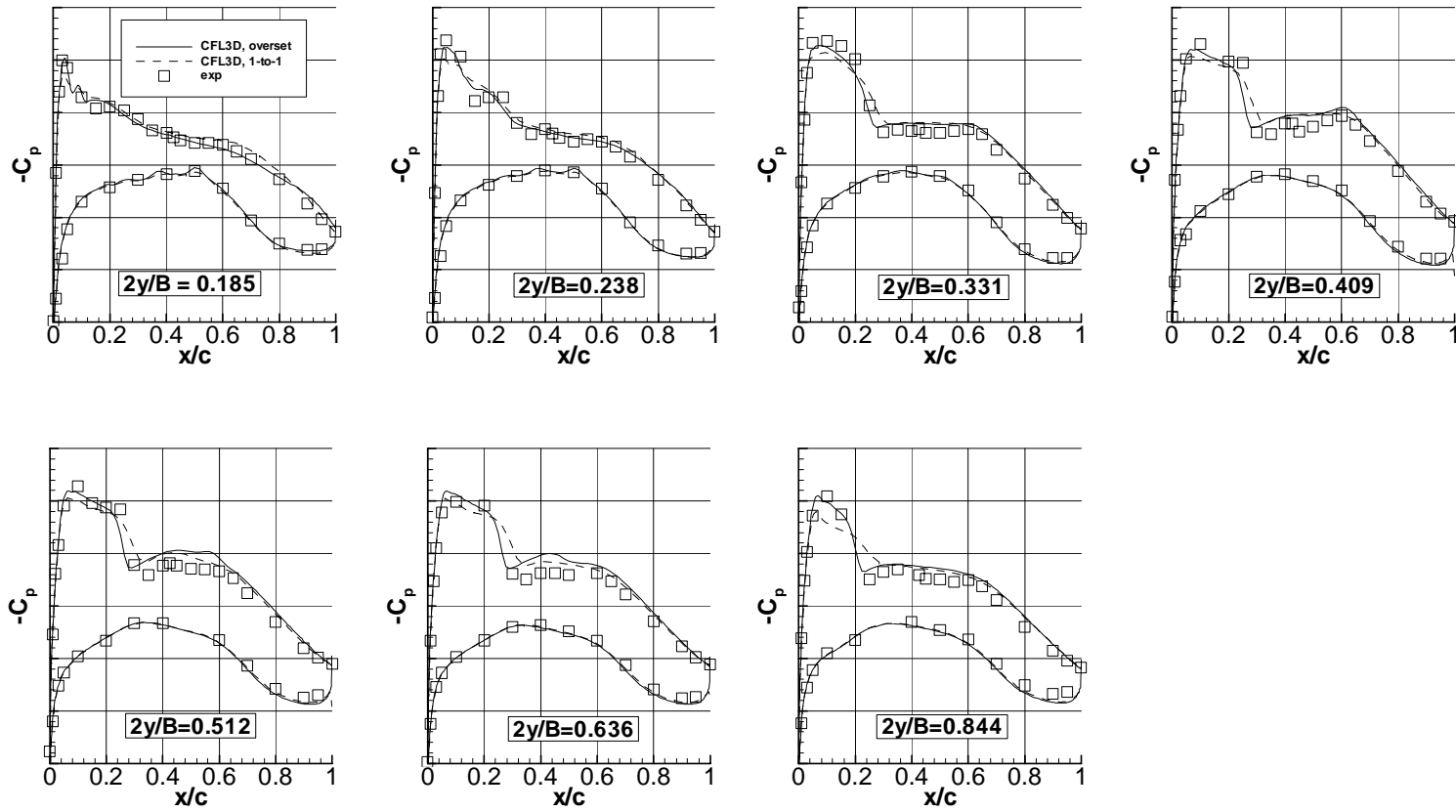
- If every-other-point grid is in asymptotic region for 2nd order global spatial convergence (doubtful), then C_D on fine grid is high by 30 counts!
- A finer-level grid of the same family is needed



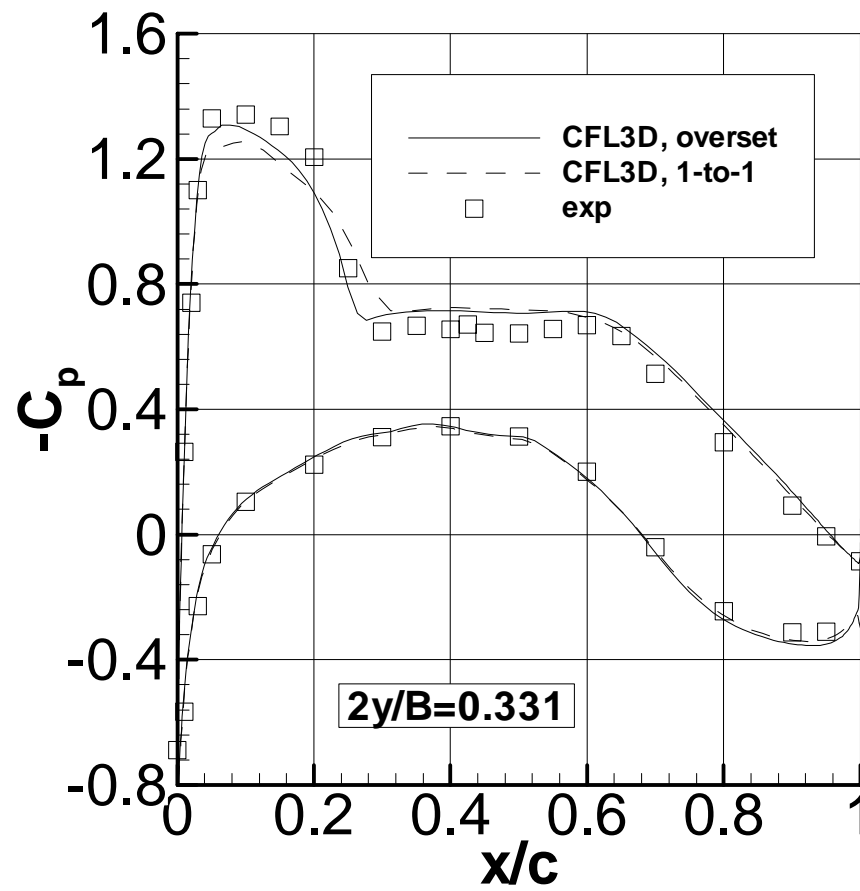
Effect of grid on surface pressures

$\alpha=0$ deg, $M=0.75$, $Re=3.e6$

Drag Prediction Workshop standard grids

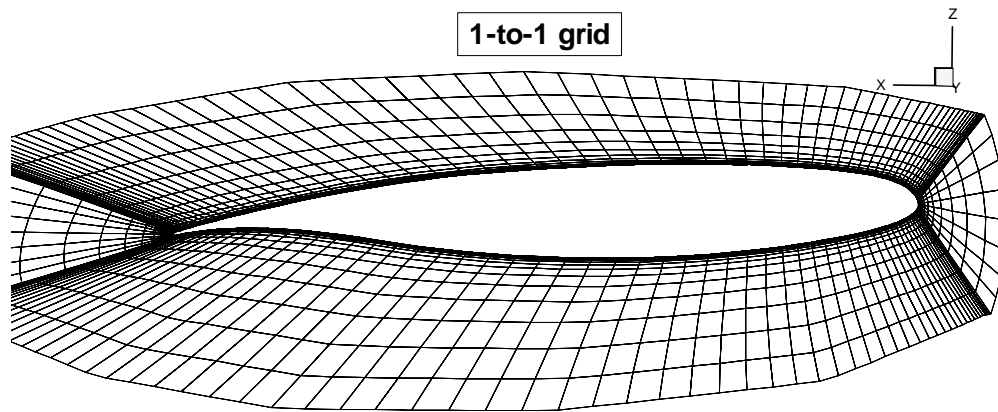


Detail



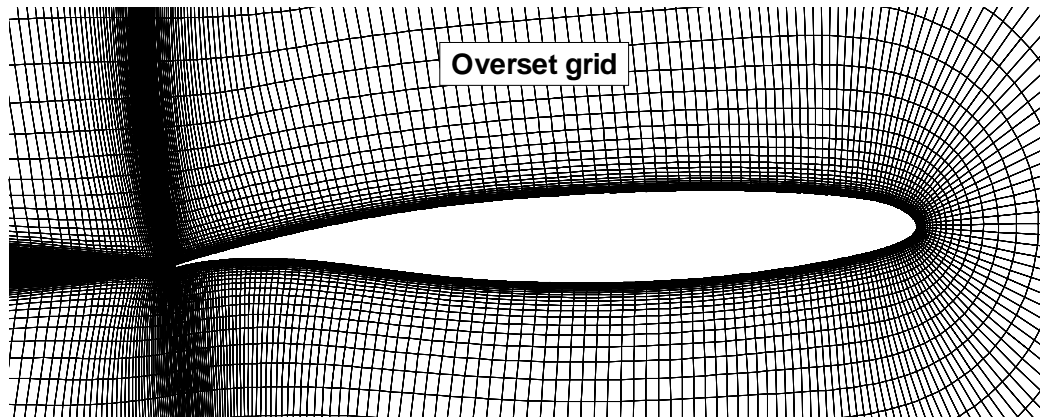
Grid comparison

near $y=230$ mm



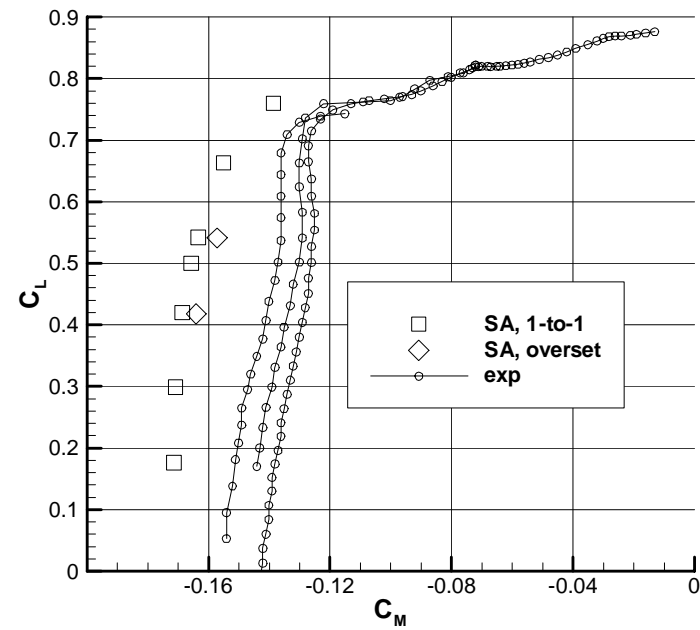
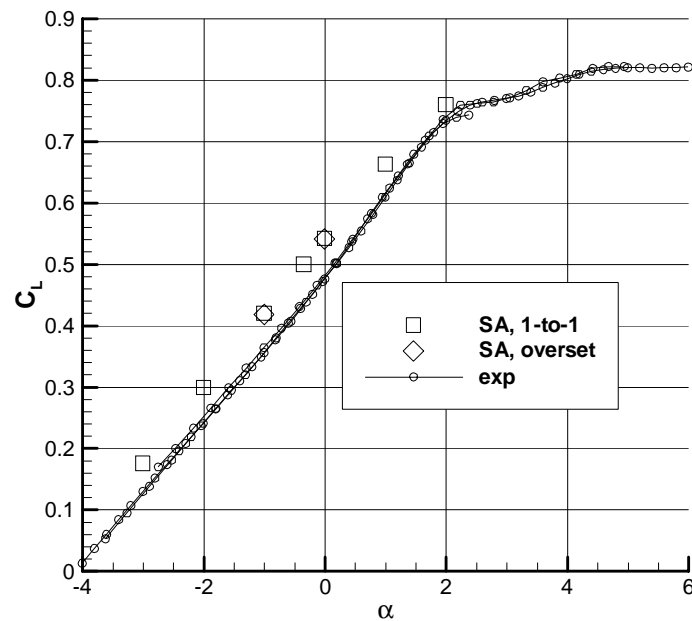
Entire grid:

3.2 million cells
50c extent

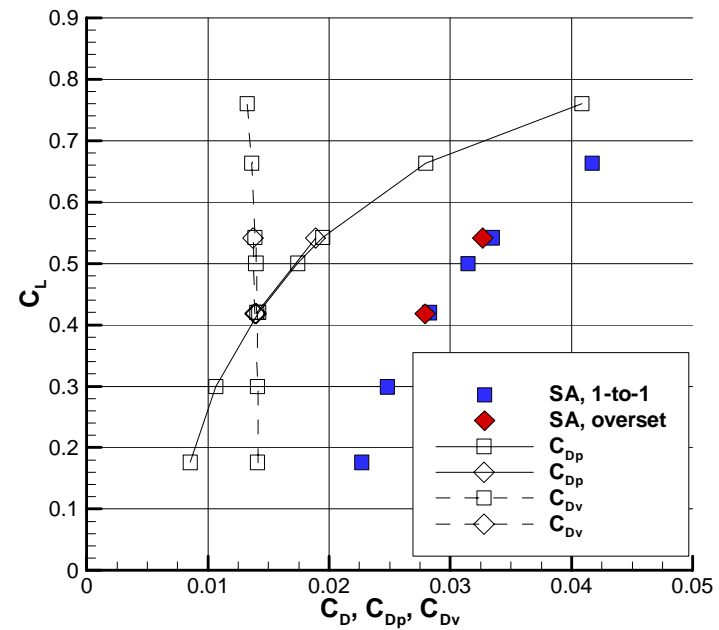
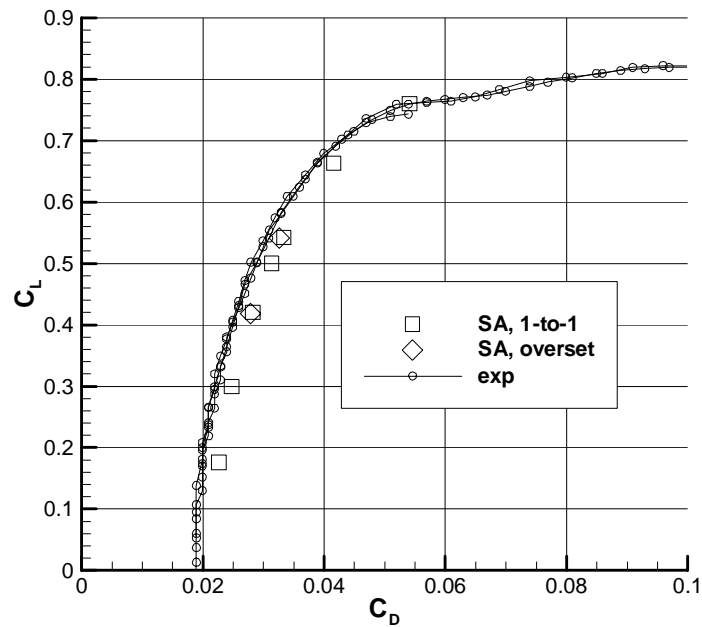


3.7 million cells
170c extent

Effect of grid on forces & moments



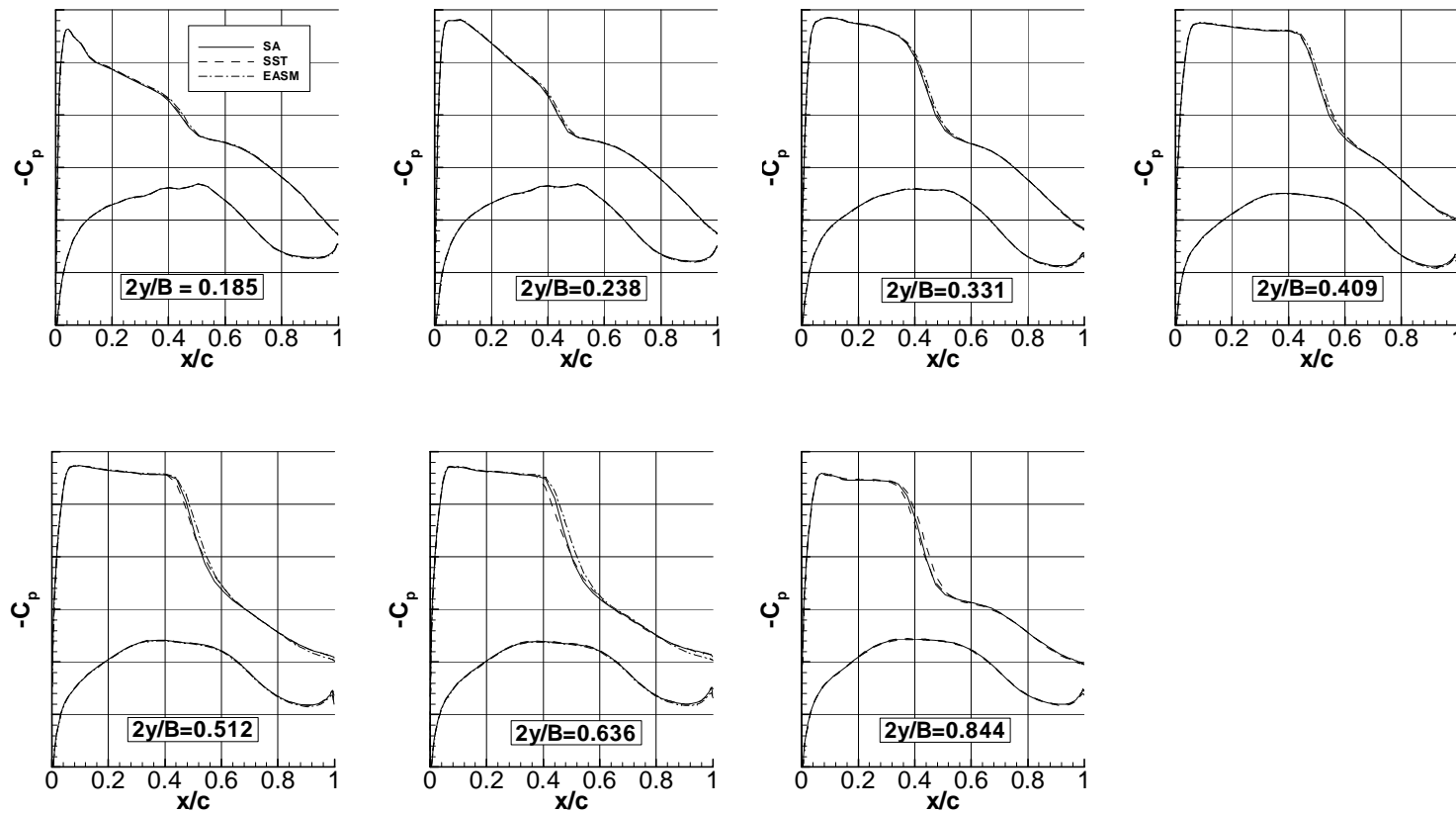
Effect of grid on forces & moments



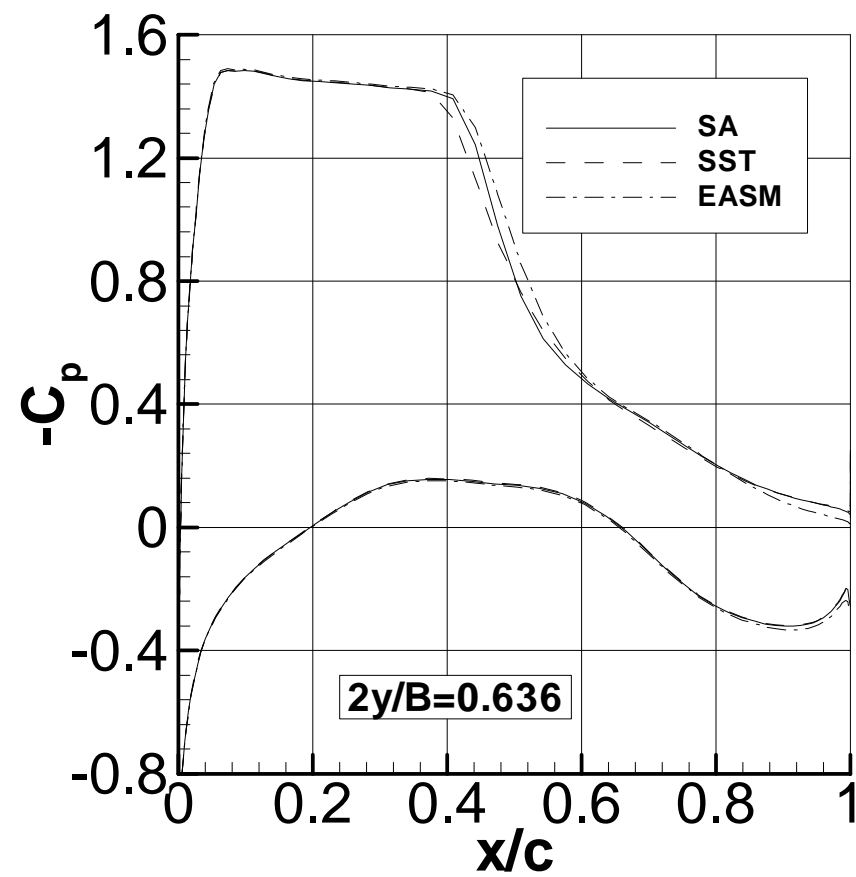
Effect of turbulence model on surface pressures

$\alpha=2$ deg, $M=0.75$, $Re=3.e6$

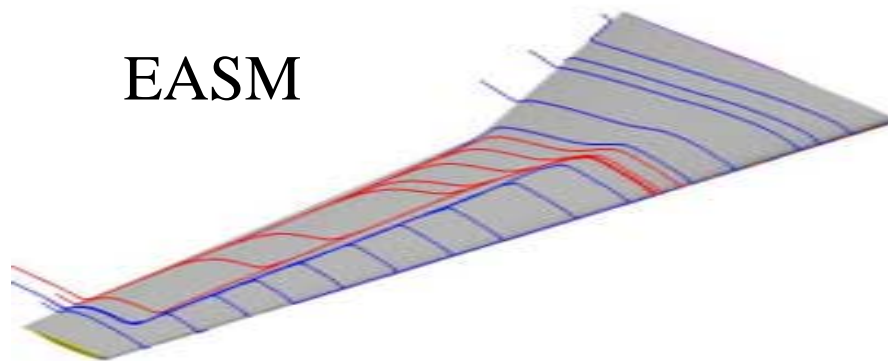
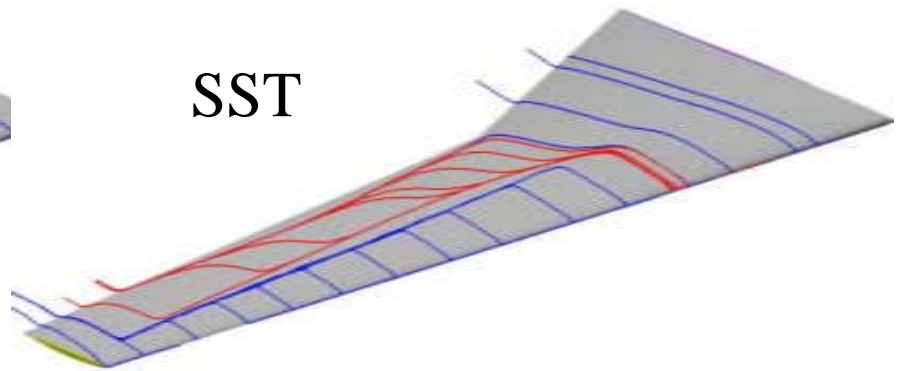
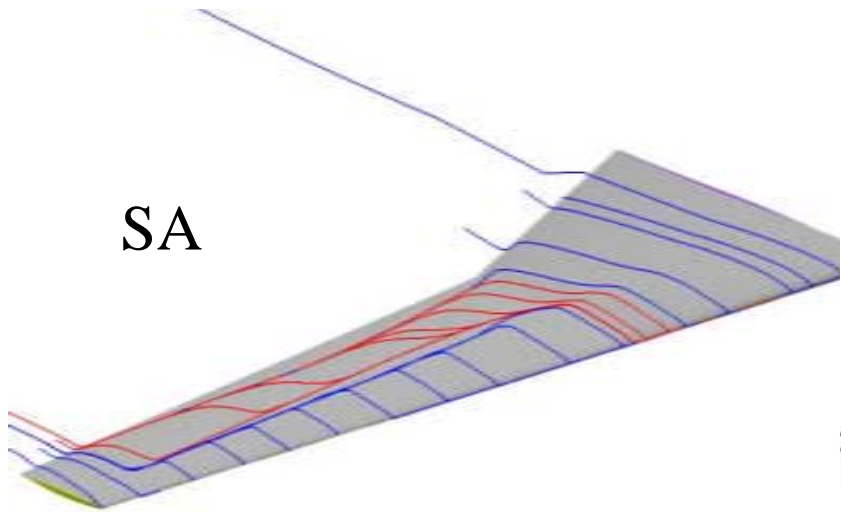
Drag Prediction Workshop 1-to-1 standard grid



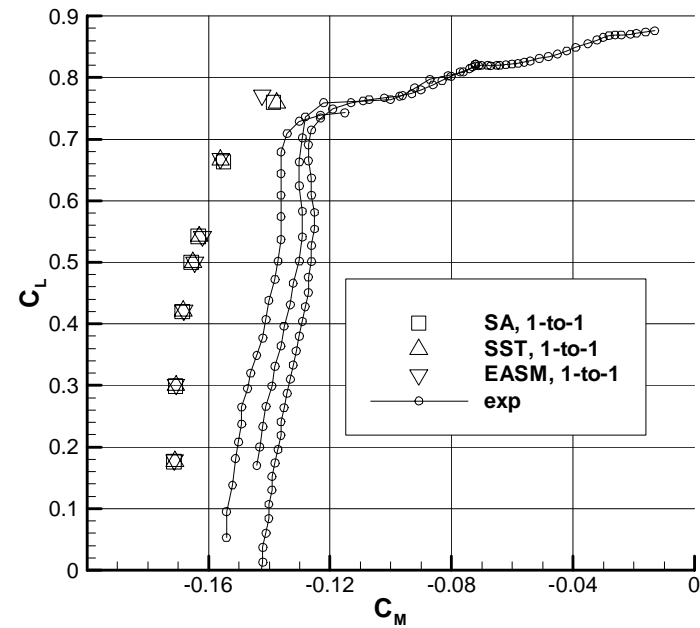
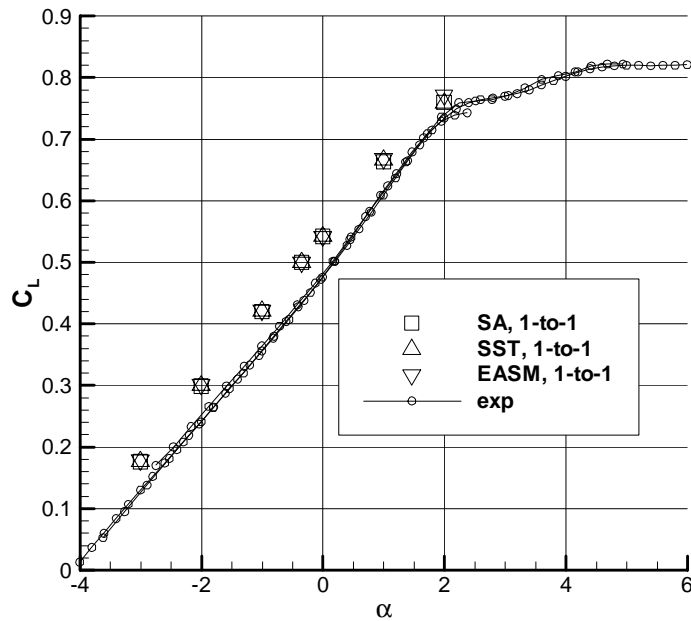
Detail



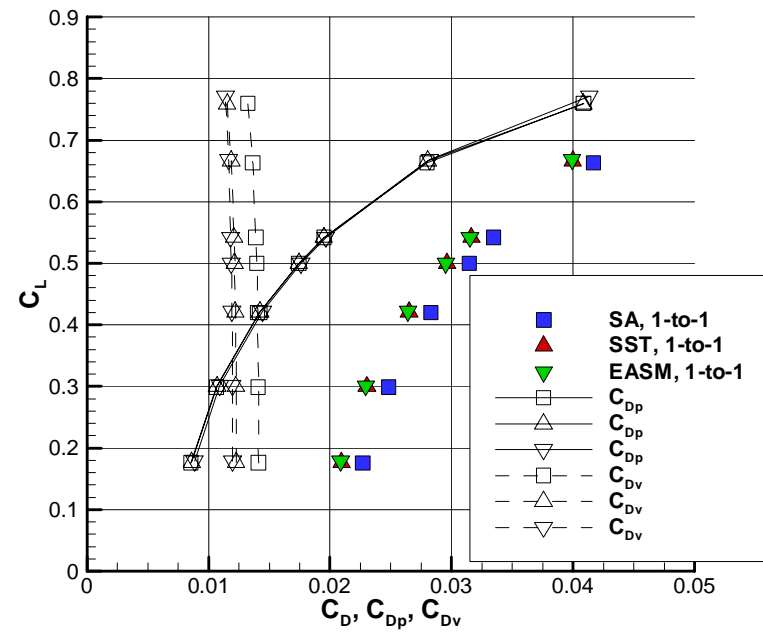
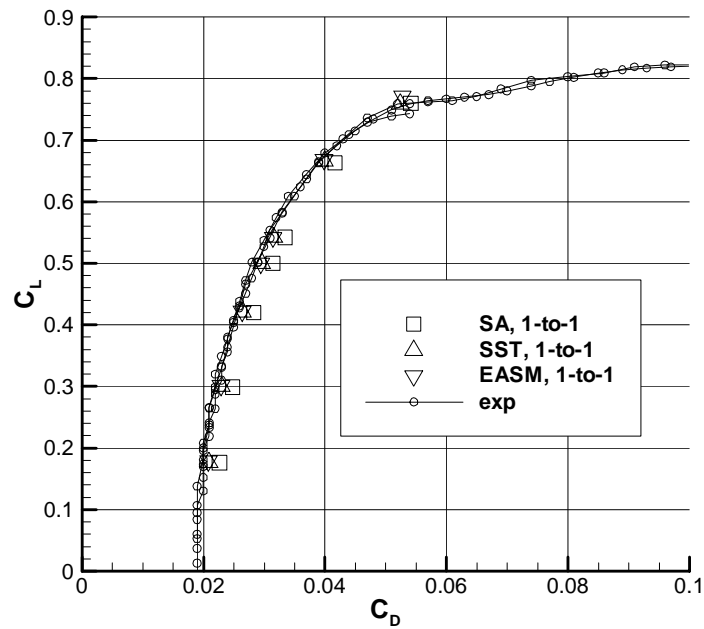
Streamlines at $\alpha=2^\circ$



Effect of turbulence model on forces & moments

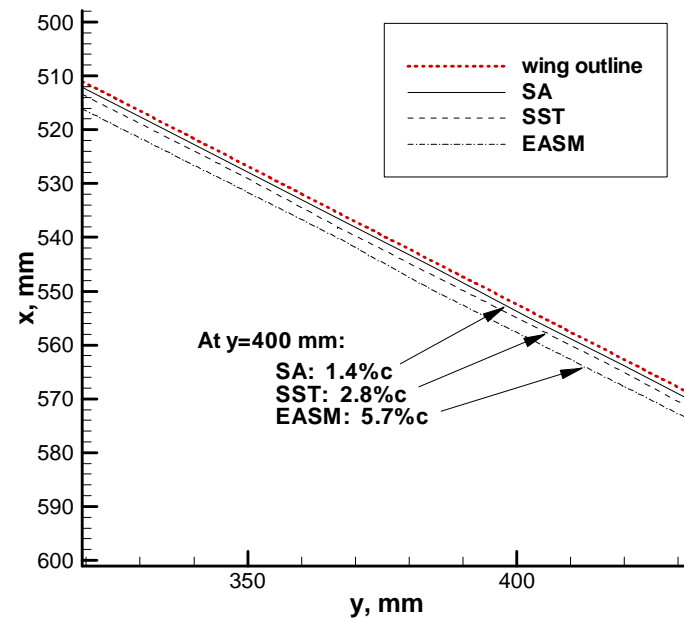
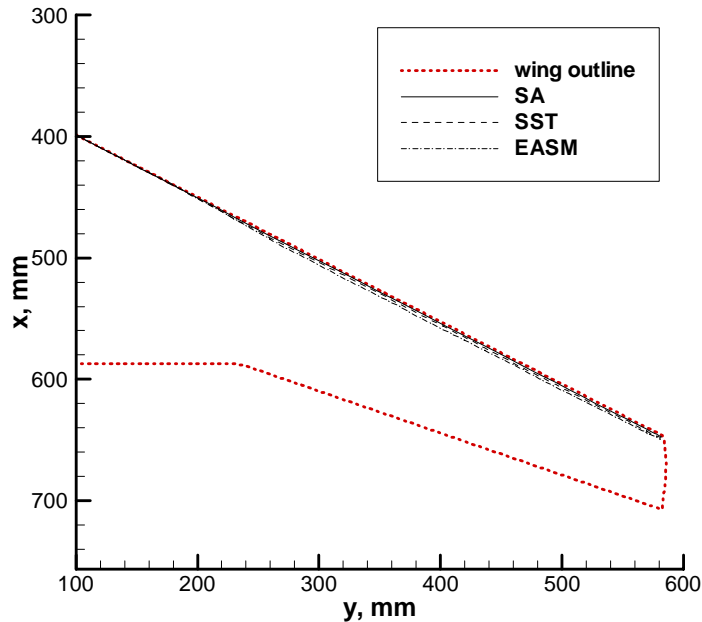


Effect of turbulence model on forces & moments

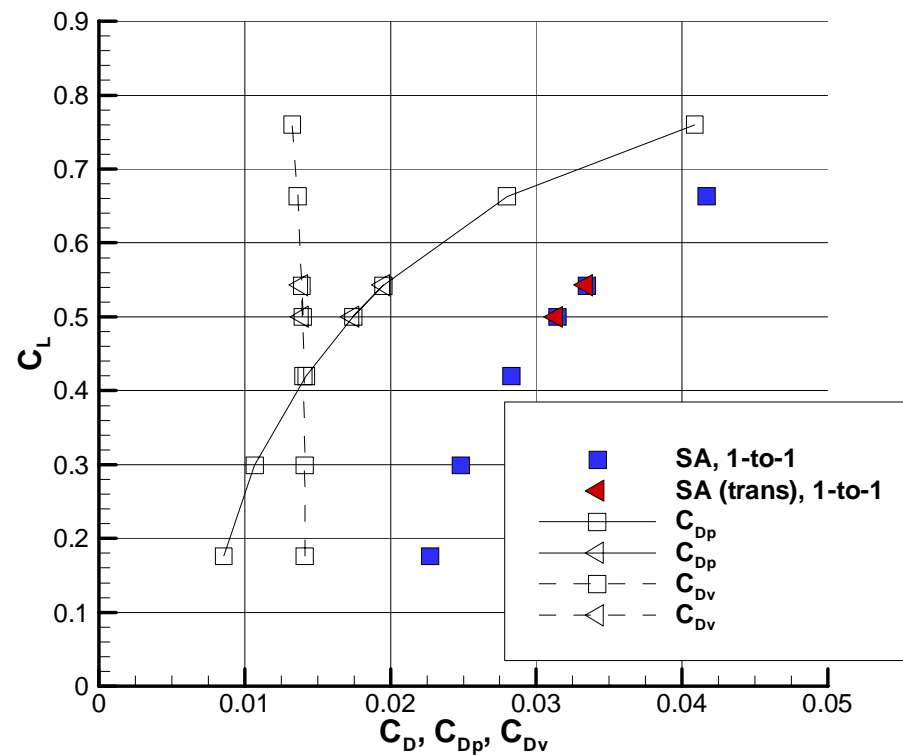


Actual “fully turbulent” transition locations for different turbulence models

$\alpha=0^\circ$



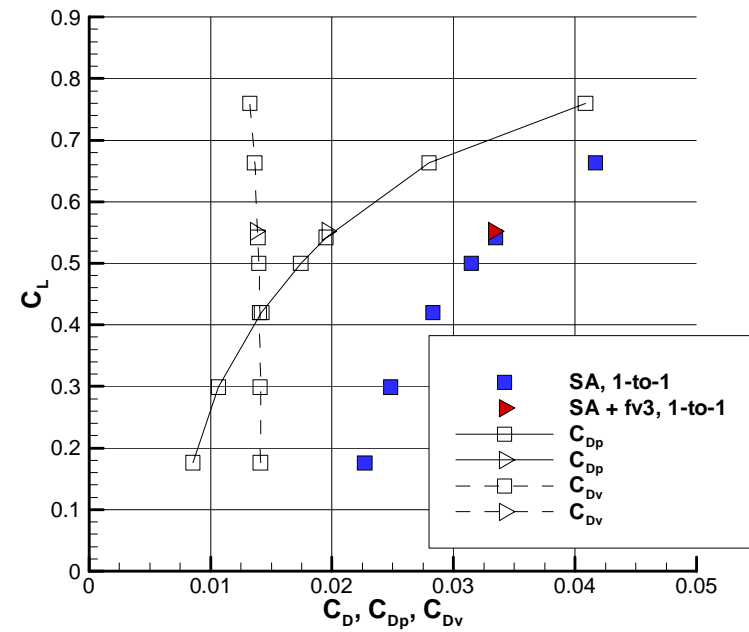
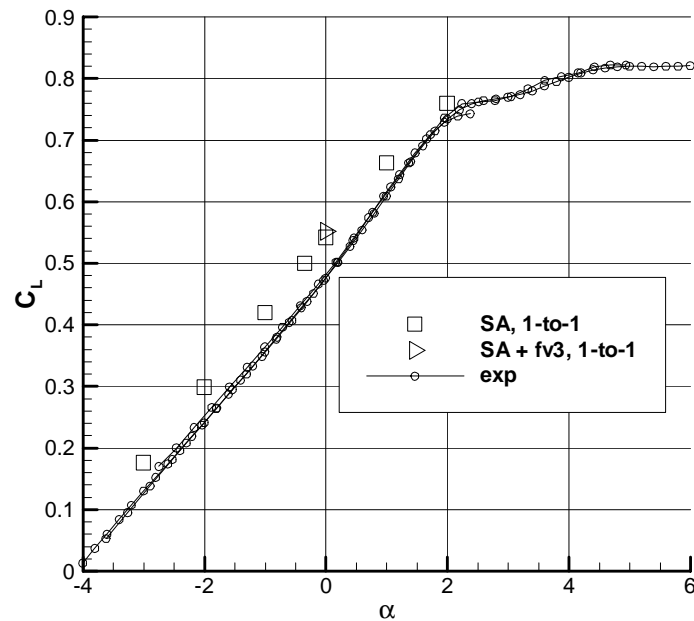
Effect of forcing SA transition to match “natural” transition of EASM



Effect of SA version on transition

- 2 versions of SA in wide use:
 - SA (Ia): “official” version in Aerospatiale Journal
 - SA+fv3: “unofficial” version resulting from a Spalart e-mail in early 90’s
- SA (Ia) transitions very near L.E.
 - Typically 1 – 2 % c for $\alpha=0$ deg case
- SA+fv3 delays transition for low Re (1-10 million)
 - 7 – 8 % c or more for $\alpha=0$ deg case (OVERFLOW results similar)
 - Seems to show more sensitivity to grid & free stream turbulence level chosen

Effect of SA version on forces



Summary

- Grid issues
 - Official 1-to-1 grid too coarse to resolve pressures (L.E. & shock under-resolved)
 - Nonetheless, global forces & moments similar to those using better quality overset grid; at $\alpha=0$:
 - C_D : ~8 count difference (2.4 %)
 - Family of grids (2 or 3 for each type) needed for grid sensitivity study

Summary, cont'd

- Turbulence model comparison (1-to-1 grid)
 - SST & EASM give lower C_D than SA by <20 counts (8.7 % difference at -3 deg, 3.3 % difference at $+2$ deg)
 - Primarily due to lower friction drag

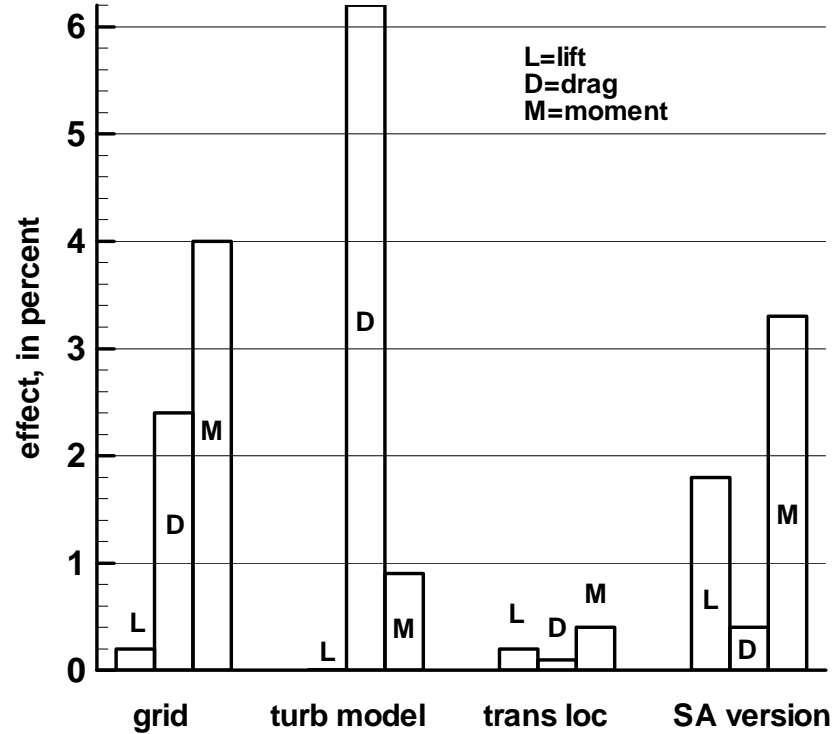
Summary, cont'd

- “Fully turbulent” is misnomer
 - All turbulence models “transition” on their own
 - At low Re (order 1-10 million), transition is not at the leading edge! E.g., for $\alpha=0$:
 - SA: 1-2 %c typical
 - SST: 2-5 %c typical
 - EASM: 2-7 %c typical
 - Effect is small: forcing SA to transition at EASM location changes C_D by <1 count (0.1 %)

Summary, cont'd

- Two versions of SA are known to be present in today's U.S. production codes
 - SA + fv3 (unofficial version) widely used, can delay transition significantly for low Re (order 1-10 million) compared to official SA (Ia)
 - Effect for $\alpha=0$:
 - $\Delta C_D = 1.4$ counts (0.4 %)

Summary of effects at $\alpha=0$



Conclusions

- Good quality grid a MUST
 - It is possible to miss details in C_p yet do reasonably well on forces and moments
 - Right answer for wrong reasons? – only a grid study using a family of grids will tell
- SA, SST, EASM turbulence models give very similar results for this case (but still ~20 count drag difference)
- CFD transition location should always be checked
- Better version control and consistency checks are needed for turbulence model coding

Comments on EASM

- Nonlinear explicit algebraic stress model, k-omega form (AIAA 2000-4323)
- More robust than earlier versions of EASM
- Roughly 40 % more expensive than SA
- As good as SA and SST for aerodynamic thin-shear flows, but better for flows where nonlinear and curvature effects are important
- Validation on-going

Recommendations for future workshops

- Give out family of successively finer grids for a required grid study
 - Grid study needed for CFD validation of this type
 - Some participants do not have 3D grid generation capability
 - “Official” grids ensure consistency
 - For wing body: 7 million, 3 million, 1.5 million cells? (structured)
 - Structured grids should be multigriddable
- Include surface Cps as part of required results
 - Integrated quantities hide things that could be helpful in evaluation
- More fixed-alpha cases and fewer fixed- C_L cases
 - Fixed alpha cases are easier to run & better for comparing code-to-code
- To ensure transition location is not a cause of variability:
 - Force transition at specified locations (harder), or...
 - Include high Re (order 50 million) fully turbulent case (easier)